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RESEARCH MEMORANDUM

PRESSURE DISTRIBUTION AT MACH NUMBERS UP TO 0.90

ON A CAMBERED AND TWISTED WING HAVING 40° OF

SWEEPBACK AND AN ASPECT RATIO OF 10,

INCLUDING THE EFFECTS OF FENCES

By Frederick W. Boltz and
Harry H. Shibata

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NATIONAL ADVISORY COMMITTEE
FOR AERONAUTICS

WASHINGTON

March 9, 1953

~~CONFIDENTIAL~~

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RESEARCH MEMORANDUM

PRESSURE DISTRIBUTION AT MACH NUMBERS UP TO 0.90
ON A CAMBERED AND TWISTED WING HAVING 40° OF
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SUMMARY

Pressure-distribution measurements were made on a semispan model of a cambered and twisted wing, alone and in combination with a fuselage. The wing had 40° of sweepback, an aspect ratio of 10, a taper ratio of 0.4, and 5° of washout at the tip. The wing thickness distribution in sections normal to the reference sweep line was the NACA 4-digit series and the maximum thickness varied from 14-percent chord at the root to 11-percent chord at the tip. The wing sections were cambered for a design lift coefficient of 0.40.

The chordwise distributions of pressure coefficient at nine semi-span stations on the wing are presented for Mach numbers of 0.165 and 0.25 at a Reynolds number of 8,000,000 and for Mach numbers from 0.25 to 0.90 at a Reynolds number of 2,000,000. Tabulated pressure data are presented for the wing without fences and with a four-fence configuration.

The results indicate that, at all Mach numbers, flow separation originated at the trailing edge near the midsemispan of the wing. The separation spread toward both the root and the tip with increase in angle of attack, complete flow separation eventually occurring at the outer sections. Increasing the Reynolds number at low speed reduced the amount of flow separation over the wing.

Upper-surface fences reduced the trailing-edge flow separation outboard of the fences. At the higher Mach numbers, the four-fence configuration was considerably more effective than the three-fence configuration.

The spanwise distribution of load was found to be accurately predicted by the modified Falkner 19×1 method, provided little flow separation existed on the wing.

INTRODUCTION

A semispan model of a high-aspect-ratio swept wing in combination with a fuselage of high fineness ratio has been tested in the Ames 12-foot pressure wind tunnel. The wing was cambered and twisted, had 40° of sweepback, and an aspect ratio of 10. The results of measurements of the forces and moments on the wing alone, on the fuselage alone, and on the wing-fuselage combination have been presented in reference 1. The results of pressure-distribution measurements at nine semispan stations of the wing, alone and in the presence of the fuselage, are presented in the present report. Pressure data are also included for the wing with three upper-surface fences and with four upper-surface fences.

NOTATION

- a mean-line designation, fraction of chord over which design load is uniform
- $\frac{b}{2}$ wing semispan perpendicular to the plane of symmetry, feet
- C_D drag coefficient $\left(\frac{\text{drag}}{qS} \right)$
- C_L lift coefficient $\left(\frac{\text{lift}}{qS} \right)$
- C_m pitching-moment coefficient about the quarter point of the wing mean aerodynamic chord $\left(\frac{\text{pitching moment}}{qS\bar{c}} \right)$
(See fig. 1(a).)
- c local chord parallel to plane of symmetry, feet
- c' local chord perpendicular to the reference sweep line, feet
- \bar{c} mean aerodynamic chord $\left(\frac{\int_0^{b/2} c^2 dy}{\int_0^{b/2} c dy} \right)$, feet

- c_{av} average chord $\left(\frac{2S}{b}\right)$, feet
- c_l section lift coefficient
- c_{l_1} design section lift coefficient
- c_m section pitching-moment coefficient [c_n (0.25-c.p.)]
- c_n section normal-force coefficient
- c.p. section center-of-pressure location, fraction of local chord
- M Mach number
- P pressure coefficient $\left(\frac{p_l - p}{q}\right)$
- p_l local static pressure, pounds per square foot
- p free-stream static pressure, pounds per square foot
- q free-stream dynamic pressure, pounds per square foot
- R Reynolds number based on the mean aerodynamic chord
- S area of semispan wing, square feet
- t maximum thickness of section, feet
- y lateral distance from the plane of symmetry, feet
- α angle of attack of the root chord at the plane of symmetry, degrees
- α_u angle of attack uncorrected for tunnel-wall interference and angle-of-attack countercorrection, degrees
- ϕ angle of twist measured in plane parallel to the plane of symmetry (positive for washin), degrees
- η fraction of semispan $\left(\frac{y}{b/2}\right)$

MODEL AND APPARATUS

The wing had 40° of sweepback, an aspect ratio of 10, and a taper ratio of 0.4. (See fig. 1(a).) The reference sweep line was the line joining the quarter-chord points of the sections inclined 40° to the plane of symmetry (26.65-percent-chord points of the streamwise sections). The thicknesses of sections perpendicular to the reference sweep line varied from 14 percent of the chord at the root to 11 percent of the chord at the tip. The tip was washed out 5° . The twist and the thickness ratio of the sections varied from the root to the tip so that straight lines joined equal-percent-chord points at all sections. These variations of thickness ratio and twist along the semispan are shown in figure 1(b). The sections perpendicular to the reference sweep line at the root and at the tip were formed by combining an NACA 4-digit thickness distribution with an $a = 0.8$ modified mean line (reference 2) having an ideal lift coefficient of 0.40. The coordinates of NACA 4-digit thickness distributions and the method of combining the thickness distribution with the mean line are given in reference 3. Details of two fence configurations investigated are shown in figure 1(c). A discussion of the basis for the selection of the geometric properties of the wing and of the fence configurations is given in reference 1.

The wing was constructed of steel and was equipped with nine rows of pressure orifices on both the upper and lower surfaces as shown in figure 1(c). The orifices were distributed along the chord from the leading edge to the 95-percent-chord point and were staggered one-eighth inch on either side of the station planes.

The fuselage, which had a fineness ratio of 12.6, was half of a body of revolution having a cylindrical midsection. Coordinates of the fuselage are listed in table I. The incidence of the wing root was 3° relative to the fuselage center line and the upper surface of the wing was tangent to the top of the fuselage at the plane of symmetry.

Photographs of the wing-fuselage combination in the wind tunnel and details of the fence installation are presented in figure 2.

TESTS

The pressure-distribution data presented in this report were obtained simultaneously with the lift, drag, and pitching-moment data presented in reference 1. For the wing-fuselage combination the chordwise distributions of pressure at nine semispan stations on the wing were measured at a Reynolds number of 2,000,000 for Mach numbers from 0.25 to 0.90 and at a Reynolds number of 8,000,000 for a Mach number of 0.25.

Data were obtained for the wing-fuselage combination without fences, with three fences, and with four fences for angles of attack from -4° to a maximum of 20° at the lower Mach numbers (maximum angle of attack was limited by lack of clearance between the fuselage and the tunnel wall). At the higher Mach numbers the maximum angles of attack were reduced due to wind-tunnel choking. In order to obtain data at angles of attack above 20° at a Mach number of 0.165 and a Reynolds number of 8,000,000, the wing was tested without the fuselage. These data for the wing alone were obtained without fences and with four fences.

CORRECTIONS TO DATA

The dynamic pressure and Mach number have been corrected for constriction effects due to the presence of the tunnel walls by the methods of reference 4. Corrections for tunnel-wall-interference effects originating from lift on the model by the method of reference 5 and for drag tares caused by aerodynamic forces on the exposed portion of the turntable on which the model was mounted have been applied to the force data. The magnitudes of these corrections may be found in reference 1.

The pressure data and the coefficients derived therefrom are presented in this report for values of uncorrected angle of attack α_u . The relation between the corrected and uncorrected angles of attack is as follows:

$$\alpha = 0.99 \alpha_u + \Delta\alpha$$

where

$$\Delta\alpha = 0.377 C_L$$

The constant 0.99 is the ratio between the geometric angle of attack and the uncorrected reading of the angle-of-attack counter, and $\Delta\alpha$ is the correction for the tunnel-wall interference.

No attempt has been made to evaluate tares due to interference between the model and the turntable or to compensate for the tunnel-floor boundary layer which, at the turntable, had a displacement thickness of one-half inch.

From the results of static load tests on the wing (reference 1) it was found that, when the aerodynamic loading was greatest ($M = 0.25$, $R = 8,000,000$), the twist at the tip due to bending and torsion was about -2.2° per unit lift coefficient. No attempt has been made to correct the data for the effects of this aeroelastic distortion.

RESULTS

The pressure data at nine semispan stations of the wing without fences and with four fences are presented as pressure coefficients in tabular form. Table II is an index to these data which are presented in tables III through XVI.

The distribution of pressure coefficient at five of the nine semi-span stations of the wing for the wing-fuselage combination without fences are presented in figures 3, 4, and 5. Data are shown at various angles of attack for Reynolds numbers of 2,000,000 and 8,000,000 at a Mach number of 0.25, and for Mach numbers of 0.80 and 0.90 at a Reynolds number of 2,000,000. Comparisons of the distribution of pressure coefficient at four semispan stations of the wing for the wing-fuselage combination without fences, with three fences, and with four fences are presented in figure 6 for a Mach number of 0.25 and a Reynolds number of 2,000,000.

Diagrams showing lines of constant pressure and approximate areas of separated flow on the upper surface of the wing for the wing-fuselage combination without fences, with three fences, and with four fences are compared in figures 7 through 10. The Mach numbers and Reynolds numbers for the data shown are the same as for the data of figures 3, 4, and 5. In all cases the diagrams are presented for angle-of-attack ranges beginning where the force and moment data were affected by fences.

The section normal-force and section pitching-moment characteristics at nine semispan stations of the wing are presented in figures 11 through 17 together with the total lift, drag, and pitching-moment characteristics obtained from reference 1. These results are shown for the wing with and without fences for Mach numbers of 0.165 and 0.25 at a Reynolds number of 8,000,000, and for Mach numbers from 0.25 to 0.90 at a Reynolds number of 2,000,000.

The effects of an increase in Reynolds number from 2,000,000 to 8,000,000 on the section characteristics and total force and moment characteristics of the wing-fuselage combination without fences and with four fences are shown in figures 18 and 19, respectively. A summary plot showing the effect of Mach number on the section normal-force coefficients of the wing-fuselage combination without fences is presented in figure 20.

Comparisons of the experimental and theoretical spanwise distributions of loading coefficient for the wing alone and for the wing-fuselage combination are presented in figures 21 and 22, respectively. The effect of fences on the span loading is shown in figure 23.

A portion of the lift, drag, and pitching-moment data at Mach numbers of 0.86 and 0.90 (figs. 16(a) and 17(a)) have been faired with a dotted line to indicate data obtained under conditions in which the wind tunnel may have been partially choked. It is to be understood that the corresponding pressure data falls under the same limitations of reliability.

DISCUSSION

Pressure Distribution and Flow Separation

Wing-fuselage combination.- It can be seen in the pressure distributions of figures 3, 4, and 5 that at Mach numbers of 0.25, 0.80, and 0.90, the minimum pressure coefficient occurred near the midsemispan of the wing for lift coefficients ranging from low to moderately high values. The pressure distributions also show that trailing-edge flow separation (as indicated by the reduction in pressure recovery at the trailing edge) first occurred near the midsemispan. The appearance of this turbulent separation at the midsemispan before it appeared at the wing tip was probably due to the variations of twist and thickness ratio along the semispan. (See fig. 1(b).) As is indicated in the diagrams shown in figures 7 through 10, this separation¹ spread toward both the root and the tip with further increase in angle of attack.

Increasing the Reynolds number from 2,000,000 to 8,000,000 at a Mach number of 0.25 (figs. 3, 7, and 8) reduced the amount of trailing-edge flow separation at all angles of attack and delayed to higher angles of attack complete separation of the flow over the outer sections. The results of these favorable changes in the flow characteristics with increasing Reynolds number are evident in the total lift, drag, and pitching-moment data of figure 18(a).

¹The indicated areas of separated flow on the wing are only approximate and are based on the pressure-recovery characteristics near the trailing edge. The separation point was arbitrarily chosen 0.05 c to the rear of the point where the chordwise pressure distribution departed from that which would be expected on the basis of inviscid airfoil theory. A comparison of the isobar diagrams with the tuft photographs in reference 1 indicates that this criterion provides a reasonably accurate estimate of the extent of turbulent separation.

Effect of fences.- From the isobar diagrams in figures 7 through 10, it is seen that the fences had little effect on the pressure contours² until trailing-edge flow separation appeared. The general effect of both the small and the extended fences was to reduce the amount of flow separation immediately outboard of each fence. The improvement in the total lift, drag, and pitching-moment characteristics of the wing due to fences may be seen in figures 11(a) through 17(a).

An increase in the Reynolds number from 2,000,000 to 8,000,000 at a Mach number of 0.25 caused a substantial reduction in the area of separated flow for both the three- and four-fence configurations (cf. figs. 7 and 8).

It is interesting to note that at a Reynolds number of 2,000,000 and a Mach number of 0.25 a peculiar flow condition existed on the wing outboard of the small fences at the higher angles of attack. The pressure distributions of figures 6 and 8(c) indicate that, in several instances, a region of low pressure developed just outboard of the forward part of the small fences. It is reasoned that these low-pressure areas developed when the turbulent separation on the inboard side of the fence extended far enough forward to allow spanwise flow of air over the forward part of the fence. It appears, therefore, that, under these conditions, the small fences acted much the same as the vortex generators described in reference 6. Increasing the Reynolds number to 8,000,000 delayed the formation of this type of flow to higher angles of attack due to the reduction in the amount of separation.

At the higher Mach numbers (figs. 9 and 10), it is evident that the extended fences were somewhat more effective than the small fences in reducing the amount of separation. The relative ineffectiveness of the small fences was possibly a result of shock-induced separation occurring far enough forward of the trailing edge of the wing to allow spanwise flow around and over the fence. This condition may also have existed at the small inboard fence of the four-fence configuration, in which case an extended fence at this location would probably have improved still further the characteristics of the four-fence configuration.

²The fairing of the isobars between the fences is only approximate due to the limited number of semispan stations where the chordwise pressure distributions were measured. (See fig. 1(c).) However, it is believed that these contours are sufficiently accurate for a qualitative study of the effect of fences.

Section Characteristics

Wing and wing-fuselage combination.- It was indicated in reference 1 that significant losses in lift-curve slope for the wing alone and for the wing-fuselage combination occurred considerably before maximum lift. The section normal-force curves of figure 11 for a Mach number of 0.165 and a Reynolds number of 8,000,000 reveal that losses in section normal-force-curve slope occurred rather uniformly across the semispan. The data also show that the maximum section normal-force coefficients at the outer stations were considerably lower than those at stations farther inboard. As might be expected, the section normal-force data for a Mach number of 0.25 and a Reynolds number of 8,000,000 (fig. 12) are similar to those at a Mach number of 0.165. Reducing the Reynolds number from 8,000,000 to 2,000,000 at a Mach number of 0.25 (fig. 18) resulted in an earlier loss in section normal-force-curve slope at most sections and a reduction in the maximum section normal-force coefficients at the outer sections.

For Mach numbers from 0.60 to 0.90 at a Reynolds number of 2,000,000 (figs. 14 through 17), the section normal-force curves exhibit characteristics similar to those at a Mach number of 0.25 and a Reynolds number of 2,000,000, although at the higher Mach numbers the reductions in section normal-force-curve slope occurred at considerably lower angles of attack over the outer half of the semispan. The effects of Mach number on the section normal-force coefficients for the wing-fuselage combination are summarized in figure 20.

An inspection of the section pitching-moment data in figures 11 through 17 reveals that, at the higher section normal-force coefficients, a rearward movement of the centers of pressure occurred at most sections. The effects of these section center-of-pressure changes are not evident in the total pitching-moment curves and, therefore, it appears that the longitudinal stability of the wing was primarily governed by changes in the spanwise distribution of normal force.

Effect of fences.- The effect of the four fences on the characteristics of the wing alone at a Mach number of 0.165 and a Reynolds number of 8,000,000 (fig. 11) was to reduce the losses in the section normal-force-curve slopes and the changes in the section centers of pressure at most sections. The net result of these changes was an increase of about 16 percent in the maximum lift coefficient of the wing, a delay in the abrupt increase in drag to approximately the maximum lift coefficient, and an elimination of practically all of the longitudinal instability of the wing at the higher lift coefficients.

Similar effects of fences were obtained for the wing-fuselage combination at a Mach number of 0.25 and a Reynolds number of 8,000,000

(fig. 12). The data indicate substantially the same improvement in the section characteristics for either the three- or the four-fence configuration. At a Reynolds number of 2,000,000 (fig. 13), the effect of the fences on the section characteristics was more pronounced than at a Reynolds number of 8,000,000 since more extensive flow separation existed at the lower Reynolds number (cf. figs. 7 and 8).

In figure 14, it is shown that at a Mach number of 0.60 the improvement in the section characteristics due to fences was considerably less than at a Mach number of 0.25, the effectiveness of the four fences having been slightly greater than that of the three fences. As the Mach number was increased from 0.60 to 0.90 (figs. 14 through 17), the effectiveness of the four fences increased, whereas the effectiveness of the three fences remained about the same. An inspection of the section data in these figures reveals that the major differences between the beneficial effects provided by the two fence configurations occurred over the outer half of the semispan. These differences near the tip appear as increases in section lift and provide an explanation of the large improvement in the longitudinal stability characteristics with the use of four fences. For both fence configurations at these higher Mach numbers it is indicated that, with one exception, there were reductions in the maximum section normal-force coefficients at inboard stations 0.31 b/2 and 0.38 b/2.

In general, the section pitching-moment characteristics in figures 12 through 17 show no large changes with the addition of fences, apart from those associated with the increase in maximum section normal-force coefficient at some sections. Therefore, the large improvements in longitudinal stability can be attributed primarily to spanwise changes of the center of pressure.

Span Loading Characteristics

Wing and wing-fuselage combination. - A comparison is made in figure 21 of the experimental spanwise distribution of additional loading coefficient ($dc_L/dc_L(c/c_{av})$) for the wing alone at a Mach number of 0.165 and a Reynolds number of 8,000,000 with two theoretical span loadings computed by the methods of references 7 and 8. The experimental loading coefficients are based upon the slopes of the section normal-force curves measured at an angle of attack of 0°. It may be seen that the theoretical distribution of loading calculated by the modified Falkner 19 × 1 method of reference 7 is in good agreement with the experimental data for a Mach number of 0.165. However, the loading calculated by the Weissinger 7 × 1 method of reference 8 is shown to be too high over the outer portions of the wing span. This result is in agreement with that noted for a wing of similar plan form in reference 7.

In figure 22, it is shown that at Mach numbers of 0.25 and 0.80 good agreement was obtained between the experimental and theoretical distributions of additional loading coefficient for the wing-fuselage combination. The theoretical distribution was calculated by the modified Falkner 19 x 1 method with the fuselage effect treated in the manner described in reference 9.

Effect of fences.- Comparisons of theoretical loadings of $c_l(c/c_{av})$ (methods of references 7 and 9) with experimental loadings of $c_n(c/c_{av})$ for the wing-fuselage combination without fences, with three fences, and with four fences are presented in figure 23 for the same Mach numbers, Reynolds numbers, and angles of attack for which isobar diagrams are given in figures 7 through 10. For the purpose of this comparison, no distinction has been made between the theoretical values of section lift coefficient and the experimental values of section normal-force coefficient. The theoretical data are based on the lift coefficients of the wing-fuselage combination without fences obtained from the force data. Inasmuch as the fairing of the loading near each fence is indefinite, no attempt has been made to fair curves through the experimental values of $c_n(c/c_{av})$ computed from the pressure measurements at the nine semi-span stations of the wing with fences.

At a Mach number of 0.25 and a Reynolds number of 8,000,000, the effect of fences on the span loading was small up to an angle of attack of 14° . The effect of either fence configuration at higher angles of attack was to increase the loading at all stations outboard of 0.33 b/2. At a Reynolds number of 2,000,000 the fences affected the span loading at an angle of attack approximately 4° lower than at a Reynolds number of 8,000,000.

At Mach numbers of 0.80 and 0.90 the loading of the wing without fences is shown to have increased mainly at the inner stations with increasing angle of attack. With the addition of four fences, the loading at the outer stations was increased to some extent without any material alteration to the loading at the inner stations.

CONCLUDING REMARKS

The results of measurements of the surface pressures on a semispan model of a cambered and twisted, high-aspect-ratio, swept wing (alone and in combination with a fuselage) have been presented for several values of Mach number and Reynolds number. Data are included for two different fence configurations.

It was indicated that, for Mach numbers up to 0.90 at a Reynolds number of 2,000,000, initial separation of the flow occurred at the

trailing edge near the midsemispan of the wing. With continued increase in angle of attack the separation spread toward both the root and the tip, complete separation eventually occurring at the outer sections. Increasing the Reynolds number to 8,000,000 at low speed reduced the amount of flow separation over the wing and caused significant improvements in the lift, drag, and pitching-moment characteristics.

The use of upper-surface fences was found to be effective in producing significant increases in lift over the outer portions of the wing by reducing the amount of separation outboard of each of the fences and thereby causing substantial improvements in the lift, drag, and pitching-moment characteristics. At the higher Mach numbers, a four-fence configuration having extended fences was considerably more effective than a three-fence configuration of small fences.

The modified Falkner 19×1 method was found to predict the spanwise load distribution to a good degree of accuracy provided little flow separation existed on the wing.

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TABLE I.- FUSELAGE COORDINATES

Distance from nose (in.)	Radius (in.)
0	0
1.27	1.04
2.54	1.57
5.08	2.35
10.16	3.36
20.31	4.44
30.47	4.90
39.44	5.00
50.00	5.00
60.00	5.00
70.00	5.00
76.00	4.96
82.00	4.83
88.00	4.61
94.00	4.27
100.00	3.77
106.00	3.03
126.00	0

 NACA

TABLE II.- INDEX OF TABULATED PRESSURE COEFFICIENTS

Table No.	$R \times 10^{-6}$	M	Configuration	α_u range
III	8.0	0.165	Wing alone	-2° to 20°
IV	8.0	.165	Wing alone + 4 fences	
V	8.0	.25	Wing + fuselage	
VI	2.0	.25		
VII		.60		-4° to 18°
VIII		.80		
IX		.86		-4° to 16°
X	↓	.90	↓	-4° to 12°
XI	8.0	.25	Wing + fuselage + 4 fences	-4° to 17.5°
XII	2.0	.25		-2° to 20°
XIII		.60		-4° to 18°
XIV		.80		-4° to 16°
XV		.86		-4° to 14°
XVI	↓	.90	↓	-4° to 10°



TABLE III.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING.
 $M_\infty = 0.165$; $R = 8,000,000$
(a) α_u , $-2^\circ, 0^\circ, 2^\circ, 4^\circ, 6^\circ, 8^\circ$

Spanwise station	Per-cent chord	Upper surface						Lower surface						
		Angle of attack						Angle of attack						
		-2°	0°	2°	4°	6°	8°	-2°	0°	2°	4°	6°	8°	
0.10 b/2	0	0.23	0.46	0.54	0.54	0.42	0.16	---	0.58	-0.23	0.05	0.27	0.42	0.52
	1.5	.32	.14	-.09	-.37	-.67	-1.06	---	.53	-.30	-.09	.09	.24	.37
	4.0	.12	-.05	-.25	-.49	-.73	-.98	---	---	---	---	---	---	---
	7.0	-.01	-.16	-.33	-.50	-.69	-.90	---	---	---	---	---	---	---
	10.0	-.12	-.29	-.41	-.55	-.70	-.86	---	-.47	-.32	-.18	-.05	.07	.18
	15.0	-.18	-.30	-.43	-.55	-.67	-.80	---	-.41	-.29	-.18	-.06	.02	.12
	20.0	-.24	-.33	-.46	-.55	-.65	-.77	---	-.33	-.24	-.14	-.06	.03	.11
	30.0	-.26	-.34	-.41	-.50	-.58	-.65	---	-.25	-.18	-.11	-.01	.02	.08
	40.0	-.25	-.31	-.37	-.43	-.49	-.55	---	-.18	-.13	-.07	-.02	.03	.08
	50.0	-.19	-.24	-.29	-.33	-.38	-.42	---	-.11	-.08	-.04	0	.04	.09
	60.0	-.19	-.23	-.26	-.29	-.33	-.35	---	-.06	-.03	-.01	.03	.06	.16
	70.0	-.16	-.19	-.22	-.24	-.26	-.28	---	-.01	-.01	.04	.06	.09	.12
0.19 b/2	0	.19	.45	.54	.51	.29	-.10	---	-.26	-.19	-.11	.34	.51	---
	1.5	.33	.10	-.19	-.36	-.66	-1.02	---	.54	-.27	-.09	.14	.31	.43
	4.0	.03	-.18	-.42	-.67	-.98	-1.33	---	---	---	---	---	---	---
	7.0	0	-.18	-.37	-.56	-.78	-1.02	---	---	---	---	---	---	---
	10.0	-.09	-.24	-.41	-.58	-.73	-.93	---	-.43	-.27	-.12	.02	.14	.23
	15.0	-.18	-.31	-.46	-.59	-.70	-.89	---	-.37	-.25	-.13	.03	.09	.18
	20.0	-.15	-.26	-.37	-.48	-.59	-.71	---	-.31	-.23	-.11	.05	.07	.15
	30.0	-.22	-.30	-.41	-.48	-.56	-.64	---	-.24	-.16	-.09	0	.03	.11
	40.0	-.03	-.32	-.38	-.45	-.51	-.57	---	-.16	-.11	-.03	0	.03	.10
	50.0	-.28	-.26	-.30	-.35	-.40	-.44	---	---	---	---	---	---	---
	60.0	-.17	-.23	-.29	-.36	-.41	-.44	---	0	-.08	.02	.05	.07	.11
	70.0	-.15	-.18	-.21	-.23	-.29	-.33	---	0	-.08	.02	.06	.10	.12
0.31 b/2	0	.11	-.13	-.14	-.15	-.16	-.15	---	---	---	---	---	---	---
	1.5	-.01	-.02	-.02	-.02	-.02	-.01	---	0.06	-.07	.09	.09	.10	.11
	4.0	-.06	-.05	-.06	-.05	-.05	-.05	---	0.07	-.07	.07	0.08	.08	.08
	7.0	0	-.05	-.05	-.05	-.05	-.05	---	0.09	-.09	.09	.09	.10	.10
	10.0	-.07	-.22	-.41	-.59	-.80	-1.01	---	-.14	-.27	-.10	.04	.17	.28
	15.0	-.13	-.27	-.43	-.57	-.73	-.89	---	-.39	-.26	-.12	.01	.16	.26
	20.0	-.17	-.28	-.41	-.52	-.62	-.78	---	-.32	-.20	-.10	.01	.06	.17
	30.0	-.20	-.26	-.37	-.49	-.55	-.63	---	-.23	-.16	-.08	.01	.06	.13
	40.0	-.22	-.26	-.35	-.48	-.56	-.65	---	-.16	-.11	-.07	0	.06	.12
	50.0	-.21	-.26	-.32	-.37	-.42	-.46	---	-.10	-.05	-.01	.03	.07	.11
	60.0	-.17	-.22	-.25	-.29	-.32	-.35	---	0.01	-.03	-.03	0	.06	---
	70.0	-.15	-.18	-.20	-.22	-.25	-.26	---	0.01	-.03	-.03	0.06	.10	.13
0.375 b/2	0	-.11	-.09	-.14	-.15	-.16	-.16	---	0.01	-.01	0.07	0.08	.10	---
	1.5	-.01	-.01	-.02	-.02	-.02	-.02	---	0.07	-.07	0.08	0.09	.10	---
	4.0	-.06	-.05	-.05	-.05	-.05	-.05	---	0.09	-.09	0.09	0.09	.10	---
	7.0	0	-.05	-.05	-.05	-.05	-.05	---	0.09	-.09	0.09	0.09	.10	---
	10.0	-.02	-.24	-.43	-.50	-.61	-.73	---	-.45	-.27	-.09	0.03	.18	.29
	15.0	-.13	-.27	-.43	-.58	-.73	-.91	---	-.38	-.24	-.11	0.01	.12	.22
	20.0	-.17	-.28	-.41	-.55	-.66	-.80	---	-.32	-.20	-.10	0	.09	.15
	30.0	-.13	-.21	-.32	-.39	-.49	-.58	---	-.23	-.15	-.07	0	.07	.14
	40.0	-.20	-.28	-.35	-.42	-.49	-.56	---	0	-.04	0.01	0	.07	.12
	50.0	-.18	-.23	-.29	-.35	-.40	-.44	---	0	-.03	0.01	0	.06	---
	60.0	-.16	-.20	-.23	-.28	-.32	-.35	---	0.03	-.01	0.02	0	.06	---
	70.0	-.14	-.17	-.20	-.22	-.25	-.26	---	0.01	0.03	0.03	0.08	.10	.13
0.44 b/2	0	-.10	-.12	-.13	-.15	-.15	-.15	---	0.01	0.07	0.08	0.09	.10	---
	1.5	-.08	-.14	-.24	-.29	-.39	-.41	---	0.01	0.07	0.08	0.09	.10	---
	4.0	.18	-.05	-.17	-.63	-.82	-.94	---	0.03	0.35	0.07	0.35	.33	---
	7.0	.04	-.18	-.41	-.63	-.89	-.97	---	0	0	0	0	0	---
	10.0	-.04	-.21	-.43	-.60	-.81	-.95	---	0.06	0.29	0.10	0.36	.30	---
	15.0	-.12	-.25	-.41	-.56	-.73	-.91	---	0.04	0.25	0.11	0.36	.22	---
	20.0	-.15	-.27	-.40	-.55	-.66	-.80	---	0.02	0.20	0.10	0.36	.18	---
	30.0	-.19	-.29	-.38	-.48	-.58	-.68	---	0.03	0.15	0.07	0.37	.14	---
	40.0	-.17	-.26	-.34	-.41	-.49	-.55	---	0.01	0.11	0.06	0.36	.11	---
	50.0	-.17	-.21	-.28	-.34	-.40	-.45	---	0.03	0.09	0.05	0.36	.12	---
	60.0	-.16	-.20	-.23	-.29	-.33	-.38	---	0.05	0.04	0.02	0.36	.08	---
	70.0	-.14	-.17	-.20	-.23	-.25	-.28	---	0.01	0.04	0.02	0.36	.11	---
	80.0	-.10	-.12	-.14	-.15	-.16	-.16	---	0.06	0.07	0.08	0.09	.10	---
	90.0	0	-.01	-.02	-.02	-.02	-.02	---	0.09	0.09	0.09	0.09	.10	---
	95.0	.06	-.06	-.06	-.06	-.06	-.06	---	0.09	0.09	0.09	0.09	.10	---

NACA

TABLE III.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING.
 $M_\infty = 0.165$; $R = 8,000,000$ - Continued
(a) $\alpha_{u_1} = -2^\circ, 0^\circ, 2^\circ, 4^\circ, 6^\circ, 8^\circ$ - Concluded

Spanwise station	Percent chord	Upper surface						Lower surface					
		Angle of attack						Angle of attack					
		-2°	0°	2°	4°	6°	8°	-2°	0°	2°	4°	6°	8°
0.56 b/2	0	-0.02	0.28	0.53	0.45	0.11	-0.50	---	---	0.08	0.36	0.52	0.56
	1.5	.41	.19	-.16	-.60	-1.12	-1.76	-0.89	-0.34	0.05	0.17	.35	.46
	4.0	.30	-.03	-.31	-.62	-.94	-.34	-.67	-.37	-.05	0.17	0.35	0.46
	7.0	.07	-.13	-.37	-.61	-.89	-1.19	---	---	---	0.05	0.18	0.30
	10.0	-.02	-.19	-.41	-.60	-.83	-1.08	-.49	-.33	-.11	0.05	0.18	0.30
	15.0	-.09	-.22	-.40	-.56	-.73	-.91	-.42	-.27	-.12	0	0.11	0.22
	20.0	-.12	-.24	-.37	-.52	-.64	-.77	-.33	-.20	-.10	0	0.10	0.19
	30.0	-.15	-.24	-.33	-.42	-.50	-.61	-.24	-.16	-.08	-.01	0.07	0.14
	40.0	-.17	-.23	-.32	-.40	-.48	-.55	-.16	-.10	-.04	0.01	0.07	0.13
	50.0	-.17	-.23	-.29	-.35	-.40	-.45	-.10	-.06	-.01	0.03	0.07	0.12
	60.0	-.14	-.19	-.23	-.28	-.31	-.35	---	---	---	0	0.10	0.20
	70.0	-.13	-.16	-.19	-.22	-.24	-.26	0	0.03	0.06	0.08	0.10	0.13
	80.0	-.09	-.11	-.13	-.15	-.16	-.19	0.05	0.06	0.08	0.09	0.11	0.13
	90.0	-.01	-.01	-.02	-.02	-.02	-.01	0.07	0.08	0.09	0.09	0.10	0.10
	95.0	.06	.06	.06	.06	.06	.05	0.10	0.09	0.10	0.10	0.10	0.10
0.68 b/2	0	---	---	---	---	---	---	---	---	0.46	0.08	0.29	0.48
	1.5	-.48	.31	-.03	-.42	-.93	-1.35	-.04	0.46	0.08	0.29	0.48	0.54
	4.0	.24	0	-.27	-.60	-.95	-1.31	-.61	-.43	0.11	0.31	0.45	0.55
	7.0	.12	-.07	-.31	-.57	-.86	-1.13	---	---	0.03	0.17	0.38	0.55
	10.0	.03	-.16	-.37	-.55	-.78	-1.02	-.53	-.32	-.13	0.03	0.11	0.21
	15.0	-.03	-.18	-.33	-.50	-.67	-.86	-.44	-.29	-.14	0.01	0.11	0.18
	20.0	-.09	-.21	-.33	-.49	-.61	-.77	-.35	-.23	-.11	0.01	0.09	0.14
	30.0	-.13	-.23	-.33	-.44	-.54	-.65	-.25	-.16	-.08	0.01	0.07	0.12
	40.0	-.14	-.22	-.30	-.35	-.46	-.53	-.17	-.11	-.04	0.01	0.06	0.12
	50.0	-.14	-.20	-.27	-.33	-.38	-.44	---	---	---	0	0.08	0.12
	60.0	-.12	-.17	-.25	-.26	-.30	-.34	0.03	0.02	0.03	0.06	0.08	0.12
	70.0	-.11	-.15	-.18	-.22	-.24	-.26	0.01	0.01	0.04	0.06	0.09	0.11
	80.0	-.08	-.11	-.13	-.15	-.16	-.16	0.04	0.05	0.06	0.08	0.10	0.12
	90.0	-.01	-.01	-.01	-.02	-.02	-.01	0.07	0.07	0.08	0.09	0.10	0.10
	95.0	.05	.05	.04	.05	.04	.04	0.08	0.08	0.09	0.09	0.09	0.10
0.80 b/2	0	-.13	.34	.56	.53	.19	-.45	---	---	0.12	.25	.45	.56
	1.5	.49	.15	0	-.41	-.91	-1.52	-.126	-.62	0.12	0.25	0.42	0.56
	4.0	.29	.09	-.18	-.49	-.82	-1.16	-.83	-.53	0.19	.08	.27	.42
	7.0	.16	-.03	-.24	-.50	-.73	-1.03	---	---	0.01	.14	.26	.36
	10.0	.09	-.09	-.30	-.49	-.70	-.95	-.60	-.37	-.19	0.04	.09	.19
	15.0	.01	-.14	-.30	-.46	-.64	-.82	-.48	-.32	-.17	0.02	.08	.16
	20.0	-.04	-.16	-.30	-.43	-.57	-.72	-.37	-.25	-.13	0.02	.05	.12
	30.0	-.07	-.18	-.27	-.35	-.45	-.56	-.27	-.19	-.10	0.02	.05	.12
	40.0	-.11	-.19	-.27	-.33	-.43	-.50	---	---	0	0.02	.06	0.10
	50.0	-.12	-.18	-.24	-.31	-.36	-.42	-.12	-.08	-.03	0.02	.06	0.10
	60.0	-.11	-.15	-.21	-.28	-.39	-.43	0.06	0.03	0.01	0.04	.06	0.10
	70.0	-.09	-.13	-.13	-.21	-.23	-.25	0.01	0.01	0.04	0.06	.09	0.11
	80.0	-.07	-.09	-.12	-.14	-.15	-.15	0.02	0.04	0.05	0.07	.08	0.10
	90.0	-.01	0	-.01	-.02	-.02	-.02	0.07	0.07	0.08	0.09	0.09	0.10
	95.0	.06	.06	.05	.05	.04	.04	0.09	0.09	0.10	0.11	.10	.10
0.94 b/2	0	-.77	-.02	.42	.56	.46	.08	---	---	0.08	.36	.53	0.53
	1.5	.51	.26	.16	.18	.39	-.113	-.169	-.93	-.37	0	0.08	0.16
	4.0	.34	.18	-.03	-.33	-.64	-1.00	---	---	0	0.05	.13	.25
	7.0	.21	.04	-.15	-.36	-.63	-.86	-.75	-.49	-.26	0.05	.09	.21
	10.0	.12	-.01	-.19	-.38	-.56	-.77	-.62	-.43	-.27	0.08	.12	.22
	15.0	.06	-.06	-.20	-.33	-.49	-.82	-.50	-.36	-.22	0.09	.08	.18
	20.0	.03	-.06	-.19	-.31	-.43	-.56	-.38	-.28	-.17	0.07	.02	.10
	30.0	-.01	-.09	-.16	-.21	-.29	-.41	-.27	-.19	-.12	0.05	.01	.07
	40.0	-.08	-.14	-.22	-.26	-.34	-.41	-.17	-.12	-.07	0.03	.01	.05
	50.0	-.11	-.15	-.21	-.23	-.30	-.34	-.09	-.06	-.03	0	0.03	.06
	60.0	-.10	-.14	-.17	-.22	-.24	-.24	-.07	---	---	0	0.03	.06
	70.0	-.09	-.11	-.13	-.16	-.18	-.21	0.01	0.02	0.03	0.04	.05	.06
	80.0	-.06	-.07	-.08	-.10	-.12	-.13	0.05	0.05	0.06	0.06	.06	.06
	90.0	-.02	.02	.01	.01	0	0	0.07	0.07	0.07	0.07	.07	.06
	95.0	.02	.06	.06	.06	.05	.05	0.10	0.10	0.10	0.09	.09	.08

NACA

TABLE III.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING.
 $M_\infty = 0.165$; $R = 8,000,000$ - Continued

(b) α_u , $10^\circ, 12^\circ, 14^\circ, 16^\circ, 18^\circ, 20^\circ$

Spanwise station	Percent chord	Upper surface						Lower surface					
		Angle of attack						Angle of attack					
		10°	12°	14°	16°	18°	20°	10°	12°	14°	16°	18°	20°
0.10 b/2	0	-0.23	-0.78	-1.41	-2.14	-2.95	-3.91	---	---	0.48	0.36	0.20	0.01
	1.5	-1.45	-1.93	-2.43	-2.94	-3.32	-4.12	0.37	0.55	0.48	0.36	0.20	0.01
	4.0	-1.27	-1.99	-2.29	-2.61	-2.99	-3.47	0.28	0.55	0.48	0.36	0.20	0.01
	7.0	-1.11	-1.36	-1.99	-1.83	-2.07	-2.35	0.21	0.29	0.37	0.47	0.51	0.55
	10.0	-1.04	-1.23	-1.41	-1.59	-1.77	-1.99	0.19	0.26	0.33	0.39	0.45	0.51
	15.0	-0.93	-1.06	-1.19	-1.32	-1.46	-1.61	0.15	0.21	0.27	0.33	0.38	0.43
	20.0	-0.86	-0.98	-1.08	-1.17	-1.27	-1.40	0.13	0.18	0.22	0.29	0.34	0.38
	30.0	-0.72	-0.80	-0.87	-0.93	-1.00	-1.07	0.12	0.14	0.18	0.21	0.24	0.27
	40.0	-0.60	-0.65	-0.70	-0.74	-0.79	-0.83	0.11	0.14	0.16	0.17	0.19	0.21
	50.0	-0.46	-0.49	-0.53	-0.56	-0.59	-0.62	0.11	0.12	0.13	0.15	0.16	0.16
	60.0	-0.38	-0.40	-0.43	-0.44	-0.46	-0.48	0.11	0.12	0.13	0.14	0.15	0.16
	70.0	-0.29	-0.30	-0.31	-0.32	-0.33	-0.34	0.11	0.12	0.13	0.14	0.15	0.16
	80.0	-0.18	-0.18	-0.18	-0.19	-0.19	-0.19	0.11	0.12	0.13	0.14	0.15	0.16
	90.0	-0.02	-0.02	-0.03	-0.04	-0.05	0.01	0.11	0.12	0.13	0.14	0.15	0.16
	95.0	.03	.04	.04	.03	.02	.01	0.11	0.12	0.13	0.14	0.15	0.16
0.19 b/2	0	-.65	-1.36	-2.21	-3.19	-4.36	-5.32	---	---	0.36	0.35	0.34	0.33
	1.5	-2.11	-2.80	-3.52	-4.26	-5.03	-5.92	0.63	0.49	0.36	0.35	0.34	0.33
	4.0	-1.67	-2.07	-2.47	-2.88	-3.29	-3.75	0.58	0.58	0.58	0.58	0.58	0.58
	7.0	-1.27	-1.54	-1.81	-2.11	-2.39	-2.71	0.35	0.30	0.30	0.33	0.33	0.33
	10.0	-1.16	-1.38	-1.60	-1.83	-2.05	-2.30	0.27	0.35	0.42	0.48	0.53	0.58
	15.0	-1.04	-1.21	-1.37	-1.52	-1.68	-1.86	0.23	0.30	0.37	0.43	0.48	0.53
	20.0	-0.83	-0.97	-1.10	-1.20	-1.34	-1.46	0.19	0.24	0.29	0.35	0.40	0.45
	30.0	-0.72	-0.81	-0.88	-0.96	-1.02	-1.11	0.17	0.21	0.26	0.30	0.35	0.39
	40.0	-0.63	-0.69	-0.73	-0.78	-0.82	-0.86	0.16	0.18	0.22	0.28	0.31	0.36
	50.0	-0.48	-0.51	-0.54	-0.56	-0.59	-0.61	0.15	0.18	0.20	0.23	0.26	0.30
	60.0	-0.36	-0.38	-0.40	-0.41	-0.41	-0.43	0.15	0.18	0.22	0.25	0.28	0.31
	70.0	-0.27	-0.27	-0.27	-0.26	-0.26	-0.28	0.15	0.18	0.20	0.23	0.26	0.29
	80.0	-0.15	-0.14	-0.13	-0.12	-0.13	-0.17	0.12	0.13	0.15	0.15	0.17	0.17
	90.0	-0.01	-0.01	-0.01	-0.04	-0.07	0.01	0.12	0.14	0.15	0.15	0.16	0.16
	95.0	.03	.03	.01	.02	.02	.00	0.08	0.08	0.08	0.08	0.08	0.08
0.31 b/2	0	-.84	-1.68	-2.66	-3.77	-5.03	-6.47	---	---	0.21	0.21	0.21	0.21
	1.5	-1.77	-2.77	-3.50	-4.26	-5.08	-6.00	0.53	0.41	0.37	0.37	0.37	0.37
	4.0	-2.38	-2.38	-2.53	-2.98	-3.56	-3.96	0.55	0.58	0.58	0.58	0.58	0.58
	7.0	-1.42	-1.72	-2.03	-2.35	-2.66	-3.01	0.38	0.46	0.52	0.56	0.59	0.61
	10.0	-1.24	-1.49	-1.72	-1.92	-2.20	-2.44	0.36	0.42	0.49	0.54	0.58	0.62
	15.0	-1.07	-1.25	-1.44	-1.58	-1.73	-1.93	0.29	0.37	0.44	0.49	0.54	0.58
	20.0	-0.92	-1.06	-1.18	-1.31	-1.43	-1.55	0.25	0.32	0.39	0.44	0.49	0.53
	30.0	-0.69	-0.78	-0.88	-0.96	-1.02	-1.08	0.19	0.25	0.30	0.36	0.40	0.45
	40.0	-0.61	-0.63	-0.72	-0.75	-0.78	-0.79	0.17	0.22	0.26	0.30	0.34	0.38
	50.0	-0.50	-0.53	-0.55	-0.56	-0.59	-0.58	0.16	0.19	0.23	0.27	0.30	0.33
	60.0	-0.37	-0.39	-0.39	-0.37	-0.35	-0.36	0.16	0.17	0.20	0.22	0.24	0.25
	70.0	-0.27	-0.26	-0.26	-0.22	-0.22	-0.27	0.16	0.17	0.20	0.22	0.24	0.25
	80.0	-0.15	-0.13	-0.11	-0.10	-0.15	-0.23	0.11	0.11	0.12	0.11	0.11	0.09
	90.0	0	-0.01	-0.03	-0.05	-0.13	-0.29	0.10	0.09	0.09	0.07	0.06	0.04
	95.0	.04	.02	-.01	-.02	-.14	-.27	0.10	0.09	0.09	0.07	0.06	0.04
0.375 b/2	0	-1.30	-1.94	-3.00	-4.22	-5.59	-7.44	---	---	0.17	0.12	0.16	0.16
	1.5	-2.39	-3.13	-3.93	-4.76	-5.62	-6.56	0.55	0.38	0.37	0.32	0.34	0.34
	4.0	-1.67	-2.12	-2.54	-3.01	-3.48	-3.96	0.57	0.58	0.57	0.52	0.54	0.54
	7.0	-1.44	-1.76	-2.06	-2.39	-2.70	-3.03	0.42	0.47	0.53	0.59	0.61	0.61
	10.0	-1.27	-1.53	-1.77	-2.01	-2.25	-2.48	0.30	0.38	0.45	0.50	0.54	0.58
	15.0	-1.08	-1.26	-1.44	-1.61	-1.76	-1.92	0.24	0.30	0.36	0.41	0.46	0.50
	20.0	-0.95	-1.09	-1.21	-1.33	-1.44	-1.53	0.20	0.26	0.31	0.36	0.40	0.45
	30.0	-0.69	-0.78	-0.85	-0.91	-0.96	-1.00	0.16	0.22	0.27	0.31	0.36	0.40
	40.0	-0.53	-0.67	-0.72	-0.74	-0.74	-0.71	0.16	0.22	0.27	0.31	0.34	0.38
	50.0	-0.41	-0.52	-0.53	-0.53	-0.49	-0.47	0.16	0.20	0.24	0.28	0.32	0.36
	60.0	-0.30	-0.36	-0.36	-0.35	-0.31	-0.36	0.16	0.18	0.21	0.24	0.26	0.28
	70.0	-0.20	-0.26	-0.23	-0.19	-0.21	-0.22	0.16	0.17	0.19	0.21	0.23	0.24
	80.0	-0.08	-0.12	-0.10	-0.10	-0.17	-0.30	0.16	0.12	0.11	0.07	0.09	0.08
	90.0	.06	-.01	-.03	-.08	-.17	-.35	0.15	0.09	0.07	0.06	0.03	0.04
	95.0	.09	.01	-.03	-.10	-.22	-.41	0.14	0.09	0.07	0.05	0.01	0.04
0.44 b/2	0	-1.02	-1.93	-3.03	-4.24	-5.56	-7.03	---	---	0.10	0.23	0.52	-1.04
	1.5	-2.33	-3.05	-3.83	-4.60	-5.50	-6.23	0.58	0.58	0.57	0.53	0.56	0.56
	4.0	-1.72	-2.17	-2.61	-3.03	-3.49	-3.95	0.55	0.58	0.58	0.54	0.56	0.56
	7.0	-1.48	-1.82	-2.13	-2.45	-2.73	-3.08	0.42	0.47	0.52	0.56	0.59	0.58
	10.0	-1.30	-1.58	-1.81	-2.04	-2.25	-2.46	0.35	0.38	0.45	0.50	0.54	0.58
	15.0	-1.11	-1.28	-1.45	-1.61	-1.74	-1.86	0.25	0.33	0.39	0.44	0.49	0.53
	20.0	-0.95	-1.09	-1.21	-1.33	-1.41	-1.46	0.20	0.25	0.31	0.36	0.43	0.44
	30.0	-0.68	-0.86	-0.94	-0.98	-1.00	-1.06	0.15	0.20	0.26	0.32	0.33	0.37
	40.0	-0.53	-0.67	-0.71	-0.72	-0.69	-0.61	0.15	0.21	0.26	0.32	0.36	0.38
	50.0	-0.41	-0.52	-0.53	-0.50	-0.44	-0.45	0.15	0.20	0.24	0.27	0.29	0.32
	60.0	-0.30	-0.38	-0.37	-0.38	-0.28	-0.40	0.15	0.18	0.21	0.23	0.25	0.27
	70.0	-0.20	-0.23	-0.21	-0.18	-0.22	-0.39	0.15	0.18	0.20	0.21	0.22	0.23
	80.0	-0.08	-0.12	-0.10	-0.11	-0.20	-0.40	0.15	0.11	0.10	0.09	0.07	0.04
	90.0	.03	-0.01	-0.04	-0.09	-0.21	-0.45	0.14	0.09	0.07	0.05	0.01	-0.04
	95.0	.09	.01	-.03	-.10	-.22	-.41	0.14	0.09	0.07	0.05	0.01	0.04

TABLE III.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING.
 $M_\infty = 0.165$; $R = 8,000,000$ - Concluded
 (b) $\alpha_u = 10^\circ, 12^\circ, 14^\circ, 16^\circ, 18^\circ, 20^\circ$ - Concluded

Spanwise station	Percent chord	Upper surface						Lower surface					
		Angle of attack						Angle of attack					
		10°	12°	14°	16°	18°	20°	10°	12°	14°	16°	18°	20°
0.56 b/2	0	-1.34	-2.41	-3.61	-4.90	-6.17	-7.38	----	----	----	----	----	----
	1.5	-2.46	-3.26	-4.05	-4.84	-5.55	-6.09	0.51	0.34	0.07	-0.24	-0.60	-0.92
	4.0	-1.77	-2.25	-2.66	-3.11	-3.48	-3.72	.57	.58	.58	.53	.47	.42
	7.0	-1.52	-1.95	-2.17	-2.46	-2.69	-2.77	----	----	----	----	----	----
	10.0	-1.33	-1.59	-1.84	-2.04	-2.21	-2.21	.43	.47	.53	.56	.59	.61
	15.0	-1.10	-1.29	-1.46	-1.59	-1.68	-1.53	.33	.38	.45	.50	.53	.57
	20.0	-.92	-1.06	-1.19	-1.27	-1.29	-1.14	.31	.34	.39	.44	.48	.52
	30.0	-.74	-.81	-.87	-.93	-.88	-.71	.23	.26	.31	.35	.39	.42
	40.0	-.51	-.57	-.70	-.68	-.57	-.64	.22	.22	.26	.30	.32	.35
	50.0	-.41	-.52	-.53	-.47	-.36	-.60	.20	.19	.22	.25	.27	.29
	60.0	-.30	-.38	-.36	-.26	-.26	-.56	----	----	----	----	----	----
	70.0	-.20	-.25	-.21	-.17	-.26	-.57	.20	.17	.19	.20	.19	.19
0.68 b/2	0	----	----	----	----	----	----	----	----	----	----	----	----
	1.5	-2.23	-2.96	-3.64	-4.34	-4.75	-5.01	----	----	----	----	----	----
	4.0	-1.74	-2.22	-2.66	-3.04	-3.24	-3.81	.56	.57	.57	.55	.50	.42
	7.0	-1.45	-1.79	-2.09	-2.34	-2.44	-2.21	----	----	----	----	----	----
	10.0	-1.27	-1.54	-1.77	-1.95	-1.99	-1.12	.39	.46	----	.55	.58	.61
	15.0	-1.05	-1.25	-1.41	-1.32	-1.49	-.99	.30	.38	----	.48	.52	.54
	20.0	-.91	-1.09	-1.19	-1.27	-1.18	-.95	.26	.32	----	.43	.46	.48
	30.0	-.75	-.84	----	-.90	-.71	-.94	.20	.26	----	.34	.37	.38
	40.0	-.60	-.66	----	-.64	-.44	-.100	.17	.22	----	.26	.30	.30
	50.0	-.49	-.51	----	-.43	-.35	-.101	----	----	----	.21	.21	----
	60.0	-.38	-.38	----	-.29	-.33	-.101	.15	.17	----	.17	.15	.18
	70.0	-.27	-.25	----	-.16	-.32	-.94	.13	.15	----	.13	.10	.03
0.80 b/2	0	-.15	-.13	----	-.13	-.32	-.85	.13	.14	----	.07	.01	-.06
	1.5	-.01	-.01	----	-.12	-.34	-.64	.11	.11	----	.07	-.08	-.20
	4.0	-.03	-.01	----	-.13	-.36	-.56	.08	.07	----	.01	-.08	-.20
	7.0	-.60	-2.48	-3.74	-5.54	-5.53	-2.29	----	----	----	----	----	----
	10.0	-2.23	-2.93	-3.56	-4.16	-4.19	-4.46	.55	.44	.27	.05	-.05	.38
	15.0	-1.59	-2.04	-2.46	-2.78	-2.72	-5.4	.53	.55	.58	.55	.61	----
	20.0	-1.34	-1.68	-1.97	-2.18	-2.05	-4.49	----	----	----	----	----	----
	30.0	-1.20	-1.47	-1.69	-1.83	-1.65	-4.46	.38	.43	.50	.53	.54	.55
	40.0	-1.02	-1.21	-1.35	-1.73	-1.49	-4.46	.28	.36	.46	.49	.44	----
	50.0	-.86	-1.02	-1.13	-1.17	-0.83	-4.45	.24	.31	----	.41	.43	.38
	60.0	-.66	-.76	-.82	-.82	-.55	-4.44	.22	.24	----	.32	.33	.29
	70.0	-.57	-.63	----	-.60	-.47	-.47	----	----	----	.22	----	----
0.94 b/2	0	-.47	-.50	----	-.40	-.43	-.46	----	----	----	----	----	----
	1.5	-.36	-.37	----	-.24	-.40	-.46	----	----	----	----	----	----
	4.0	-.26	-.26	----	-.15	-.40	-.45	----	----	----	----	----	----
	7.0	-.15	-.13	----	-.12	-.40	-.45	----	----	----	----	----	----
	10.0	-.02	-.02	----	-.11	-.41	-.42	.10	.10	----	.06	-.03	-.10
	15.0	-.04	-.02	----	-.12	-.38	-.42	.10	.09	----	.03	-.08	-.16
	20.0	-.60	-1.53	-2.62	-3.57	-2.42	-1.77	----	----	----	----	----	----
	30.0	-1.63	-2.79	-2.77	-3.22	-2.11	-1.58	.57	.52	.38	.22	.34	.44
	40.0	-1.38	-1.80	-2.21	-2.46	-1.46	-1.00	----	----	----	----	----	----
	7.0	-1.16	-1.46	-1.73	-1.90	-1.90	-4.49	----	----	----	----	----	----
	10.0	-1.00	-1.23	-1.43	-1.55	-1.63	-3.4	.32	.38	.45	.49	.50	.47
	15.0	-.82	-1.00	-1.13	-1.24	-1.49	-3.33	.21	.29	.38	.41	.39	.36
	20.0	-.71	-.84	-.94	-.99	-.44	-.33	.17	.24	----	.33	.32	.29
	30.0	-.51	-.60	-.65	-.68	-.40	-.31	.12	.17	----	.24	.23	.21
	40.0	-.47	-.52	----	-.51	-.41	-.32	.09	.14	----	.18	.16	.14
	50.0	-.38	-.42	----	-.36	-.38	-.31	.08	.11	----	.14	.12	.10
	60.0	-.30	-.32	----	-.22	-.37	-.30	----	----	----	----	----	----
	70.0	-.22	-.23	----	-.12	-.35	-.29	.07	.08	----	.08	.03	.02
	80.0	-.13	-.12	----	-.06	-.35	-.29	.07	.07	----	.05	-.02	-.03
	90.0	0	0	----	-.01	-.32	-.27	.06	.06	----	.02	-.09	-.10
	95.0	.05	.04	----	-.01	-.31	-.27	.07	.06	----	-.14	-.14	-.14

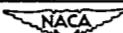


TABLE IV.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING.
 $M_\infty = 0.165$; $R = 8,000,000$
(a) $a_u, -2^\circ, 0^\circ, 2^\circ, 4^\circ, 6^\circ, 8^\circ$

Spanwise Station	Percent chord	Upper surface						Lower surface						
		Angle of attack						Angle of attack						
		-2°	0°	2°	4°	6°	8°	-2°	0°	2°	4°	6°	8°	
0.10 b/2	0	---	---	0.55	0.55	0.41	0.14	---	-0.56	-0.23	0.04	0.27	0.42	0.56
	1.5	---	---	-0.09	-0.38	-0.69	-1.06	---	-0.52	-0.30	-0.09	-0.09	-0.24	-0.36
	4.0	---	---	-0.26	-0.49	-0.74	-1.00	---	-0.40	-0.29	-0.19	-0.09	-0.02	-0.12
	7.0	---	---	-0.34	-0.52	-0.73	-0.93	---	-0.32	-0.23	-0.15	-0.06	-0.02	-0.11
	10.0	---	---	-0.41	-0.56	-0.73	-0.90	---	-0.24	-0.18	-0.12	-0.05	-0.02	-0.08
	15.0	---	---	-0.43	-0.55	-0.69	-0.86	---	-0.17	-0.12	-0.08	-0.02	-0.03	-0.08
	20.0	---	---	-0.46	-0.56	-0.69	-0.78	---	-0.12	-0.08	-0.04	-0.01	-0.04	-0.08
	30.0	-0.25	-0.33	-0.42	-0.50	-0.58	-0.66	---	-0.06	-0.03	0	0.04	0.07	0.10
	40.0	-0.24	-0.31	-0.37	-0.43	-0.49	-0.55	---	-0.01	-0.02	0.04	0.07	0.09	0.12
	50.0	-0.19	-0.24	-0.29	-0.33	-0.38	-0.43	---	-0.06	-0.07	0.07	0.09	0.10	0.11
	60.0	-0.18	-0.22	-0.26	-0.29	-0.33	-0.36	---	-0.06	-0.03	0	0.04	0.07	0.10
	70.0	-0.16	-0.19	-0.22	-0.24	-0.26	-0.28	---	-0.01	-0.02	0.04	0.07	0.09	0.12
	80.0	-0.12	-0.14	-0.16	-0.16	-0.18	-0.18	---	-0.06	-0.07	0.07	0.09	0.10	0.11
	90.0	-0.08	-0.03	-0.03	-0.03	-0.03	-0.03	---	-0.06	-0.06	0.06	0.09	0.09	0.10
	95.0	.06	.06	.05	.05	.05	.05	---	.08	.08	.08	.09	.09	.10
0.19 b/2	0	---	---	.53	.50	.49	.11	---	---	---	---	---	---	---
	1.5	---	---	-0.19	-0.59	-1.05	-1.57	---	-0.57	-0.20	.10	.34	.49	.56
	4.0	---	---	-0.41	-0.68	-1.00	-1.34	---	-0.53	-0.27	-.05	.15	.30	.43
	7.0	---	---	-0.36	-0.57	-0.79	-1.05	---	---	---	---	---	---	---
	10.0	---	---	-0.41	-0.59	-0.79	-0.96	---	-0.43	-0.27	-0.12	.08	.14	.25
	15.0	---	---	-0.46	-0.60	-0.74	-0.91	---	-0.37	-0.23	-0.13	-0.08	.06	.18
	20.0	---	---	-0.38	-0.49	-0.63	-0.74	---	-0.31	-0.21	-0.12	-0.08	.06	.15
	30.0	---	---	-0.41	-0.48	-0.58	-0.66	---	-0.23	-0.16	-0.09	-0.05	.05	.10
	40.0	-0.25	-0.31	-0.38	-0.45	-0.51	-0.58	---	-0.16	-0.11	-0.06	0	0.05	0.10
	50.0	-0.20	-0.29	-0.30	-0.35	-0.39	-0.44	---	---	---	---	---	---	---
	60.0	-0.17	-0.21	-0.25	-0.28	-0.31	-0.35	---	-0.05	-0.02	.01	.05	.06	.11
	70.0	-0.15	-0.18	-0.21	-0.23	-0.25	-0.27	---	.01	.03	.05	.07	.10	.12
	80.0	-0.10	-0.12	-0.14	-0.15	-0.16	-0.16	---	---	---	---	---	---	---
	90.0	-0.01	-0.06	-0.02	-0.08	-0.02	-0.02	---	.07	.07	.08	.09	.10	.10
	95.0	.06	.06	.05	.05	.06	.05	---	.07	.07	.07	.08	.08	.08
0.31 b/2	0	---	---	.55	.49	.24	-.23	---	---	---	---	---	---	---
	1.5	---	---	-0.13	-0.50	-0.96	-1.51	---	-0.63	-0.20	.12	.38	.52	.57
	4.0	---	---	-0.34	-0.62	-0.88	-1.32	---	-0.58	-0.29	-.03	.18	.35	.47
	7.0	---	---	-0.38	-0.62	-0.88	-1.15	---	---	---	---	---	---	---
	10.0	---	---	-0.41	-0.60	-0.82	-1.03	---	-0.44	-0.26	-0.10	.05	.17	.28
	15.0	---	---	-0.42	-0.58	-0.74	-0.96	---	-0.39	-0.25	-0.13	-.01	.09	.17
	20.0	---	---	-0.41	-0.53	-0.66	-0.80	---	-0.31	-0.20	-0.10	0	0.09	.13
	30.0	---	---	-0.38	-0.47	-0.57	-0.65	---	-0.23	-0.15	-0.08	-0.01	.01	.06
	40.0	-0.20	-0.28	-0.35	-0.42	-0.49	-0.56	---	-0.16	-0.10	-0.05	0.01	.06	.11
	50.0	-0.19	-0.26	-0.32	-0.37	-0.42	-0.47	---	-0.09	-0.03	0	.03	.08	.12
	60.0	-0.17	-0.21	-0.25	-0.29	-0.33	-0.36	---	---	---	---	---	---	---
	70.0	-0.15	-0.18	-0.21	-0.23	-0.25	-0.27	---	.01	.03	.05	.08	.10	.13
	80.0	-0.11	-0.12	-0.14	-0.15	-0.16	-0.16	---	---	---	---	---	---	---
	90.0	0	-0.01	-0.01	-0.01	-0.01	0	---	.07	.08	.08	.09	.10	.11
	95.0	.06	.06	.06	.06	.06	.06	---	.09	.09	.09	.10	.10	.10
0.375 b/2	0	---	---	.53	.48	.19	-.33	---	---	---	---	---	---	---
	1.5	---	---	-0.21	-0.63	-1.14	-1.73	---	-0.65	-0.32	-.06	.38	.52	.56
	4.0	---	---	-0.32	-0.59	-0.93	-1.31	---	-0.59	-0.32	-.13	.18	.35	.47
	7.0	---	---	-0.32	-0.62	-0.88	-1.18	---	---	---	---	---	---	---
	10.0	---	---	-0.34	-0.61	-0.83	-1.06	---	-0.45	-0.27	-.10	.05	.18	.29
	15.0	---	---	-0.38	-0.58	-0.74	-0.94	---	-0.39	-0.24	-.12	.01	.11	.21
	20.0	---	---	-0.35	-0.52	-0.69	-0.88	---	-0.32	-0.21	-.10	0	.09	.18
	30.0	---	---	-0.38	-0.41	-0.51	-0.60	---	-0.23	-0.15	-.08	0	.06	.13
	40.0	-0.20	-0.28	-0.35	-0.42	-0.50	-0.57	---	-0.16	-0.10	-.05	0.01	.06	.12
	50.0	-0.18	-0.24	-0.30	-0.35	-0.41	-0.46	---	---	---	---	---	---	---
	60.0	-0.17	-0.21	-0.25	-0.29	-0.33	-0.37	---	.05	-0.01	.02	.03	.06	.12
	70.0	-0.15	-0.18	-0.21	-0.24	-0.27	-0.29	---	.01	.03	.05	.08	.10	.13
	80.0	-0.11	-0.13	-0.15	-0.17	-0.18	-0.19	---	---	---	---	---	---	---
	90.0	-0.01	-0.03	-0.03	-0.04	-0.04	-0.04	---	.07	.08	.08	.09	.10	.11
	95.0	.05	.05	.04	.04	.04	.04	---	.09	.09	.09	.10	.10	.10
0.44 b/2	0	---	---	.53	.49	.20	-.32	---	---	---	---	---	---	---
	1.5	---	---	-0.20	-0.62	-1.13	-1.72	---	---	---	---	---	---	---
	4.0	---	---	-0.33	-0.60	-0.96	-1.34	---	-0.63	-0.33	-.08	.17	.35	.47
	7.0	---	---	-0.41	-0.64	-0.91	-1.21	---	---	---	---	---	---	---
	10.0	---	---	-0.43	-0.68	-0.85	-1.09	---	-0.46	-0.29	-.11	.05	.12	.22
	15.0	---	---	-0.41	-0.62	-0.76	-0.94	---	-0.40	-0.25	-.12	.01	.09	.18
	20.0	---	---	-0.33	-0.52	-0.69	-0.83	---	-0.32	-0.21	-.10	0	.07	.14
	30.0	-0.19	-0.29	-0.39	-0.42	-0.50	-0.57	---	-0.23	-0.15	-.08	0	.05	.11
	40.0	-0.19	-0.26	-0.34	-0.42	-0.50	-0.47	---	-0.09	-0.05	-.01	.02	.06	.12
	50.0	-0.18	-0.24	-0.30	-0.35	-0.41	-0.47	---	-0.05	-0.01	.02	.06	.08	.12
	60.0	-0.16	-0.21	-0.25	-0.29	-0.34	-0.37	---	.01	.04	.06	.08	.10	.13
	70.0	-0.14	-0.17	-0.21	-0.23	-0.26	-0.28	---	.06	.07	.07	.09	.10	.10
	80.0	-0.10	-0.12	-0.14	-0.16	-0.17	-0.17	---	.09	.09	.09	.10	.09	.09
	90.0	0	-0.01	-0.06	-0.06	-0.05	-0.05	---	.09	.09	.09	.10	.09	.09
	95.0	.06	.06	.06	.06	.06	.06	---	.09	.09	.09	.10	.09	.09

NACA

TABLE IV.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING.

 $M_\infty = 0.165; R = 8,000,000$ - Continued(a) a_{u1} , $-2^\circ, 0^\circ, 2^\circ, 4^\circ, 6^\circ, 8^\circ$ - Concluded

Spanwise station	Percent chord	Upper surface						Lower surface					
		Angle of attack						Angle of attack					
		-2°	0°	2°	4°	6°	8°	-2°	0°	2°	4°	6°	8°
0.56 b/2	0	---	---	0.53	0.46	0.10	-0.54	---	---	0.07	0.35	0.51	0.56
	1.5	---	---	-1.16	-1.61	-1.16	-1.79	---	---	-0.07	0.16	0.34	0.48
	4.0	---	---	-0.31	-0.64	-0.97	-1.37	---	---	-0.27	-0.14	0.11	0.21
	7.0	---	---	-0.36	-0.62	-0.91	-1.21	---	---	-0.33	-0.20	0.01	0.19
	10.0	---	---	-0.41	-0.61	-0.85	-1.10	---	---	-0.37	-0.26	0.06	0.13
	15.0	---	---	-0.40	-0.56	-0.77	-0.94	---	---	-0.33	-0.20	0.01	0.11
	20.0	---	---	-0.38	-0.50	-0.66	-0.81	---	---	-0.29	-0.16	0.08	0.13
	30.0	---	---	-0.35	-0.44	-0.56	-0.66	---	---	-0.17	-0.10	0.03	0.07
	40.0	---	-1.17	-1.25	-0.32	-0.41	-0.49	-0.56	---	---	-0.11	-0.06	0.03
	50.0	---	-1.17	-1.23	-0.27	-0.35	-0.41	-0.47	---	---	-0.05	-0.01	0.07
	60.0	---	-1.13	-1.20	-0.24	-0.29	-0.33	-0.36	---	---	0.05	0.08	0.10
	70.0	---	-1.13	-1.16	-0.20	-0.23	-0.26	-0.28	0	0.03	0.06	0.10	0.13
	80.0	---	-1.10	-1.12	-0.14	-0.16	-0.17	-0.17	0.05	0.08	0.10	0.11	0.12
	90.0	---	-0.01	-0.08	-0.03	-0.03	-0.03	-0.04	0.09	0.08	0.09	0.10	0.10
	95.0	0.06	-0.03	-0.03	-0.03	-0.06	-0.03	-0.04	0.09	0.10	0.10	0.09	0.09
0.68 b/2	0	---	---	---	---	---	---	---	---	0.03	0.30	0.47	0.55
	1.5	---	---	-0.03	-0.14	-0.97	-1.60	---	---	-0.13	0.12	0.30	0.45
	4.0	---	---	-0.29	-0.68	-1.00	-1.37	---	---	-0.24	-0.11	0.11	0.21
	7.0	---	---	-0.32	-0.59	-0.90	-1.17	---	---	-0.28	-0.14	0.04	0.17
	10.0	---	---	-0.37	-0.57	-0.81	-1.06	---	---	-0.32	-0.14	0.06	0.29
	15.0	---	---	-0.36	-0.53	-0.70	-0.92	---	---	-0.24	-0.11	0.08	0.18
	20.0	---	---	-0.35	-0.53	-0.66	-0.81	---	---	-0.22	-0.11	0.07	0.14
	30.0	---	-1.14	-1.23	-0.34	-0.45	-0.57	-0.69	---	---	-0.17	0.01	0.07
	40.0	---	-1.14	-1.22	-0.30	-0.39	-0.47	-0.55	---	---	-0.11	-0.05	0.12
	50.0	---	-1.15	-1.21	-0.27	-0.33	-0.40	-0.45	0.05	0.01	0.02	0.06	0.09
	60.0	---	-1.12	-1.18	-0.22	-0.26	-0.31	-0.34	0.01	0.02	0.04	0.07	0.11
	70.0	---	-1.11	-1.14	-0.18	-0.21	-0.24	-0.26	0.07	0.03	0.05	0.09	0.12
	80.0	---	-0.08	-0.10	-0.13	-0.15	-0.16	-0.18	0.09	0.03	0.05	0.09	0.10
	90.0	0.01	0	0.01	0.01	0.01	0.02	0.03	0.09	0.03	0.05	0.09	0.10
	95.0	0.03	-0.05	-0.05	-0.05	-0.05	-0.05	-0.05	0.09	0.03	0.05	0.09	0.09
0.80 b/2	0	---	---	0.56	0.53	0.17	-0.47	---	---	-0.13	0.24	0.45	0.55
	1.5	---	---	0	-0.43	-0.93	-1.58	---	---	-0.20	0.08	0.26	0.42
	4.0	---	---	-0.18	-0.30	-0.85	-1.20	---	---	-0.21	-0.01	0.14	0.24
	7.0	---	---	-0.23	-0.32	-0.81	-1.08	---	---	-0.24	-0.03	0.09	0.19
	10.0	---	---	-0.31	-0.31	-0.73	-0.98	---	---	-0.27	-0.13	0.08	0.17
	15.0	---	---	-0.31	-0.30	-0.66	-0.85	---	---	-0.31	-0.18	0.06	0.12
	20.0	---	---	-0.30	-0.45	-0.60	-0.75	---	---	-0.37	-0.18	0.08	0.12
	30.0	---	---	-0.28	-0.37	-0.48	-0.59	---	---	-0.27	-0.18	0.05	0.12
	40.0	---	-0.11	-0.19	-0.27	-0.35	-0.43	-0.51	---	---	-0.12	-0.07	0.02
	50.0	---	-0.12	-0.18	-0.24	-0.31	-0.37	-0.43	0.06	0.03	0.01	0.04	0.06
	60.0	---	-0.11	-0.15	-0.20	-0.25	-0.30	-0.34	0.01	0.02	0.04	0.07	0.10
	70.0	---	-0.10	-0.13	-0.18	-0.20	-0.24	-0.26	0.03	0.04	0.05	0.07	0.11
	80.0	---	-0.07	-0.09	-0.12	-0.14	-0.15	-0.18	0.07	0.05	0.07	0.09	0.10
	90.0	0.01	0	0.01	-0.02	-0.03	-0.04	0.09	0.07	0.10	0.10	0.10	0.10
	95.0	0.06	-0.06	-0.05	-0.05	-0.05	-0.04	0.09	0.09	0.10	0.10	0.10	0.10
0.94 b/2	0	---	---	0.40	0.56	0.46	-0.07	---	---	-0.38	0.06	0.36	0.52
	1.5	---	---	-0.06	-0.15	-0.19	-0.60	---	---	-0.20	-0.06	0.10	0.24
	4.0	---	---	-0.14	-0.23	-0.33	-0.65	---	---	-0.29	-0.09	0.03	0.18
	7.0	---	---	-0.14	-0.24	-0.38	-0.67	---	---	-0.33	-0.22	0.07	0.10
	10.0	---	---	-0.18	-0.30	-0.38	-0.71	---	---	-0.38	-0.27	-0.07	0.10
	15.0	---	---	-0.20	-0.35	-0.31	-0.71	---	---	-0.40	-0.33	-0.07	0.09
	20.0	---	---	-0.19	-0.31	-0.28	-0.65	---	---	-0.38	-0.27	-0.07	0.10
	30.0	---	---	-0.16	-0.25	-0.28	-0.51	---	---	-0.26	-0.18	-0.05	0.07
	40.0	-0.06	-0.14	-0.21	-0.27	-0.25	-0.49	0.03	0.01	-0.06	0.03	0.01	0.06
	50.0	-0.11	-0.15	-0.20	-0.25	-0.28	-0.43	0.09	0.07	-0.06	0.03	0.01	0.05
	60.0	-0.10	-0.13	-0.18	-0.20	-0.20	-0.42	0.04	0.02	-0.07	0.02	0.01	0.04
	70.00	-0.09	-0.11	-0.13	-0.15	-0.15	-0.39	0.03	0.02	-0.03	0.03	0.01	0.03
	80.0	-0.05	-0.07	-0.08	-0.10	-0.12	-0.20	0.05	0.06	-0.05	0.06	0.01	0.07
	90.0	0.03	0.02	0.01	0.01	0.01	0	0.05	0.07	0.07	0.07	0.07	0.07
	95.0	0.07	0.07	0.07	0.06	0.06	0.05	0.05	0.10	0.10	0.10	0.09	0.08

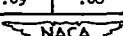


TABLE IV.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING.
 $M_\infty = 0.165$; $R = 8,000,000$ - Continued
 (b) a_u , $10^\circ, 12^\circ, 14^\circ, 16^\circ, 18^\circ, 20^\circ$

Spanwise station	Percent chord	Upper surface						Lower surface					
		Angle of attack						Angle of attack					
		10°	12°	14°	16°	18°	20°	10°	12°	14°	16°	18°	20°
0.10 b/2	0	-0.26	-0.79	-1.43	-2.18	-3.03	-4.00	—	—	—	—	—	—
	1.5	-1.51	-1.97	-2.46	-3.03	-3.58	-4.19	0.56	0.55	0.48	0.36	0.19	-0.03
	4.0	-1.31	-1.62	-1.95	-2.31	-2.65	-3.03	0.48	0.55	0.60	0.62	0.61	0.58
	7.0	-1.14	-1.39	-1.68	-1.87	-2.12	-2.37	—	—	—	—	—	—
	10.0	-1.07	-1.26	-1.43	-1.63	-1.82	-2.01	—	—	—	—	—	—
	15.0	-0.95	-1.09	-1.21	-1.35	-1.49	-1.68	—	—	—	—	—	—
	20.0	-0.89	-1.00	-1.11	-1.21	-1.31	-1.41	—	—	—	—	—	—
	30.0	-0.73	-0.80	-0.87	-0.93	-1.00	-1.07	—	—	—	—	—	—
	40.0	-0.60	-0.65	-0.70	-0.74	-0.79	-0.84	—	—	—	—	—	—
	50.0	-0.46	-0.49	-0.53	-0.56	-0.58	-0.62	—	—	—	—	—	—
	60.0	-0.38	-0.40	-0.43	-0.44	-0.46	-0.48	—	—	—	—	—	—
	70.0	-0.29	-0.30	-0.31	-0.31	-0.33	-0.34	—	—	—	—	—	—
	80.0	-0.18	-0.18	-0.18	-0.18	-0.19	-0.20	—	—	—	—	—	—
	90.0	-0.03	-0.02	-0.03	-0.03	-0.04	-0.05	—	—	—	—	—	—
	95.0	.05	.04	.04	.03	.03	0	—	—	—	—	—	—
0.19 b/2	0	.67	-1.40	-2.26	-3.31	-4.43	-5.77	—	—	—	—	—	—
	1.5	-2.19	-2.85	-3.56	-4.35	-5.16	-6.01	.56	.49	.36	.15	-.12	-.46
	4.0	-1.73	-2.10	-2.55	-2.93	-3.36	-3.81	.52	.57	.59	.58	.54	.46
	7.0	-1.30	-1.57	-1.86	-2.16	-2.14	-2.73	—	—	—	—	—	—
	10.0	-1.20	-1.42	-1.64	-1.87	-2.10	-2.33	.34	.43	.50	.56	.59	.61
	15.0	-1.07	-1.23	-1.40	-1.56	-1.71	-1.87	.27	.35	.42	.48	.53	.57
	20.0	-0.86	-0.99	-1.12	-1.24	-1.35	-1.48	.23	.30	.37	.43	.48	.53
	30.0	-0.73	-0.83	-0.90	-0.98	-1.04	-1.10	.17	.24	.30	.35	.40	.45
	40.0	-0.63	-0.68	-0.73	-0.78	-0.82	-0.86	.15	.21	.26	.31	.35	.39
	50.0	-0.48	-0.51	-0.54	-0.56	-0.59	-0.61	—	—	—	—	—	—
	60.0	-0.37	-0.38	-0.40	-0.42	-0.42	-0.43	.14	.18	.22	.25	.28	.31
	70.0	-0.27	-0.27	-0.27	-0.26	-0.26	-0.28	.15	.18	.21	.24	.26	.29
	80.0	-0.15	-0.14	-0.13	-0.12	-0.13	-0.17	—	—	—	—	—	—
	90.0	-0.01	-0.01	-0.02	-0.03	-0.07	-0.12	.12	.13	.14	.15	.16	.17
	95.0	.05	.03	.02	.02	.01	.06	.08	.08	.08	.08	.08	.08
0.31 b/2	0	-0.89	-1.73	-2.70	-3.90	-5.20	-6.64	—	—	—	—	—	—
	1.5	-2.14	-2.83	-3.56	-4.35	-5.34	-6.09	.53	.41	.21	-.08	-.44	-.86
	4.0	-1.73	-2.38	-2.59	-3.07	-3.53	-4.00	.55	.58	.57	.53	.44	.38
	7.0	-1.45	-1.73	-2.08	-2.41	-2.72	-3.03	—	—	—	—	—	—
	10.0	-1.26	-1.51	-1.76	-2.01	-2.24	-2.47	.38	.46	.52	.57	.59	.61
	15.0	-1.10	-1.26	-1.44	-1.63	-1.78	-1.91	.29	.37	.44	.50	.54	.57
	20.0	-0.93	-1.08	-1.21	-1.34	-1.56	-1.55	.23	.38	.43	.49	.53	.53
	30.0	-0.75	-0.83	-0.90	-0.99	-1.03	-1.06	.19	.25	.31	.36	.41	.45
	40.0	-0.62	-0.67	-0.72	-0.73	-0.77	-0.76	.17	.22	.26	.31	.35	.39
	50.0	-0.51	-0.54	-0.56	-0.56	-0.54	-0.50	.16	.20	.24	.28	.31	.34
	60.0	-0.38	-0.39	-0.39	-0.37	-0.33	-0.38	—	—	—	—	—	—
	70.0	-0.27	-0.26	-0.24	-0.20	-0.18	-0.23	.15	.18	.20	.23	.25	.27
	80.0	-0.15	-0.12	-0.09	-0.08	-0.12	-0.19	—	—	—	—	—	—
	90.0	.01	.02	0	-0.03	-0.08	-0.09	.12	.12	.13	.13	.13	.13
	95.0	.05	.04	.02	.02	.01	.03	.10	.10	.10	.10	.09	.08
0.375 b/2	0	-1.07	-0.00	-3.10	-4.42	-5.83	-7.07	—	—	—	—	—	—
	1.5	-2.44	-3.20	-4.02	-4.91	-5.81	-6.60	.51	.37	.16	-.14	-.51	-.94
	4.0	-1.72	-2.19	-2.61	-3.10	-3.58	-4.06	.54	.57	.56	.51	.43	.31
	7.0	-1.49	-1.81	-2.13	-2.47	-2.78	-3.08	—	—	—	—	—	—
	10.0	-1.31	-1.56	-1.85	-2.07	-2.21	-2.50	.38	.46	.52	.57	.59	.61
	15.0	-1.11	-1.29	-1.48	-1.66	-1.86	-1.93	.30	.38	.45	.50	.53	.58
	20.0	-0.98	-1.11	-1.24	-1.38	-1.48	-1.54	.26	.33	.39	.45	.50	.54
	30.0	-0.70	-0.80	-0.87	-0.96	-1.01	-1.00	.20	.26	.31	.37	.42	.46
	40.0	-0.63	-0.69	-0.74	-0.78	-0.79	-0.78	.17	.22	.27	.32	.36	.39
	50.0	-0.50	-0.54	-0.57	-0.59	-0.60	-0.63	—	—	—	—	—	—
	60.0	-0.39	-0.42	-0.43	-0.45	-0.46	-0.54	.15	.19	.22	.25	.28	.31
	70.0	-0.30	-0.31	-0.32	-0.34	-0.37	-0.47	.15	.18	.21	.24	.26	.28
	80.0	-0.26	-0.20	-0.21	-0.23	-0.27	-0.33	—	—	—	—	—	—
	90.0	-0.04	-0.04	-0.06	-0.09	-0.12	-0.15	.12	.15	.17	.18	.19	.19
	95.0	.03	.02	.01	.01	.03	.03	.10	.11	.12	.14	.15	.17
0.44 b/2	0	-1.07	-0.02	-3.16	-4.50	-5.96	-7.51	—	—	—	—	—	—
	1.5	-0.41	-3.18	-3.93	-4.82	-5.68	-6.53	.51	.34	.07	-.29	-.72	-.19
	4.0	-1.77	-2.83	-2.69	-3.20	-4.69	-5.13	.55	.58	.57	.51	.42	.30
	7.0	-1.54	-1.86	-2.20	-2.57	-3.89	-3.19	—	—	—	—	—	—
	10.0	-1.35	-1.60	-1.88	-2.15	-2.39	-2.60	.39	.47	.53	.57	.59	.60
	15.0	-1.14	-1.32	-1.58	-1.70	-1.85	-1.98	.30	.38	.45	.50	.55	.58
	20.0	-0.98	-1.13	-1.27	-1.42	-1.52	-1.60	.26	.33	.40	.45	.50	.54
	30.0	-0.80	-0.89	-0.98	-1.06	-1.12	-1.14	.20	.26	.29	.37	.42	.46
	40.0	-0.64	-0.70	-0.75	-0.80	-0.83	-0.83	.16	.22	.26	.31	.35	.39
	50.0	-0.51	-0.55	-0.58	-0.61	-0.62	-0.61	.16	.20	.24	.28	.32	.35
	60.0	-0.40	-0.42	-0.43	-0.44	-0.44	-0.47	.15	.19	.22	.25	.26	.31
	70.0	-0.29	-0.29	-0.28	-0.28	-0.28	-0.36	.16	.18	.21	.24	.26	.28
	80.0	-0.17	-0.15	-0.14	-0.14	-0.18	-0.29	—	—	—	—	—	—
	90.0	-0.02	-0.02	-0.03	-0.06	-0.13	-0.24	.11	.12	.12	.13	.13	.14
	95.0	.04	.02	.01	.01	.03	.03	.09	.09	.09	.09	.09	.07

NACA

TABLE IV.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING;
 $M_\infty = 0.165$; $R = 8,000,000$ - Concluded

(b) a_u , $10^\circ, 12^\circ, 14^\circ, 16^\circ, 18^\circ, 20^\circ$ - Concluded

Spanwise station	Percent chord	Upper surface						Lower surface						
		Angle of attack						Angle of attack						
		10°	12°	14°	16°	18°	20°		10°	12°	14°	16°	18°	20°
0.56 b/2	0	-1.39	-2.50	-3.80	-5.33	-6.98	-8.72							
	1.5	-2.53	-3.34	-4.18	-5.13	-6.06	-6.83		0.51	0.32	0.03	-0.35	-0.79	-1.29
	4.0	-1.82	-2.29	-2.78	-3.30	-3.87	-4.25		.56	.39	.56	.52	.43	.31
	7.0	-1.56	-1.88	-2.21	-2.61	-2.94	-3.23							
	10.0	-1.35	-1.63	-1.89	-2.18	-2.42	-2.68		.39	.47	.53	.57	.59	.59
	15.0	-1.14	-1.32	-1.46	-1.74	-1.87	-1.96		.30	.38	.42	.50	.54	.57
	20.0	-0.95	-1.11	-1.24	-1.38	-1.51	-1.57		.27	.34	.40	.46	.50	.54
	30.0	-0.76	-0.86	-0.93	-1.01	-1.07	-1.10		.20	.26	.32	.37	.42	.46
	40.0	-0.66	-0.69	-0.74	-0.79	-0.83	-0.87		.18	.23	.27	.32	.36	.40
	50.0	-0.51	-0.55	-0.58	-0.61	-0.63	-0.70		.16	.20	.24	.28	.31	.34
	60.0	-0.39	-0.42	-0.44	-0.46	-0.49	-0.58							
	70.0	-0.29	-0.30	-0.31	-0.32	-0.37	-0.47		.15	.18	.21	.23	.26	.28
	80.0	-0.17	-0.17	-0.18	-0.22	-0.26	-0.35		.14	.16	.18	.20	.22	.24
	90.0	-0.02	-0.03	-0.06	-0.10	-0.14	-0.20		.11	.12	.13	.14	.16	.18
	95.0	.03	.02	-0.02	-0.05	-0.09	-0.10		.09	.09	.10	.10	.11	.12
0.68 b/2	0	---	---	---	---	---	---							
	1.5	-0.32	-3.07	-3.84	-4.74	-5.63	-6.51		.51	.36	.08	.27	.69	-1.17
	4.0	-1.82	-2.30	-2.81	-3.34	-3.84	-4.35		.55	.27	.56	.53	.43	.32
	7.0	-1.32	-1.85	-2.22	-2.60	-2.92	-3.21							
	10.0	-1.33	-1.60	-1.88	-2.16	-2.41	-2.61		.39	.47	.53	.57	.58	.59
	15.0	-1.13	-1.32	-1.53	-1.73	-1.89	-2.00		.31	.38	.45	.50	.54	.57
	20.0	-0.98	-1.14	-1.31	-1.45	-1.54	-1.60		.26	.33	.40	.45	.49	.53
	30.0	-0.80	-0.90	-0.99	-1.07	-1.12	-1.10		.21	.27	.32	.37	.41	.45
	40.0	-0.63	-0.69	-0.74	-0.78	-0.78	-0.71		.17	.22	.27	.31	.35	.38
	50.0	-0.50	-0.54	-0.56	-0.55	-0.51	-0.45							
	60.0	-0.37	-0.39	-0.39	-0.36	-0.31	-0.33		.15	.17	.21	.24	.26	.28
	70.0	-0.27	-0.27	-0.24	-0.19	-0.17	-0.28		.14	.16	.18	.20	.22	.23
	80.0	-0.15	-0.13	-0.10	-0.09	-0.14	-0.29		.13	.15	.16	.17	.18	.19
	90.0	0	0	-0.01	-0.04	-0.12	-0.19		.11	.12	.11	.11	.11	.10
	95.0	.04	.03	0	-0.05	-0.15	-0.26		.09	.09	.08	.06	.04	.02
0.80 b/2	0	-1.40	-2.60	-4.04	-5.71	-7.47	-9.33							
	1.5	-2.30	-3.02	-3.76	-4.64	-5.49	-6.31		.55	.45	.21	.09	.46	.87
	4.0	-1.53	-2.10	-2.59	-3.09	-3.57	-4.00		.32	.37	.54	.47	.37	
	7.0	-1.40	-1.74	-2.09	-2.47	-2.73	-3.03							
	10.0	-1.24	-1.51	-1.76	-2.05	-2.29	-2.47		.36	.45	.49	.54	.58	.61
	15.0	-1.06	-1.25	-1.45	-1.64	-1.80	-1.91		.28	.37	.43	.49	.53	.56
	20.0	-0.90	-1.03	-1.20	-1.34	-1.45	-1.52		.25	.32	.38	.44	.48	.51
	30.0	-0.70	-0.80	-0.89	-0.98	-1.04	-1.03		.19	.25	.30	.33	.39	.43
	40.0	-0.58	-0.63	-0.71	-0.76	-0.79	-0.79							
	50.0	-0.48	-0.52	-0.55	-0.57	-0.57	-0.58		.14	.18	.22	.25	.28	.32
	60.0	-0.37	-0.39	-0.40	-0.40	-0.40	-0.45		.13	.17	.20	.23	.25	.27
	70.0	-0.27	-0.28	-0.27	-0.25	-0.26	-0.35		.13	.15	.18	.20	.21	.23
	80.0	-0.16	-0.14	-0.13	-0.13	-0.17	-0.28		.11	.13	.14	.15	.16	.17
	90.0	-0.02	-0.02	-0.03	-0.07	-0.13	-0.23		.10	.11	.11	.11	.11	.11
	95.0	.04	.01	-0.01	-0.06	-0.12	-0.20		.10	.10	.09	.07	.07	.06
0.94 b/2	0	-1.66	-1.60	-2.82	-4.28	-5.86	-7.57							
	1.5	-2.23	-2.91	-3.62	-4.35	-5.05	-5.77		.57	.53	.35	.11	.20	.56
	4.0	-1.42	-1.84	-2.29	-2.71	-3.19	-3.61							
	7.0	-1.19	-1.49	-1.80	-2.13	-2.42	-2.69		.37	.46	.51	.57	.57	
	10.0	-1.01	-1.25	-1.49	-1.73	-1.94	-2.11		.29	.39	.44	.51	.53	.57
	15.0	-0.86	-1.01	-1.18	-1.35	-1.49	-1.62		.21	.30	.36	.42	.46	.50
	20.0	-0.73	-0.86	-1.00	-1.13	-1.23	-1.32		.17	.24	.30	.35	.40	.43
	30.0	-0.58	-0.61	-0.70	-0.78	-0.83	-0.87		.09	.13	.17	.21	.23	.26
	40.0	-0.46	-0.52	-0.57	-0.61	-0.65	-0.66		.09	.11	.14	.17	.19	.21
	50.0	-0.38	-0.42	-0.44	-0.46	-0.46	-0.47		.09	.11	.14	.17	.19	.21
	60.0	-0.29	-0.31	-0.33	-0.33	-0.38	-0.39							
	70.0	-0.21	-0.22	-0.22	-0.20	-0.20	-0.26		.07	.08	.09	.10	.11	
	80.0	-0.12	-0.12	-0.11	-0.09	-0.12	-0.21		.06	.07	.07	.06	.06	
	90.0	0	0	-0.01	-0.03	-0.06	-0.19		.06	.06	.05	.04	.02	0
	95.0	.05	.04	.02	-0.02	-0.08	-0.17		.08	.07	.05	.03	-.01	-.04

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TABLE V.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING.
 $M_\infty = 0.25$; $R = 8,000,000$
(a) $\alpha_u = -2^\circ, 0^\circ, 2^\circ, 4^\circ, 6^\circ, 8^\circ$

Spanwise station	Percent chord	Upper surface						Lower surface					
		Angle of attack						Angle of attack					
		-2°	0°	2°	4°	6°	8°	-2°	0°	2°	4°	6°	8°
0.10 b/2	0	0.20	0.43	0.55	0.57	0.46	0.25	---	---	0.08	0.30	0.48	0.59
	1.5	.33	.18	-.04	-.32	-.63	-1.03	-.56	-0.20	---	-.10	.10	.27
	4.0	.14	-.03	-.21	-.43	-.70	-.96	-.56	-.32	-.10	---	---	.39
	7.0	.03	-.11	-.27	-.45	-.65	-.86	---	---	---	---	---	---
	10.0	-.03	-.15	-.29	-.44	-.60	-.77	---	-.46	-.30	-.16	-.01	.18
	15.0	-.09	-.20	-.31	-.43	-.56	-.70	-.42	-.29	-.17	-.05	.07	.16
	20.0	-.13	-.22	-.33	-.43	-.54	-.65	-.36	-.26	-.16	-.05	.03	.13
	30.0	-.17	-.25	-.33	-.41	-.48	-.57	-.29	-.21	-.14	-.05	.03	.09
	40.0	-.17	-.23	-.29	-.35	-.40	-.48	-.23	-.17	-.10	-.03	.03	.09
	50.0	-.15	-.20	-.25	-.31	-.34	-.40	-.18	-.13	-.08	-.02	.03	.07
	60.0	-.18	-.19	-.23	-.26	-.29	-.34	-.11	-.07	-.03	.01	.06	---
	70.0	-.14	-.17	-.20	-.23	-.24	-.28	-.05	-.03	0	.04	.09	.15
0.19 b/2	0	-.11	-.14	-.16	-.17	-.18	-.20	---	---	---	---	---	---
	1.5	.12	.41	.55	.53	.33	-.03	---	---	---	---	---	---
	4.0	.41	.23	-.03	-.11	-.56	-1.36	-.73	-.30	.04	.30	.48	.56
	7.0	.05	-.02	-.24	-.58	-.83	-.16	-.64	-.35	-.12	.11	.29	.42
	10.0	-.04	-.12	-.31	-.53	-.78	-.103	---	---	---	---	---	---
	15.0	-.10	-.23	-.36	-.56	-.76	-.98	-.51	-.33	-.17	-.01	.11	.23
	20.0	-.11	-.22	-.36	-.52	-.68	-.85	-.44	-.29	-.17	-.04	.07	.17
	30.0	-.17	-.26	-.39	-.53	-.74	-.93	-.37	-.25	-.16	-.04	.05	.13
	40.0	-.20	-.28	-.41	-.55	-.78	-.92	-.30	-.20	-.12	-.04	.03	.10
	50.0	-.18	-.23	-.29	-.41	-.59	-.74	-.26	-.19	-.12	-.04	.05	.09
	60.0	-.16	-.20	-.24	-.29	-.31	-.33	-.08	-.05	-.02	.02	.07	---
	70.0	-.13	-.18	-.21	-.23	-.24	-.28	-.02	0	.03	.06	.09	.11
0.31 b/2	0	-.11	-.13	-.14	-.16	-.16	-.18	---	---	---	---	---	---
	1.5	.01	-.03	-.03	-.03	-.02	-.03	---	---	---	---	---	---
	4.0	.05	.03	-.03	-.05	-.05	-.05	---	---	---	---	---	---
	7.0	.06	.40	.54	.51	.26	-.18	---	---	---	---	---	---
	10.0	.43	.22	-.08	-.46	-.99	-1.51	-.77	-.30	.07	.34	.51	.57
	15.0	.18	-.04	-.31	-.60	-.94	-1.32	-.68	-.36	.15	.35	.46	---
	20.0	.04	-.14	-.36	-.60	-.92	-1.17	---	---	---	---	---	---
	30.0	-.03	-.18	-.37	-.58	-.80	-1.04	-.50	-.31	-.14	.02	.16	.26
	40.0	-.11	-.24	-.39	-.56	-.74	-.92	-.45	-.30	-.16	-.03	.09	.19
	50.0	-.11	-.26	-.38	-.52	-.67	-.81	-.36	-.24	-.14	-.03	.08	.15
	60.0	-.18	-.26	-.36	-.46	-.56	-.67	-.26	-.19	-.10	-.03	.05	.11
	70.0	-.21	-.28	-.35	-.43	-.50	-.58	-.19	-.13	-.08	-.01	.05	.10
0.375 b/2	0	-.19	-.25	-.30	-.35	-.41	-.47	---	---	---	---	---	---
	1.5	.19	-.29	-.35	-.43	-.50	-.58	---	---	---	---	---	---
	4.0	.19	-.29	-.35	-.43	-.50	-.58	---	---	---	---	---	---
	7.0	.19	-.29	-.35	-.43	-.50	-.58	---	---	---	---	---	---
	10.0	-.16	-.20	-.25	-.29	-.32	-.36	---	---	---	---	---	---
	15.0	-.10	-.14	-.19	-.23	-.25	-.28	---	---	---	---	---	---
	20.0	-.11	-.16	-.20	-.24	-.25	-.28	---	---	---	---	---	---
	30.0	-.13	-.19	-.22	-.27	-.29	-.32	---	---	---	---	---	---
	40.0	-.20	-.26	-.35	-.43	-.50	-.57	---	---	---	---	---	---
	50.0	-.19	-.23	-.30	-.36	-.41	-.48	---	---	---	---	---	---
	60.0	-.17	-.20	-.25	-.29	-.33	-.37	-.06	-.03	.01	.04	.06	---
0.44 b/2	0	-.15	-.18	-.20	-.24	-.26	-.28	0	.01	.04	.07	.10	.11
	1.5	.02	-.14	-.18	-.21	-.25	-.28	---	---	---	---	---	---
	4.0	.20	-.03	-.30	-.62	-.96	-1.35	-.72	-.40	-.08	.15	.33	.46
	7.0	.06	-.14	-.38	-.63	-.91	-1.22	---	---	---	---	---	---
	10.0	-.09	-.23	-.41	-.61	-.85	-1.10	-.53	-.33	-.14	.08	.16	.26
	15.0	.02	-.19	-.41	-.57	-.75	-.94	-.44	-.26	-.14	-.01	.10	.21
	20.0	-.13	-.25	-.37	-.52	-.68	-.82	-.37	-.23	-.12	-.01	.09	.17
	30.0	-.19	-.26	-.39	-.48	-.59	-.70	-.27	-.16	-.10	-.01	.06	.12
	40.0	-.19	-.26	-.34	-.41	-.49	-.57	-.20	-.13	-.07	0	.03	.10
	50.0	-.18	-.24	-.29	-.35	-.40	-.46	-.12	-.07	-.02	.02	.07	.11
	60.0	-.17	-.21	-.25	-.29	-.33	-.37	-.06	-.04	.01	.03	.08	.11
	70.0	-.14	-.18	-.21	-.24	-.25	-.27	0	-.02	.03	.07	.10	.12
	80.0	-.10	-.13	-.14	-.16	-.16	-.17	---	---	---	---	---	---
	90.0	-.01	-.02	-.02	-.03	-.01	-.02	0.05	.06	.07	.08	.09	.09
	95.0	.05	.03	.05	.05	.05	.04	.08	.07	.08	.09	.09	.09

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TABLE V.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING.

 $M_\infty = 0.25; R = 8,000,000$ - Continued(a) α_u , $-2^\circ, 0^\circ, 2^\circ, 4^\circ, 6^\circ, 8^\circ$ - Concluded

Spanwise station	Per-cent chord	Upper surface						Lower surface					
		Angle of attack						Angle of attack					
		-2°	0°	2°	4°	6°	8°	-2°	0°	2°	4°	6°	8°
0.56 b/2	0	-0.01	0.39	0.55	0.49	0.17	-0.39	-0.97	-0.40	0.05	0.35	0.52	0.58
	1.5	.45	.23	-.10	-.53	-1.06	-1.68	.72	-.41	-.08	.14	.34	.48
	4.0	.22	.01	.28	.62	.96	1.37	---	---	---	---	---	---
	7.0	.08	-.11	.36	-.65	-.91	-1.23	---	---	---	---	---	---
	10.0	0	-.18	.40	-.60	-.89	-1.11	-.57	-.37	-.15	.01	.17	.29
	15.0	-.08	-.22	-.40	-.59	-.76	-.95	-.45	-.30	-.15	-.01	.11	.21
	20.0	-.09	-.22	-.35	-.49	-.65	-.81	-.36	-.22	-.11	0	.09	.18
	30.0	-.13	-.22	-.33	-.43	-.54	-.65	-.28	-.19	-.10	-.01	.06	.12
	40.0	-.17	-.23	-.32	-.40	-.48	-.56	-.18	-.12	-.05	.01	.06	.11
	50.0	-.17	-.23	-.29	-.36	-.40	-.46	-.12	-.08	-.02	.03	.07	.11
	60.0	-.14	-.20	-.24	-.26	-.32	-.36	---	---	---	---	---	---
	70.0	-.13	-.16	-.19	-.23	-.24	-.27	0	.01	.05	.08	.10	.11
	80.0	-.10	-.13	-.14	-.16	-.16	-.17	.03	.05	.07	.09	.10	.11
	90.0	-.01	-.03	-.02	-.03	-.02	-.02	.08	.07	.08	.09	.10	.10
	95.0	.06	.05	.06	.06	.06	.04	.09	.08	.09	.10	.10	.09
0.68 b/2	0	---	---	0	---	---	---	---	---	---	---	---	---
	1.5	.49	.30	0	-.25	-.40	-.93	-.155	-.09	-.50	-.03	.30	.48
	4.0	.29	.02	-.25	-.58	-.97	-.134	-.82	-.47	-.15	.10	.30	.46
	7.0	.12	-.07	-.30	-.56	-.88	-.116	---	---	---	---	---	---
	10.0	.03	-.14	-.35	-.55	-.79	-.104	-.56	-.34	-.15	0	.16	.28
	15.0	-.03	-.17	-.33	-.51	-.69	-.89	-.46	-.30	-.16	-.02	.10	.20
	20.0	-.07	-.19	-.33	-.48	-.63	-.79	-.36	-.24	-.13	-.01	.09	.17
	30.0	-.13	-.23	-.33	-.43	-.54	-.65	-.26	-.18	-.09	-.01	.06	.13
	40.0	-.14	-.22	-.30	-.38	-.46	-.54	-.18	-.12	-.06	.01	.06	.11
	50.0	-.14	-.20	-.27	-.33	-.39	-.44	---	---	---	---	---	---
	60.0	-.12	-.17	-.22	-.26	-.30	-.34	-.05	-.02	-.01	.06	.09	.11
	70.0	-.10	-.14	-.19	-.21	-.24	-.25	-.01	.01	.04	.06	.09	.11
	80.0	-.08	-.11	-.14	-.15	-.15	-.15	.04	.05	.07	.09	.11	.11
	90.0	0	-.01	-.01	-.02	-.02	-.01	.07	.07	.08	.09	.10	.10
	95.0	.07	.06	.06	.06	.05	.05	.08	.08	.09	.10	.09	.09
0.80 b/2	0	-.16	.34	.58	.57	.27	-.28	---	---	---	---	---	---
	1.5	.50	.32	.03	-.38	-.90	-.151	-.129	-.64	-.13	.23	.46	.57
	4.0	.30	.10	-.15	-.47	-.82	-.118	-.86	-.56	-.22	.25	.43	---
	7.0	.17	-.02	-.23	-.49	-.79	-.104	---	---	---	---	---	---
	10.0	.09	-.09	-.29	-.48	-.72	-.96	-.60	-.39	-.21	-.02	.10	.26
	15.0	.01	-.12	-.29	-.49	-.65	-.84	-.49	-.33	-.19	-.05	.07	.18
	20.0	-.04	-.16	-.29	-.45	-.59	-.75	-.38	-.26	-.14	-.03	.07	.15
	30.0	-.07	-.16	-.26	-.36	-.47	-.58	-.28	-.18	-.11	-.03	.03	.11
	40.0	-.11	-.19	-.27	-.34	-.42	-.50	---	---	---	---	---	---
	50.0	-.12	-.18	-.25	-.31	-.35	-.42	-.12	-.08	-.04	.01	.06	.10
	60.0	-.10	-.15	-.20	-.25	-.29	-.32	-.03	-.03	0	.04	.08	.10
	70.0	-.09	-.13	-.18	-.20	-.23	-.25	-.01	.01	.04	.07	.09	.10
	80.0	-.07	-.09	-.12	-.14	-.14	-.15	.03	.05	.06	.07	.09	.10
	90.0	.01	0	-.02	-.02	-.02	-.02	.07	.07	.08	.10	.10	.10
	95.0	.06	.05	.05	.04	.06	.05	.09	.09	.09	.11	.11	.10
0.94 b/2	0	-.73	-.01	.42	.57	.49	.15	---	---	---	---	---	---
	1.5	.53	.39	.17	-.16	-.58	-.110	-.172	-.97	-.38	.05	.35	.52
	4.0	.37	.20	-.01	-.29	-.61	-.98	---	---	---	---	---	---
	7.0	.22	.05	-.12	-.35	-.63	-.91	-.74	-.50	-.25	-.05	.11	.27
	10.0	.13	0	-.18	-.38	-.55	-.77	-.62	-.43	-.27	-.09	.04	.17
	15.0	.07	-.05	-.19	-.34	-.50	-.66	-.51	-.37	-.23	-.10	.02	.12
	20.0	.02	-.06	-.20	-.30	-.46	-.59	-.39	-.28	-.18	-.08	.01	.10
	30.0	-.02	-.10	---	-.25	-.33	-.44	-.27	-.20	-.13	-.05	.01	.06
	40.0	-.09	-.14	-.21	-.26	-.34	-.41	-.17	-.13	-.08	-.03	.01	.06
	50.0	-.10	-.15	-.20	-.24	-.29	-.35	-.09	-.05	-.04	0	.03	.06
	60.0	-.10	-.13	-.18	-.20	-.24	-.27	---	---	---	---	---	---
	70.0	-.08	-.11	-.14	-.16	-.18	-.20	.01	.02	.03	.05	.06	.07
	80.0	-.05	-.07	-.09	-.10	-.11	-.12	.06	.06	.06	.07	.08	.08
	90.0	.03	.02	.01	.01	.01	.01	.06	.06	.06	.08	.09	.08
	95.0	.07	.06	.06	.06	.06	.06	.10	.09	.09	.10	.10	.09

NACA

TABLE V. - PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING

 $M_\infty = 0.25; R = 8,000,000$ - Continued(b) α_{u1} , $10^\circ, 12^\circ, 14^\circ, 16^\circ, 18^\circ, 20^\circ$

Spanwise Station	Percent chord	Upper surface						Lower surface							
		Angle of attack						Angle of attack							
		10°	12°	14°	16°	18°	20°	10°	12°	14°	16°	18°	20°		
0.10 b/2	0	-0.09	-0.52	-1.05	-1.71	-2.41	-3.27	---	---	0.68	0.65	0.59	0.49	0.35	
	1.5	-1.45	-1.91	-2.39	-3.01	-3.60	-4.19	0.66	0.62	0.68	0.73	0.76	0.75	---	
	4.0	-1.24	-1.55	-1.87	-2.24	-2.60	-2.97	0.53	0.52	0.58	0.62	0.66	0.71	---	
	7.0	-1.09	-1.31	-1.54	-1.87	-2.06	-2.32	0.41	0.40	0.43	0.42	0.46	0.50	0.55	
	10.0	-0.96	-1.12	-1.30	-1.50	-1.69	-1.88	0.35	0.32	0.37	0.42	0.46	0.50	0.54	
	15.0	-0.84	-0.97	-1.10	-1.25	-1.39	-1.52	0.27	0.30	0.37	0.44	0.49	0.56	0.61	
	20.0	-0.76	-0.86	-1.08	-1.21	-1.37	-1.52	0.22	0.24	0.30	0.36	0.40	0.45	0.50	
	30.0	-0.65	-0.71	-0.79	-0.84	-0.90	-0.96	0.17	0.21	0.25	0.31	0.36	0.40	0.45	
	40.0	-0.52	-0.59	-0.62	-0.66	-0.70	-0.73	0.15	0.18	0.22	0.27	0.31	0.36	0.40	
	50.0	-0.43	-0.48	-0.51	-0.53	-0.55	-0.58	0.13	0.16	0.21	0.26	0.29	0.32	0.36	
	60.0	-0.36	-0.40	-0.40	-0.42	-0.44	-0.45	0.14	0.18	0.21	0.26	0.28	0.30	0.33	
	70.0	-0.29	-0.31	-0.31	-0.32	-0.33	-0.35	0.14	0.18	0.21	0.26	0.28	0.30	0.32	
	80.0	-0.20	-0.21	-0.21	-0.20	-0.23	-0.25	0.11	0.12	0.14	0.17	0.18	0.20	0.22	
	90.0	-0.05	-0.05	-0.05	-0.07	-0.09	-0.10	0.09	0.10	0.11	0.12	0.13	0.14	0.16	
	95.0	0.02	0	0	-0.01	-0.02	-0.04	0.09	0.09	0.10	0.11	0.12	0.13	0.14	
0.19 b/2	0	-0.57	-1.26	-2.10	-3.13	-4.27	-5.59	---	---	0.58	0.50	0.37	0.17	-0.09	-0.42
	1.5	-1.96	-2.61	-3.33	-4.16	-5.03	-6.00	0.53	0.58	0.60	0.60	0.66	0.68	0.69	0.69
	4.0	-1.55	-1.93	-2.35	-2.82	-3.29	-3.79	0.44	0.43	0.49	0.57	0.60	0.66	0.68	0.69
	7.0	-1.31	-1.59	-1.88	-2.21	-2.54	-2.87	0.34	0.35	0.42	0.50	0.55	0.60	0.63	0.65
	10.0	-1.21	-1.43	-1.63	-1.91	-2.17	-2.43	0.29	0.35	0.42	0.50	0.55	0.60	0.63	0.65
	15.0	-1.02	-1.18	-1.34	-1.53	-1.71	-1.89	0.21	0.29	0.37	0.43	0.49	0.55	0.59	0.61
	20.0	-0.86	-0.98	-1.11	-1.26	-1.39	-1.53	0.16	0.22	0.29	0.35	0.40	0.45	0.50	0.53
	30.0	-0.72	-0.80	-0.88	-0.96	-1.05	-1.13	0.15	0.20	0.25	0.30	0.35	0.40	0.45	0.48
	40.0	-0.60	-0.67	-0.71	-0.73	-0.80	-0.84	0.13	0.17	0.21	0.25	0.27	0.31	0.35	0.38
	50.0	-0.48	-0.52	-0.55	-0.57	-0.56	-0.62	0.13	0.17	0.20	0.22	0.25	0.28	0.31	0.33
	60.0	-0.37	-0.40	-0.41	-0.41	-0.42	-0.44	0.13	0.17	0.20	0.22	0.25	0.28	0.31	0.33
	70.0	-0.28	-0.29	-0.28	-0.28	-0.28	-0.30	0.13	0.17	0.20	0.22	0.25	0.28	0.31	0.33
	80.0	-0.16	-0.15	-0.14	-0.13	-0.15	-0.16	0.10	0.11	0.12	0.13	0.14	0.16	0.18	0.20
	90.0	-0.02	-0.02	-0.04	-0.05	-0.10	-0.15	0.09	0.09	0.10	0.10	0.09	0.09	0.08	0.08
	95.0	0.03	0	0	-0.04	-0.05	-0.14	0.09	0.09	0.10	0.10	0.09	0.09	0.08	0.08
0.31 b/2	0	-0.84	-1.66	-2.66	-3.85	-5.19	-6.65	---	---	0.54	0.44	0.21	-0.04	-0.36	-0.78
	1.5	-2.17	-2.88	-3.65	-4.53	-5.46	-6.44	0.54	0.58	0.58	0.54	0.46	0.34	0.34	0.34
	4.0	-1.76	-2.18	-2.64	-3.15	-3.67	-4.18	0.55	0.58	0.58	0.54	0.46	0.34	0.34	0.34
	7.0	-1.49	-1.79	-2.11	-2.47	-2.81	-3.17	0.48	0.52	0.52	0.57	0.50	0.54	0.59	0.62
	10.0	-1.21	-1.43	-1.63	-1.91	-2.17	-2.43	0.41	0.45	0.48	0.51	0.54	0.59	0.62	0.65
	15.0	-1.02	-1.18	-1.34	-1.53	-1.71	-1.89	0.34	0.36	0.43	0.50	0.54	0.59	0.63	0.65
	20.0	-0.86	-0.98	-1.11	-1.26	-1.39	-1.53	0.29	0.31	0.36	0.41	0.46	0.51	0.54	0.57
	30.0	-0.77	-0.85	-0.92	-1.01	-1.06	-1.12	0.19	0.23	0.30	0.35	0.40	0.45	0.48	0.51
	40.0	-0.63	-0.69	-0.73	-0.77	-0.80	-0.80	0.16	0.20	0.25	0.30	0.33	0.36	0.37	0.38
	50.0	-0.51	-0.54	-0.55	-0.57	-0.55	-0.54	0.15	0.19	0.23	0.26	0.30	0.34	0.34	0.34
	60.0	-0.38	-0.41	-0.40	-0.38	-0.36	-0.38	0.15	0.19	0.21	0.22	0.24	0.26	0.27	0.28
	70.0	-0.28	-0.28	-0.29	-0.21	-0.22	-0.29	0.15	0.16	0.19	0.21	0.22	0.22	0.23	0.23
	80.0	-0.15	-0.14	-0.11	-0.11	-0.15	-0.26	0.10	0.10	0.11	0.11	0.11	0.11	0.11	0.11
	90.0	-0.01	-0.01	-0.04	-0.09	-0.19	-0.36	0.09	0.08	0.08	0.08	0.08	0.08	0.08	0.08
	95.0	0.04	0.01	0.01	-0.03	-0.19	-0.36	0.09	0.08	0.08	0.08	0.08	0.08	0.08	0.08
0.375 b/2	0	-1.01	-1.93	-3.02	-4.34	-5.80	-7.45	---	---	0.52	0.39	0.19	-0.08	-0.41	-0.80
	1.5	-2.48	-3.26	-4.11	-5.08	-6.10	-7.17	0.52	0.57	0.56	0.53	0.46	0.34	0.34	0.34
	4.0	-1.75	-2.18	-2.64	-3.15	-3.65	-4.14	0.54	0.57	0.56	0.59	0.54	0.59	0.60	0.60
	7.0	-1.53	-1.86	-2.18	-2.53	-2.87	-3.20	0.48	0.51	0.51	0.56	0.54	0.59	0.60	0.61
	10.0	-1.33	-1.58	-1.83	-2.09	-2.34	-2.58	0.41	0.45	0.48	0.51	0.56	0.59	0.60	0.61
	15.0	-1.13	-1.31	-1.49	-1.68	-1.84	-1.96	0.36	0.37	0.44	0.49	0.54	0.57	0.57	0.57
	20.0	-0.98	-1.12	-1.25	-1.40	-1.51	-1.59	0.29	0.32	0.37	0.43	0.49	0.53	0.53	0.53
	30.0	-0.72	-0.80	-0.88	-0.96	-1.02	-1.03	0.19	0.25	0.30	0.35	0.40	0.44	0.44	0.44
	40.0	-0.64	-0.69	-0.74	-0.77	-0.74	-0.70	0.16	0.20	0.25	0.29	0.34	0.38	0.38	0.37
	50.0	-0.50	-0.55	-0.56	-0.55	-0.49	-0.47	0.15	0.17	0.20	0.23	0.26	0.27	0.27	0.27
	60.0	-0.39	-0.40	-0.40	-0.36	-0.31	-0.38	0.15	0.17	0.20	0.23	0.26	0.26	0.27	0.27
	70.0	-0.28	-0.27	-0.24	-0.20	-0.21	-0.34	0.15	0.16	0.19	0.20	0.21	0.21	0.21	0.21
	80.0	-0.15	-0.13	-0.10	-0.11	-0.18	-0.34	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10
	90.0	-0.01	-0.02	-0.04	-0.10	-0.22	-0.45	0.09	0.08	0.08	0.09	0.07	0.06	0.06	0.06
	95.0	0.04	0.01	0.01	-0.04	-0.10	-0.28	0.09	0.08	0.08	0.08	0.04	0	0.01	0.01
0.44 b/2	0	-0.97	-1.87	-2.94	-4.19	-5.53	-6.96	---	---	0.53	0.37	0.13	-0.19	-0.37	-1.18
	1.5	-2.43	-3.17	-3.96	-4.85	-5.72	-6.98	0.54	0.58	0.57	0.53	0.46	0.36	0.36	0.36
	4.0	-1.79	-2.28	-2.70	-3.20	-3.69	-4.12	0.54	0.58	0.57	0.53	0.46	0.36	0.36	0.36
	7.0	-1.56	-1.87	-2.21	-2.56	-2.88	-3.15	0.48	0.51	0.52	0.51	0.46	0.36	0.36	0.36
	10.0	-1.37	-1.62	-1.87	-2.13	-2.37	-2.57	0.41	0.46	0.44	0.49	0.54	0.57	0.57	0.57
	15.0	-1.14	-1.31	-1.50	-1.66	-1.82	-1.91	0.36	0.37	0.44	0.49	0.54	0.57	0.57	0.57
	20.0	-0.98	-1.11	-1.24	-1.38	-1.47	-1.51	0.26	0.26	0.38	0.44	0.48	0.52	0.52	0.52
	30.0	-0.79	-0.89	-0.96	-1.00	-1.03	-1.09	0.19	0.20	0.25	0.30	0.33	0.39	0.43	0.43
	40.0	-0.63	-0.69	-0.73	-0.74	-0.69	-0.62	0.16	0.15	0.19	0.22	0.26	0.33	0.36	0.36
	50.0	-0.50	-0.54	-0.54	-0.52	-0.44	-0.47	0.15	0.17	0.20	0.22	0.24	0.26	0.30	0.30
	60.0	-0.38	-0.40	-0.39	-0.34	-0.29	-0.43	0.15	0.17	0.20	0.22	0.24	0.26	0.30	0.30
	70.0	-0.27	-0.27	-0.23	-0.19	-0.23	-0.42	0.15	0.17	0.19	0.20	0.21	0.21	0.21	0.21
	80.0	-0.15	-0.13	-0.10	-0.12	-0.21	-0.42	0.10	0.10	0.10	0.10	0			

TABLE V. - PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING.
 $M_\infty = 0.25$; $R = 8,000,000$ - Concluded
 (b) α_u , $10^\circ, 12^\circ, 14^\circ, 16^\circ, 18^\circ, 20^\circ$ - Concluded

Spanwise station	Percent chord	Upper surface						Lower surface						
		Angle of attack						Angle of attack						
		10°	12°	14°	16°	18°	20°	10°	12°	14°	16°	18°	20°	
0.56 b/2	0	-1.20	-2.19	-3.36	-4.63	-5.87	-6.91	---	0.32	0.36	0.11	-0.20	-0.52	-0.80
	1.5	-2.41	-3.15	-3.92	-4.73	-5.47	-5.87	---	.55	.58	.58	.54	.49	.44
	4.0	-1.83	-2.28	-2.75	-3.22	-3.61	-3.72	---	---	---	---	---	---	---
	7.0	-1.57	-1.90	-2.23	-2.55	-2.78	-2.74	---	.38	.46	.51	.55	.59	.61
	10.0	-1.38	-1.64	-1.89	-2.12	-2.28	-2.16	---	.30	.38	.44	.49	.53	.56
	15.0	-1.15	-1.33	-1.51	-1.66	-1.73	-1.57	---	.26	.33	.38	.44	.47	.51
	20.0	-.96	-1.09	-1.22	-1.32	-1.35	-1.14	---	.20	.29	.30	.33	.38	.41
	30.0	-.76	-.84	-.90	-.94	-.88	-.89	---	.17	.21	.26	.29	.32	.34
	40.0	-.68	-.68	-.71	-.69	-.55	-.75	---	.16	.19	.22	.25	.27	.27
	50.0	-.50	-.54	-.54	-.48	-.37	-.67	---	---	---	---	---	---	---
	60.0	-.38	-.40	-.37	-.29	-.30	-.60	---	---	---	---	---	---	---
	70.0	-.27	-.26	-.21	-.18	-.28	-.29	---	.15	.16	.18	.19	.16	---
	80.0	-.15	-.13	-.10	-.13	-.28	-.60	---	.14	.15	.15	.13	.09	---
	90.0	-.01	-.01	-.04	-.12	-.30	-.56	---	.11	.10	.09	.08	.03	-.02
	95.0	.04	.01	-.04	-.13	-.30	-.46	---	.10	.08	.06	.03	-.04	-.11
0.68 b/2	0	---	---	---	---	---	---	---	---	---	---	---	---	---
	1.5	-2.27	-3.01	-3.63	-4.37	-4.79	-4.65	---	.54	.41	.21	-.04	-.24	.14
	4.0	-1.78	-2.23	-2.68	-3.11	-3.29	-3.02	---	.54	.57	.58	.56	.53	.61
	7.0	-1.49	-1.81	-2.12	-2.40	-2.43	-.87	---	---	---	---	---	---	---
	10.0	-1.32	-1.56	-1.80	-1.93	-2.00	-.84	---	.38	.46	.52	.55	.58	.59
	15.0	-1.09	-1.27	-1.44	-1.56	-1.49	-.75	---	.30	.37	.43	.48	.51	.52
	20.0	-.95	-1.08	-1.20	-1.26	-1.14	-.72	---	.28	.38	.38	.42	.45	.45
	30.0	-.73	-.85	-.91	-.90	-.66	-.68	---	.19	.25	.30	.34	.36	.35
	40.0	-.60	-.66	-.69	-.64	-.45	-.69	---	.17	.21	.25	.28	.30	.27
	50.0	-.49	-.52	-.51	-.42	-.40	-.71	---	---	---	---	---	---	---
	60.0	-.36	-.38	-.35	-.24	-.37	-.80	---	.15	.17	.20	.21	.20	.16
	70.0	-.27	-.29	-.20	-.16	-.36	-.77	---	.14	.15	.17	.15	.10	---
	80.0	-.15	-.13	-.09	-.13	-.37	-.73	---	.13	.14	.15	.13	.09	.02
	90.0	-.01	-.01	-.05	-.12	-.39	-.61	---	.11	.11	.09	.07	0	---
	95.0	.05	.01	-.03	-.13	-.58	-.09	---	.07	.05	0	-.10	-.24	---
0.80 b/2	0	-1.08	-2.07	-3.21	-4.30	-4.45	-2.04	---	---	---	---	---	---	---
	1.5	-2.22	-2.97	-3.55	-4.18	-3.97	-1.62	---	.58	.49	.32	.13	.09	.40
	4.0	-1.61	-2.04	-2.47	-2.81	-2.55	-.64	---	.51	.57	.58	.58	.58	.62
	7.0	-1.38	-1.69	-1.99	-2.21	-1.85	-.53	---	---	---	---	---	---	---
	10.0	-1.22	-1.47	-1.70	-1.85	-1.45	-.49	---	.35	.45	.50	.54	.56	.54
	15.0	-1.04	-1.21	-1.38	-1.47	-1.00	-.49	---	.27	.36	.41	.46	.48	.42
	20.0	-.90	-1.03	-1.15	-1.19	-.80	-.47	---	.24	.30	.36	.40	.42	.37
	30.0	-.68	-.77	-.83	-.82	-.63	-.45	---	.18	.23	.29	.32	.32	---
	40.0	-.57	-.63	-.66	-.59	-.56	-.46	---	---	---	---	---	---	---
	50.0	-.46	-.50	-.50	-.38	-.53	-.44	---	.14	.17	.20	.22	.20	.15
	60.0	-.35	-.37	-.35	-.23	-.49	-.45	---	.14	.16	.19	.16	.16	.11
	70.0	-.25	-.26	-.21	-.15	-.49	-.44	---	.13	.15	.16	.16	.11	.06
	80.0	-.15	-.14	-.09	-.12	-.48	-.43	---	.12	.13	.13	.11	.04	0
	90.0	0	-.01	-.04	-.11	-.48	-.40	---	.11	.11	.10	.06	-.04	-.10
	95.0	.05	.02	-.02	-.11	-.42	-.40	---	.10	.08	.08	.02	-.10	-.16
0.94 b/2	0	-.46	-1.30	-2.30	-3.16	-1.79	-1.62	---	---	---	---	---	---	---
	1.5	-1.71	-2.12	-2.73	-3.39	-1.81	-1.61	---	.57	.55	.44	.31	.47	.48
	4.0	-1.31	-1.70	-2.10	-2.38	-1.17	-.99	---	---	---	---	---	---	---
	7.0	-1.16	-1.45	-1.72	-1.90	-1.69	-.92	---	.57	.46	.32	.25	.22	.23
	10.0	-1.00	-1.22	-1.43	-1.54	-1.46	-.36	---	.29	.38	.44	.49	.48	.46
	20.0	-.74	-.86	-.96	-1.00	-1.00	-.36	---	.34	.21	.29	.32	.30	.29
	30.0	-.54	-.62	-.68	-.68	-.54	-.32	---	.12	.17	.21	.24	.21	.20
	40.0	-.47	-.52	-.55	-.50	-.34	-.31	---	.10	.12	.16	.17	.15	.13
	50.0	-.38	-.41	-.42	-.33	-.33	-.30	---	.09	.11	.13	.14	.11	.09
	60.0	-.29	-.31	-.31	-.21	-.33	-.30	---	---	---	---	---	---	---
	70.0	-.21	-.22	-.20	-.11	-.31	-.29	---	.08	.09	.09	.08	.08	0
	80.0	-.12	-.12	-.09	-.06	-.30	-.26	---	.08	.08	.08	.06	-.01	-.02
	90.0	0	0	0	-.05	-.28	-.26	---	.08	.07	.06	.03	-.06	-.09
	95.0	.05	.05	.03	-.04	-.28	-.26	---	.08	.06	.05	0	-.15	-.15

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TABLE VI. - PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING.
 $M_\infty = 0.25$; $R = 2,000,000$
(a) $\alpha_u = -2^\circ, 0^\circ, 2^\circ, 4^\circ, 6^\circ, 8^\circ$

Spanwise station	Percent chord	Upper surface					Lower surface				
		Angle of attack					Angle of attack				
		-2°	0°	2°	4°	6°	-2°	0°	2°	4°	6°
0.10 b/2	0	0.21	0.44	0.55	0.56	0.46	0.25	-	-	-	-
	1.5	.33	.16	-.07	-.34	-.57	-1.05	-0.55	-0.20	0.06	-0.30
	4.0	.12	-.05	-.24	-.46	-.71	-.97	-.59	-.34	-.11	0.09
	7.0	-.01	-.16	-.32	-.50	-.70	-.91	-	-	-	-
	10.0	-.07	-.20	-.34	-.49	-.65	-.82	-.49	-.33	-.17	0.03
	15.0	-.13	-.25	-.35	-.48	-.61	-.75	-.43	-.30	-.18	0.06
	20.0	-.16	-.26	-.36	-.46	-.58	-.65	-.38	-.27	-.17	0.03
	30.0	-.19	-.27	-.34	-.43	-.48	-.56	-.29	-.23	-.14	0.02
	40.0	-.18	-.24	-.30	-.36	-.41	-.47	-.23	-.16	-.11	0.02
	50.0	-.16	-.23	-.27	-.30	-.35	-.40	-.17	-.12	-.07	0.01
	60.0	-.15	-.20	-.25	-.27	-.30	-.33	-.12	-.08	-.03	0.00
	70.0	-.14	-.18	-.20	-.23	-.26	-.28	-.06	-.03	0.01	0.00
	80.0	-.12	-.14	-.15	-.17	-.18	-.19	-	-	-	0.00
	90.0	-.02	-.03	-.03	-.04	-.05	-.05	0.02	0.03	0.04	0.05
	95.0	.03	.03	.03	.03	.03	.01	.04	.05	.05	.08
0.19 b/2	0	.14	.44	.56	.50	.31	-.06	-	-	-	-
	1.5	.39	.18	.08	-.46	-.91	-1.43	-.74	-.29	0.05	.48
	4.0	.14	-.06	-.29	-.58	-.89	-1.23	-.68	-.37	-.11	.29
	7.0	-.01	-.17	-.37	-.59	-.83	-1.09	-	-	-	-
	10.0	-.08	-.24	-.41	-.61	-.81	-1.02	-.53	-.34	-.17	.21
	15.0	-.14	-.28	-.42	-.58	-.74	-.84	-.46	-.31	-.18	.16
	20.0	-.19	-.30	-.42	-.55	-.68	-.74	-.35	-.26	-.17	.06
	30.0	-.22	-.33	-.39	-.49	-.54	-.65	-.28	-.22	-.13	.08
	40.0	-.23	-.29	-.36	-.42	-.48	-.54	-.20	-.14	-.10	.04
	50.0	-.21	-.27	-.32	-.34	-.40	-.44	-	-	-	-
	60.0	-.18	-.24	-.28	-.29	-.33	-.35	-.09	-.05	0.01	.06
	70.0	-.16	-.19	-.21	-.24	-.25	-.27	-.03	0	0.03	.08
	80.0	-.12	-.14	-.16	-.16	-.17	-.16	-	-	-	-
	90.0	-.04	-.04	-.04	-.04	-.03	-.02	0.03	.06	0.07	.08
	95.0	.03	.03	.04	.04	.03	.03	.08	.08	.08	.07
0.31 b/2	0	.08	.42	.55	.48	.21	-.25	-	-	-	-
	1.5	.39	.18	-.13	-.54	-.61	-1.61	-.76	-.27	.10	.51
	4.0	.13	-.03	-.36	-.67	-.81	-1.40	-.71	-.36	-.08	.34
	7.0	0	-.19	-.41	-.66	-.93	-1.24	-	-	-	-
	10.0	-.07	-.24	-.43	-.64	-.86	-1.05	-.54	-.34	-.15	.26
	15.0	-.15	-.30	-.45	-.65	-.80	-.94	-.47	-.20	-.17	.08
	20.0	-.19	-.31	-.44	-.68	-.73	-.84	-.34	-.26	-.14	.15
	30.0	-.22	-.31	-.41	-.51	-.58	-.68	-.27	-.20	-.12	.08
	40.0	-.23	-.30	-.37	-.43	-.51	-.60	-.20	-.12	-.06	.03
	50.0	-.21	-.27	-.34	-.37	-.42	-.46	-.12	-.07	0.01	.03
	60.0	-.19	-.24	-.26	-.30	-.34	-.35	-	-	-	-
	70.0	-.17	-.20	-.22	-.25	-.26	-.26	-.01	0.01	0.04	.11
	80.0	-.13	-.15	-.16	-.17	-.17	-.15	-	-	-	-
	90.0	-.04	-.03	-.03	-.04	-.03	-.01	0.03	0.07	0.08	.08
	95.0	.03	.03	.04	.04	.03	.03	.08	.08	.09	.08
0.375 b/2	0	.05	.42	.55	.48	.17	-.35	-	-	-	-
	1.5	.38	.15	-.20	-.65	-.70	-1.82	-.74	-.25	.11	.37
	4.0	.17	-.06	-.33	-.64	-.80	-1.40	-.70	-.36	-.07	.16
	7.0	-.01	-.20	-.43	-.68	-.96	-1.24	-	-	-	-
	10.0	-.07	-.23	-.45	-.67	-.89	-1.07	-.52	-.32	-.14	.08
	15.0	-.14	-.30	-.46	-.63	-.81	-.96	-.45	-.20	-.15	.10
	20.0	-.18	-.32	-.45	-.65	-.74	-.85	-.32	-.23	-.13	.07
	30.0	-.20	-.30	-.41	-.51	-.54	-.66	-.25	-.19	-.11	.05
	40.0	-.22	-.30	-.37	-.43	-.50	-.56	-.18	-.11	-.07	.03
	50.0	-.20	-.27	-.32	-.35	-.41	-.45	-	-	-	-
	60.0	-.18	-.23	-.25	-.29	-.32	-.35	-.06	-.03	0.01	.03
	70.0	-.16	-.20	-.21	-.24	-.26	-.29	0	0.02	0.05	.08
	80.0	-.12	-.14	-.15	-.16	-.16	-.14	-	-	-	-
	90.0	-.02	-.04	-.04	-.03	-.02	-.01	0.07	0.07	0.08	.08
	95.0	.04	.04	.04	.05	.05	.03	.09	.09	.10	.09
0.44 b/2	0	.03	.42	.56	.48	.19	-.32	-	-	-	-
	1.5	.38	.14	-.20	-.64	-.78	-1.78	-.80	-.27	.13	.40
	4.0	.17	-.06	-.34	-.67	-.93	-1.44	-.73	-.38	-.08	.16
	7.0	-.03	-.19	-.42	-.68	-.97	-1.28	-	-	-	-
	10.0	-.05	-.24	-.45	-.67	-.90	-1.10	-.53	-.32	-.14	.09
	15.0	-.12	-.29	-.46	-.63	-.83	-.96	-.42	-.30	-.15	.10
	20.0	-.17	-.30	-.44	-.58	-.73	-.85	-.33	-.23	-.13	.06
	30.0	-.20	-.30	-.41	-.51	-.59	-.69	-.23	-.18	-.10	.03
	40.0	-.20	-.29	-.37	-.44	-.49	-.56	-.18	-.11	-.07	0.00
	50.0	-.19	-.26	-.32	-.39	-.41	-.45	-.10	-.06	-.01	.03
	60.0	-.18	-.24	-.25	-.30	-.33	-.39	-.05	-.02	0.02	.06
	70.0	-.15	-.20	-.20	-.21	-.25	-.28	0.01	0.03	0.06	.12
	80.0	-.11	-.13	-.15	-.15	-.16	-.13	-	-	-	-
	90.0	-.01	-.02	-.02	-.02	-.01	-.01	0.07	0.07	0.06	.08
	95.0	.03	.03	.05	.06	.06	.03	.09	.09	.09	.07

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TABLE VI.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING.
 $M_\infty = 0.25$; $R = 2,000,000$ - Continued
(a) $\alpha_u = -2^\circ, 0^\circ, 2^\circ, 4^\circ, 6^\circ, 8^\circ$ - Concluded

Spanwise station	Percent chord	Upper surface						Lower surface					
		Angle of attack						Angle of attack					
		-2°	0°	2°	4°	6°	8°	-2°	0°	2°	4°	6°	8°
0.56 b/2	0	0.02	0.42	0.56	0.46	0.11	-0.47	---	---	---	0.38	0.53	0.56
	1.5	.44	.20	-.13	-.58	-1.13	-1.75	-0.93	-0.35	0.09	0.38	0.53	0.47
	4.0	.20	-.03	-.31	-.65	-1.03	-1.14	-.74	-.38	-.08	.16	.35	-.17
	7.0	.03	-.16	-.41	-.67	-.97	-1.29	---	---	---	---	---	---
	10.0	-.03	-.22	-.43	-.66	-.90	-1.09	-.55	-.33	-.14	.63	.17	.29
	15.0	-.10	-.27	-.44	-.61	-.81	-.95	-.43	-.30	-.15	.01	.10	.21
	20.0	-.12	-.27	-.41	-.56	-.71	-.81	-.33	-.25	-.12	-.01	.09	.18
	30.0	-.17	-.28	-.38	-.49	-.56	-.66	-.23	-.17	-.09	-.01	.06	.13
	40.0	-.18	-.27	-.35	-.42	-.48	-.55	-.17	-.10	-.05	-.01	.07	.12
	50.0	-.18	-.25	-.31	-.35	-.41	-.45	-.10	-.06	-.01	.03	.07	.11
	60.0	-.16	-.22	-.23	-.28	-.32	-.34	---	---	---	---	---	---
	70.0	-.15	-.19	-.20	-.23	-.25	-.29	-.01	.03	.05	.08	.10	.12
	80.0	-.11	-.13	-.15	-.15	-.16	-.13	-.05	.06	.08	.10	.11	.12
	90.0	-.02	-.03	-.03	-.02	-.02	0	-.08	.08	.09	.10	.10	.09
	95.0	.03	.05	.06	.06	.06	.04	.11	.11	.11	.10	.08	.08
0.68 b/2	0	-.26	.27	.53	.53	.29	-.18	---	---	---	---	---	---
	1.5	.48	.28	-.03	-.46	-.99	-1.61	-.06	-.46	-.01	.32	.50	.57
	4.0	.23	0	-.27	-.62	-.90	-1.42	-.84	-.46	-.13	.32	.46	---
	7.0	.10	-.11	-.39	-.62	-.92	-1.29	---	---	---	---	---	---
	10.0	.01	-.18	-.38	-.61	-.85	-1.06	-.52	-.37	-.16	.01	.16	.28
	15.0	-.06	-.22	-.39	-.57	-.76	-.88	-.46	-.32	-.16	-.02	.10	.20
	20.0	-.11	-.25	-.39	-.55	-.70	-.81	-.36	-.23	-.13	-.02	.08	.17
	30.0	-.14	-.25	-.35	-.47	-.53	-.65	-.26	-.17	-.09	-.01	.06	.13
	40.0	-.16	-.24	-.33	-.41	-.46	-.53	-.18	-.12	-.05	-.01	.05	.10
	50.0	-.16	-.22	-.29	-.33	-.39	-.43	---	---	---	---	---	---
	60.0	-.14	-.19	-.24	-.26	-.30	-.33	-.03	-.02	-.02	.04	.07	.11
	70.0	-.13	-.17	-.18	-.21	-.23	-.24	-.01	.01	.04	.07	.09	.11
	80.0	-.10	-.14	-.13	-.15	-.17	-.14	-.04	.03	.07	.09	.10	.11
	90.0	-.02	-.01	-.02	-.02	-.02	0	-.07	.07	.09	.09	.09	.08
	95.0	.03	.05	.03	.05	.07	.04	.09	.10	.10	.09	.09	.08
0.80 b/2	0	-.18	.35	.57	.58	.21	-.36	---	---	---	---	---	---
	1.5	.49	.30	0	-.43	-.93	-1.56	-.27	-.62	-.10	.26	.48	.57
	4.0	.29	.08	-.19	-.52	-.87	-1.26	-.31	-.55	-.21	.06	.27	---
	7.0	.16	-.04	-.25	-.54	-.82	-1.13	---	---	---	---	---	---
	10.0	.07	-.11	-.31	-.54	-.77	-1.03	-.60	-.41	-.20	-.03	.13	.25
	15.0	-.02	-.18	-.34	-.53	-.71	-.85	-.49	-.35	-.19	-.05	.07	.18
	20.0	-.07	-.21	-.34	-.49	-.65	-.76	-.38	-.26	-.15	-.04	.06	.15
	30.0	-.10	-.21	-.31	-.42	-.51	-.60	-.27	-.18	-.12	-.03	.04	.11
	40.0	-.13	-.21	-.29	-.38	-.43	-.50	---	---	---	---	---	---
	50.0	-.14	-.21	-.27	-.33	-.36	-.41	-.12	-.08	-.02	0	.05	.09
	60.0	-.13	-.18	-.23	-.26	-.29	-.32	-.03	-.02	-.01	.03	.07	.09
	70.0	-.11	-.16	-.18	-.20	-.23	-.23	0	-.02	-.03	.06	.08	.10
	80.0	-.09	-.12	-.12	-.14	-.15	-.18	-.03	-.03	-.06	.08	.09	.10
	90.0	-.02	-.01	-.01	-.02	-.02	0	-.07	.07	.09	.09	.10	.09
	95.0	.03	.05	.06	.05	.03	.02	.10	.10	.10	.10	.09	.09
0.94 b/2	0	-.75	0	.43	.56	.33	.04	---	---	---	---	---	---
	1.5	.51	.36	.13	-.22	-.66	-1.18	-.55	-.91	-.34	.09	.37	.53
	4.0	.36	.18	-.05	-.34	-.67	-1.04	---	---	---	---	---	---
	7.0	.21	.04	-.17	-.41	-.67	-.93	-.74	-.49	-.27	-.06	.12	.26
	10.0	.12	-.04	-.21	-.41	-.62	-.83	-.63	-.45	-.26	-.09	.06	.18
	15.0	.04	-.09	-.23	-.39	-.55	-.73	-.50	-.36	-.22	-.10	.02	.12
	20.0	-.02	-.13	-.25	-.39	-.53	-.61	-.39	-.28	-.19	-.09	.01	.09
	30.0	-.08	-.16	-.23	-.34	-.44	-.48	-.27	-.20	-.13	-.07	0	.06
	40.0	-.10	-.16	-.23	-.30	-.36	-.41	-.17	-.12	-.06	-.04	0	.04
	50.0	-.12	-.16	-.22	-.27	-.39	-.43	-.10	-.05	-.02	-.02	0	.02
	60.0	-.11	-.15	-.19	-.23	-.24	-.27	---	---	---	---	---	---
	70.0	-.10	-.13	-.15	-.16	-.18	-.20	-.01	.02	.04	.05	.07	---
	80.0	-.08	-.10	-.09	-.11	-.11	-.12	-.06	.06	.07	.08	.08	---
	90.0	-.03	.01	.01	0	0	0	-.06	.08	.09	.08	.09	---
	95.0	.07	.06	.06	.06	.06	.06	.11	.11	.11	.10	.09	---

TABLE VI.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING.
 $M_\infty = 0.25$; $R = 2,000,000$ - Continued
(b) $\alpha_u = 10^\circ, 12^\circ, 14^\circ, 16^\circ, 18^\circ, 20^\circ$

Spanwise station	Percent chord	Upper surface						Lower surface					
		Angle of attack						Angle of attack					
		10°	12°	14°	16°	18°	20°	10°	12°	14°	16°	18°	20°
0.10 b/2	0	-0.08	-0.51	-1.02	-1.64	-2.39	-3.16	-	-	-	-	-	-
	1.5	-1.46	-1.94	-2.14	-3.05	-3.79	-4.55	0.65	0.67	0.65	0.59	0.49	0.36
	4.0	-1.27	-1.59	-1.80	-2.16	-2.52	-2.86	.52	.61	.67	.72	.75	.76
	7.0	-1.13	-1.29	-1.53	-1.77	-2.00	-2.26	-	-	-	-	-	-
	10.0	-.94	-1.13	-1.29	-1.48	-1.68	-1.84	.33	.42	.50	.57	.64	.69
	15.0	-.83	-.97	-1.10	-1.28	-1.38	-1.49	.25	.33	.41	.48	.54	.59
	20.0	-.75	-.86	-.96	-1.06	-1.17	-1.29	.21	.27	.36	.42	.48	.53
	30.0	-.63	-.71	-.77	-.84	-.92	-.96	.16	.23	.29	.34	.39	.43
	40.0	-.52	-.58	-.61	-.66	-.71	-.75	.14	.19	.23	.27	.31	.35
	50.0	-.43	-.48	-.51	-.54	-.58	-.61	.14	.18	.23	.27	.31	.35
	60.0	-.36	-.39	-.41	-.43	-.47	-.50	.14	.17	.21	.25	.29	.32
	70.0	-.29	-.31	-.34	-.34	-.37	-.39	.14	.17	.20	.24	.27	.30
	80.0	-.20	-.21	-.21	-.23	-.26	-.29	-	-	-	-	-	-
	90.0	-.05	-.07	-.09	-.11	-.13	-.14	.10	.11	.13	.15	.17	.19
	95.0	0	-.03	-.04	-.05	-.07	-.08	.09	.08	.09	.10	.11	.12
0.19 b/2	0	-.58	-1.27	-2.10	-3.10	-4.29	-5.20	-	-	-	-	-	-
	1.5	-2.02	-2.67	-3.38	-4.05	-5.19	-5.73	.57	.59	.57	.56	.56	.49
	4.0	-1.62	-2.15	-2.16	-2.71	-3.23	-3.69	.52	.57	.68	.59	.61	.64
	7.0	-1.26	-1.37	-1.85	-2.17	-2.49	-2.80	-	-	-	-	-	-
	10.0	-1.20	-1.44	-1.65	-1.90	-2.16	-2.37	.34	.42	.50	.56	.61	.60
	15.0	-1.02	-1.19	-1.34	-1.52	-1.71	-1.86	.26	.34	.42	.48	.55	.54
	20.0	-.88	-1.01	-1.13	-1.27	-1.40	-1.53	.21	.28	.36	.43	.49	.54
	30.0	-.73	-.82	-.89	-.97	-1.05	-1.13	.16	.22	.29	.35	.40	.45
	40.0	-.60	-.66	-.70	-.75	-.80	-.86	.14	.19	.24	.29	.35	.40
	50.0	-.47	-.51	-.53	-.56	-.60	-.67	-	-	-	-	-	-
	60.0	-.37	-.38	-.39	-.41	-.46	-.53	.13	.16	.20	.24	.27	.31
	70.0	-.26	-.26	-.29	-.28	-.35	-.42	.13	.16	.18	.21	.24	.27
	80.0	-.14	-.13	-.14	-.19	-.27	-.34	-	-	-	-	-	-
	90.0	-.03	-.06	-.10	-.16	-.25	-.29	.09	.07	.10	.11	.13	.15
	95.0	0	-.04	-.09	-.16	-.22	-.26	.07	.05	.06	.05	.07	.08
0.31 b/2	0	-.90	-1.72	-2.68	-3.85	-5.22	-6.49	-	-	-	-	-	-
	1.5	-2.25	-2.99	-3.71	-4.71	-5.82	-5.79	.53	.51	.53	.55	.46	.37
	4.0	-1.84	-2.06	-2.53	-3.08	-3.60	-3.99	.54	.57	.57	.53	.56	.49
	7.0	-1.43	-1.77	-2.07	-2.41	-2.76	-2.99	-	-	-	-	-	-
	10.0	-1.28	-1.53	-1.75	-2.00	-2.27	-2.42	.36	.44	.51	.56	.59	.62
	15.0	-1.12	-1.29	-1.45	-1.63	-1.85	-1.96	.28	.35	.42	.48	.54	.59
	20.0	-.97	-1.10	-1.22	-1.35	-1.47	-1.50	.23	.30	.37	.43	.49	.54
	30.0	-.76	-.84	-.90	-.97	-1.02	-1.15	.17	.23	.29	.34	.40	.45
	40.0	-.62	-.66	-.69	-.71	-.75	-.89	.16	.19	.24	.29	.33	.38
	50.0	-.48	-.50	-.50	-.49	-.58	-.68	.14	.17	.21	.23	.29	.33
	60.0	-.36	-.36	-.33	-.35	-.47	-.68	-	-	-	-	-	-
	70.0	-.24	-.22	-.21	-.20	-.41	-.48	.13	.14	.16	.18	.21	.23
	80.0	-.12	-.11	-.15	-.24	-.34	-.32	-	-	-	-	-	-
	90.0	-.03	-.07	-.14	-.23	-.33	-.26	.06	.08	.06	.06	.07	.07
	95.0	-.01	-.07	-.14	-.28	-.32	-.26	.06	.04	.02	0	0	0
0.375 b/2	0	-.104	-1.93	-2.96	-4.21	-4.67	-6.80	-	-	-	-	-	-
	1.5	-2.47	-3.17	-3.95	-4.94	-6.08	-6.91	.52	.59	.57	.54	.46	.42
	4.0	-1.56	-1.98	-2.35	-2.95	-3.43	-3.68	.54	.57	.57	.54	.46	.42
	7.0	-1.51	-1.82	-2.10	-2.41	-2.71	-2.78	-	-	-	-	-	-
	10.0	-1.33	-1.57	-1.79	-2.03	-2.23	-2.22	.37	.46	.51	.56	.60	.64
	15.0	-1.14	-1.31	-1.45	-1.61	-1.71	-1.99	.29	.37	.43	.49	.54	.59
	20.0	-.99	-1.12	-1.22	-1.32	-1.37	-1.25	.24	.31	.38	.43	.49	.54
	30.0	-.75	-.88	-.87	-.90	-.90	-.108	.18	.24	.30	.35	.40	.45
	40.0	-.62	-.65	-.66	-.65	-.74	-.10	.15	.20	.25	.28	.33	.36
	50.0	-.48	-.48	-.46	-.47	-.69	-.117	-	-	-	-	-	-
	60.0	-.35	-.34	-.31	-.40	-.66	-.122	.13	.15	.18	.21	.24	.25
	70.0	-.24	-.20	-.22	-.38	-.64	-.106	.13	.14	.16	.18	.20	.20
	80.0	-.12	-.12	-.19	-.35	-.58	-.72	-	-	-	-	-	-
	90.0	-.03	-.09	-.19	-.36	-.55	-.51	.07	.07	.05	.05	.06	.03
	95.0	-.02	-.09	-.19	-.34	-.45	-.41	.05	.03	0	-.02	-.01	-.06
0.44 b/2	0	-.102	-1.88	-2.84	-4.00	-5.19	-6.27	-	-	-	-	-	-
	1.5	-2.43	-3.10	-3.85	-4.83	-5.17	-6.16	.49	.55	.57	.54	.49	.43
	4.0	-1.98	-2.06	-2.93	-4.01	-4.36	-5.16	.54	.58	.57	.54	.49	.43
	7.0	-1.54	-1.85	-2.12	-2.40	-2.56	-2.73	-	-	-	-	-	-
	10.0	-1.36	-1.59	-1.79	-1.99	-2.06	-2.13	.38	.46	.52	.56	.60	.64
	15.0	-1.14	-1.31	-1.42	-1.53	-1.46	-1.65	.29	.37	.43	.49	.54	.58
	20.0	-.99	-1.10	-1.18	-1.22	-1.14	-1.66	.25	.32	.38	.43	.49	.51
	30.0	-.78	-.84	-.85	-.78	-.89	-.142	.18	.24	.29	.34	.40	.42
	40.0	-.61	-.63	-.59	-.54	-.82	-.127	.15	.19	.24	.28	.32	.32
	50.0	-.47	-.46	-.38	-.45	-.75	-.118	.15	.18	.21	.24	.26	.26
	60.0	-.34	-.30	-.27	-.42	-.69	-.108	.14	.15	.18	.20	.22	.20
	70.0	-.22	-.18	-.22	-.41	-.68	-.96	.14	.15	.16	.17	.19	.19
	80.0	-.10	-.11	-.22	-.46	-.77	-.88	-	-	-	-	-	-
	90.0	-.03	-.09	-.22	-.36	-.62	-.76	.07	.06	.04	.01	.01	-.10
	95.0	-.02	-.10	-.25	-.48	-.45	-.69	.03	.01	-.03	-.07	-.09	-.24

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TABLE VI.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING.
 M_∞ , 0.25; R, 2,000,000 - Concluded
 (b) α_u , 10°, 12°, 14°, 16°, 18°, 20° - Concluded

Spanwise station	Per-cent chord	Upper surface						Lower surface					
		Angle of attack						Angle of attack					
		10°	12°	14°	16°	18°	20°	10°	12°	14°	16°	18°	20°
0.56 b/2	0	-1.23	-2.14	-3.07	-3.97	-1.93	-0.89	-	-	-	-	-	-
	1.5	-2.42	-3.10	-3.73	-4.39	-1.45	-0.75	0.49	0.35	0.16	-0.06	0.34	0.40
	4.0	-2.05	-2.12	-2.52	-2.76	-1.42	-0.74	.54	.58	.58	.56	.66	.62
	7.0	-1.58	-1.83	-2.05	-2.13	-1.26	-0.72	-	-	-	-	-	-
	10.0	-1.37	-1.58	-1.72	-1.72	-1.27	-0.72	.38	.46	.51	.56	.60	.55
	15.0	-1.14	-1.28	-1.35	-1.22	-1.03	-0.69	.29	.36	.43	.47	.50	.47
	20.0	-0.95	-1.05	-1.07	-0.87	-0.96	-0.69	.26	.34	.37	.42	.44	.41
	30.0	-0.75	-0.79	-0.73	-0.55	-0.81	-0.66	.19	.23	.26	.32	.33	.31
	40.0	-0.60	-0.60	-0.47	-0.52	-0.81	-0.67	.16	.20	.23	.26	.23	.26
	50.0	-0.47	-0.43	-0.31	-0.32	-0.79	-0.67	.14	.18	.20	.21	.20	.18
	60.0	-0.33	-0.30	-0.25	-0.24	-0.77	-0.68	-	-	-	-	-	-
	70.0	-0.22	-0.16	-0.24	-0.24	-0.66	-0.66	.13	.14	.14	.13	.10	.07
0.68 b/2	80.0	-0.09	-0.11	-0.24	-0.59	-0.69	-0.63	.12	.11	.10	.07	.03	0
	90.0	-0.03	-0.10	-0.26	-0.60	-0.80	-0.58	.07	.05	.01	.04	.11	.14
	95.0	-0.01	-0.10	-0.26	-0.50	-0.58	-0.56	.06	.02	.04	.13	.22	.24
	0	-0.86	-1.63	-2.29	-2.43	-0.44	-0.45	-	-	-	-	-	-
	1.5	-2.25	-2.91	-3.42	-3.38	-0.54	-0.53	.52	.41	.29	.26	.49	.46
	4.0	-1.88	-2.12	-2.36	-2.02	-0.52	-0.52	.53	.57	.58	.60	.56	.57
	7.0	-1.43	-1.71	-1.85	-1.41	-0.53	-0.53	-	-	-	-	-	-
	10.0	-1.28	-1.48	-1.55	-1.03	-0.52	-0.52	.37	.45	.49	.52	.46	.48
	15.0	-1.07	-1.20	-1.20	-0.52	-0.52	-0.53	.29	.36	.40	.43	.38	.41
	20.0	-0.94	-1.04	-0.98	-0.47	-0.51	-0.52	.25	.31	.35	.37	.33	.35
	30.0	-0.72	-0.75	-0.62	-0.42	-0.49	-0.53	.18	.23	.26	.26	.23	.26
	40.0	-0.57	-0.56	-0.38	-0.43	-0.49	-0.51	.15	.18	.20	.21	.20	.20
	50.0	-0.44	-0.40	-0.27	-0.42	-0.47	-0.51	-	-	-	-	-	-
	60.0	-0.32	-0.24	-0.24	-0.43	-0.46	-0.49	.14	.19	.14	.12	.11	.12
	70.0	-0.21	-0.14	-0.24	-0.45	-0.45	-0.47	.12	.12	.11	.07	.07	.07
0.80 b/2	80.0	-0.09	-0.10	-0.24	-0.48	-0.43	-0.44	.11	.10	.07	.02	.02	.02
	90.0	-0.01	-0.09	-0.25	-0.46	-0.38	-0.40	.08	.05	-0.01	-0.03	-0.08	-0.09
	95.0	-0.01	-0.08	-0.25	-0.43	-0.37	-0.38	0	-0.08	-0.18	-0.17	-0.18	-0.18
	0	-1.11	-1.93	-2.44	-2.01	-1.44	-1.23	-	-	-	-	-	-
	1.5	-2.18	-2.75	-3.09	-2.48	-1.30	-0.99	.56	.40	.41	.45	.41	.41
	4.0	-1.73	-1.87	-2.00	-1.44	-1.31	-1.07	.51	.56	.57	.58	.57	.57
	7.0	-1.35	-1.59	-1.62	-1.04	-1.16	-0.97	-	-	-	-	-	-
	10.0	-1.21	-1.39	-1.36	-0.75	-1.22	-1.04	.55	.42	.46	.46	.48	.49
	15.0	-1.03	-1.15	-1.07	-0.42	-1.08	-0.96	.26	.33	.37	.37	.40	.41
	20.0	-0.89	-0.96	-0.83	-0.33	-1.13	-1.02	.23	.29	.31	.31	.35	.36
	30.0	-0.68	-0.71	-0.49	-0.30	-0.97	-0.96	.17	.21	.23	.22	.26	.26
	40.0	-0.54	-0.53	-0.30	-0.30	-0.93	-0.94	-	-	-	-	-	-
	50.0	-0.43	-0.38	-0.24	-0.30	-0.73	-0.80	.12	.14	.14	.13	.17	.17
	60.0	-0.32	-0.24	-0.23	-0.29	-0.59	-0.67	.12	.13	.12	.09	.15	.14
	70.0	-0.22	-0.14	-0.22	-0.29	-0.47	-0.57	.12	.12	.09	.07	.12	.10
0.94 b/2	80.0	-0.10	-0.09	-0.22	-0.29	-0.36	-0.48	.11	.09	.05	.01	.08	.04
	90.0	-0.01	-0.07	-0.23	-0.26	-0.28	-0.40	.09	.05	-0.02	-0.06	.02	-.03
	95.0	.01	-.08	-.24	-.26	-.24	-.36	.07	.02	-.06	-.11	-.02	-.09
	0	-.55	-1.19	-1.48	-1.26	-.73	-.64	-	-	-	-	-	-
	1.5	-1.78	-2.56	-2.82	-2.44	-.85	-.69	.56	.54	.51	.52	.53	.53
	4.0	-1.26	-1.59	-1.61	-1.27	-.86	-.70	-	-	-	-	-	-
	7.0	-1.18	-1.39	-1.34	-1.01	-.81	-.66	.37	.45	.48	.47	.51	.52
	10.0	-1.02	-1.18	-1.10	-.75	-.82	-.69	.28	.35	.38	.36	.43	.43
	15.0	-.84	-.95	-.84	-.47	-.78	-.65	.21	.27	.30	.30	.35	.36
	20.0	-.74	-.82	-.67	-.32	-.78	-.65	.16	.21	.23	.23	.28	.29
	30.0	-.56	-.59	-.39	-.22	-.70	-.60	.11	.15	.16	.15	.20	.21
	40.0	-.46	-.46	-.23	-.22	-.69	-.60	.08	.10	.10	.09	.14	.13
	50.0	-.36	-.34	-.16	-.20	-.63	-.56	.07	.09	.08	.07	.10	.09
	60.0	-.27	-.23	-.14	-.20	-.61	-.55	-	-	-	-	-	-
	70.0	-.19	-.13	-.13	-.19	-.54	-.50	.08	.07	.04	.04	.03	.03
	80.0	-.10	-.05	-.12	-.19	-.49	-.46	.08	.06	.02	0	-.01	-.02
	90.0	.01	0	-.11	-.19	-.42	-.40	.07	.05	-.02	-.05	-.07	-.11
	95.0	.05	0	-.12	-.19	-.38	-.38	.07	.03	-.06	-.10	-.17	-.18

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TABLE VII.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING
 $M_\infty = 0.60$; $R = 2,000,000$
(a) α_u , $-4^\circ, -2^\circ, 0^\circ, 2^\circ, 4^\circ, 6^\circ$

Spanwise Station	Percent chord	Upper surface						Lower surface						
		Angle of attack						Angle of attack						
		-4°	-2°	0°	2°	4°	6°	-4°	-2°	0°	2°	4°	6°	
0.10 b/2	0	-0.01	0.27	0.46	0.56	0.60	0.55	---	-0.94	---	-0.21	0.07	0.29	0.47
	1.5	.46	.35	.19	-.01	-.21	-.43	-.69	-.91	-.63	-.37	-.13	.07	.24
	4.0	.27	.14	.01	-.15	-.38	-.50	-.72	---	---	---	---	---	---
	7.0	.13	.01	-.15	-.38	-.50	-.68	---	-.72	-.54	-.36	-.20	-.05	.08
	10.0	.06	-.06	-.21	-.35	-.50	-.68	---	-.60	-.49	-.35	-.21	-.09	.03
	15.0	-.02	-.13	-.25	-.38	-.50	-.65	---	-.53	-.43	-.31	-.20	-.09	.02
	20.0	-.07	-.17	-.26	-.39	-.50	-.62	---	-.43	-.33	-.27	-.18	-.09	0
	30.0	-.11	-.21	-.29	-.38	-.47	-.56	---	-.34	-.26	-.20	-.14	-.07	0
	40.0	-.12	-.19	-.27	-.35	-.41	-.46	---	-.26	-.20	-.14	-.09	-.04	.02
	50.0	-.13	-.18	-.26	-.32	-.35	-.41	---	-.19	-.14	-.09	-.03	0	.04
	60.0	-.12	-.17	-.23	-.26	-.31	-.35	---	-.10	-.07	-.04	0	.04	.07
	70.0	-.12	-.16	-.21	-.24	-.27	-.30	---	---	---	---	---	---	---
0.19 b/2	80.0	-.10	-.13	-.16	-.18	-.23	-.20	---	---	---	---	---	0	0
	90.0	-.01	-.02	-.03	-.03	-.04	-.04	---	0.01	-.02	-.03	-.04	-.06	-.07
	95.0	.05	.04	.04	.04	.03	.02	---	-.05	-.05	-.05	-.05	-.06	-.06
0.31 b/2	0	.20	.19	.45	.57	.56	.41	---	---	---	---	---	---	---
	1.5	.58	.41	.22	-.05	-.39	-.84	---	-.41	-.82	-.34	.02	.29	.47
	4.0	.31	.16	-.04	-.29	-.57	-.92	---	-.20	-.77	-.43	-.15	.08	.27
	7.0	.17	.02	-.17	-.38	-.61	-.88	---	---	---	---	---	---	---
	10.0	.07	-.08	-.25	-.44	-.65	-.88	---	-.76	-.60	-.40	-.22	-.05	.10
	15.0	-.02	-.15	-.30	-.46	-.63	-.81	---	-.65	-.50	-.36	-.22	-.08	.04
	20.0	-.08	-.19	-.33	-.46	-.60	-.76	---	-.55	-.40	-.32	-.20	-.09	.02
	30.0	-.14	-.24	-.34	-.44	-.55	-.63	---	-.41	-.32	-.24	-.16	-.08	0
	40.0	-.16	-.25	-.33	-.41	-.49	-.54	---	-.30	-.24	-.16	-.12	-.05	.00
	50.0	-.15	-.22	-.30	-.36	-.48	-.47	---	---	---	---	---	---	---
	60.0	-.15	-.19	-.26	-.28	-.32	-.36	---	-.13	-.10	-.06	-.02	-.03	.06
	70.0	-.14	-.17	-.21	-.24	-.27	-.26	---	-.06	-.03	-.01	-.02	-.05	.08
0.375 b/2	80.0	-.11	-.13	-.16	-.17	-.20	-.17	---	---	---	---	---	---	---
	90.0	-.02	-.03	-.04	-.03	-.03	-.02	---	-.04	-.01	-.01	0	.04	.07
	95.0	.05	.04	.04	.05	.05	.06	---	-.01	-.06	-.07	-.07	-.08	-.08
0.44 b/2	0	-.40	.10	.44	.57	.53	.31	---	---	---	---	---	---	---
	1.5	.53	.40	.17	-.17	-.63	-.123	---	-.54	-.83	-.29	.10	.36	.51
	4.0	.35	.18	-.04	-.33	-.66	-.107	---	-.32	-.61	-.42	-.11	.13	.32
	7.0	.19	.01	-.21	-.43	-.71	-.103	---	---	---	---	---	---	---
	10.0	.09	-.07	-.26	-.46	-.70	-.96	---	-.79	-.62	-.39	-.19	-.02	.13
	15.0	-.02	-.16	-.33	-.51	-.69	-.90	---	-.67	-.51	-.35	-.20	-.06	.06
	20.0	-.07	-.20	-.34	-.49	-.65	-.83	---	-.54	-.38	-.30	-.17	-.06	.05
	30.0	-.14	-.24	-.35	-.46	-.58	-.65	---	-.39	-.30	-.20	-.14	-.05	.03
	40.0	-.16	-.25	-.34	-.43	-.49	-.56	---	-.28	-.20	-.15	-.10	-.04	.04
	50.0	-.16	-.23	-.31	-.38	-.41	-.46	---	---	---	---	---	0	.06
	60.0	-.15	-.20	-.27	-.29	-.33	-.36	---	---	---	---	---	---	---
	70.0	-.14	-.18	-.22	-.24	-.27	-.27	---	-.04	-.01	-.01	0	.04	.07
0.44 b/2	80.0	-.11	-.14	-.15	-.17	-.17	-.16	---	---	---	---	---	0	.09
	90.0	-.02	-.03	-.04	-.04	-.03	-.02	---	-.01	-.06	-.07	-.07	-.08	-.08
	95.0	.04	.05	.05	.05	.05	.05	---	-.09	-.10	-.10	-.09	-.09	-.08

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TABLE VII.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING.
 $M_\infty = 0.60$; $R = 2,000,000$ - Continued
(a) α_u , $-4^\circ, -2^\circ, 0^\circ, 2^\circ, 4^\circ, 6^\circ$ - Concluded

Spanwise station	Percent chord	Upper surface						Lower surface					
		Angle of attack						Angle of attack					
		-4°	-2°	0°	2°	4°	6°	-4°	-2°	0°	2°	4°	6°
0.56 b/2	0	-0.44	0.08	0.44	0.57	0.51	0.24	---	---	---	---	---	---
	1.5	.56	.45	.23	-.11	-.26	-1.14	-1.79	-1.06	0.40	0.06	0.36	0.53
	4.0	.38	.21	.02	-.38	-.68	-1.12	-1.68	-.87	-.45	-.11	.14	.33
	7.0	.23	.05	-.17	-.44	-.74	-1.09	---	---	---	---	---	---
	10.0	.13	-.04	-.23	-.48	-.74	-1.03	-.84	-.66	-.40	-.19	0	.15
	15.0	.03	-.12	-.30	-.50	-.71	-.94	-.69	-.49	-.35	-.19	-.04	.06
	20.0	-.03	-.15	-.30	-.47	-.64	-.85	-.54	-.40	-.29	-.16	-.04	.07
	30.0	-.08	-.22	-.32	-.44	-.56	-.64	-.39	-.30	-.19	-.13	-.04	.04
	40.0	-.12	-.22	-.31	-.40	-.47	-.55	-.27	-.20	-.13	-.08	-.02	.04
	50.0	-.14	-.22	-.29	-.36	-.40	-.45	-.17	-.12	-.08	-.02	.01	.05
	60.0	-.12	-.19	-.23	-.29	-.32	-.35	---	---	---	---	---	---
	70.0	-.12	-.17	-.22	-.22	-.26	-.26	-.03	0	.02	.03	.08	.08
0.68 b/2	80.0	-.10	-.13	-.14	-.17	-.17	-.15	-.03	.05	.07	.08	.10	.11
	90.0	-.02	-.03	-.03	-.04	-.02	-.01	.07	.08	.09	.09	.09	.09
	95.0	.04	.05	.05	.05	.06	.05	.09	.13	.11	.10	.10	.09
0.80 b/2	0	.02	.01	.01	.01	.01	.02	---	---	---	---	---	---
	1.5	.57	.49	.30	-.01	-.44	-1.00	-1.88	-1.20	-.51	-.01	.31	.50
	4.0	.40	.23	0	-.30	-.67	-1.12	-1.88	-.96	-.52	-.17	.11	.31
	7.0	.26	.09	-.13	-.39	-.70	-1.05	---	---	---	---	---	---
	10.0	.17	0	-.20	-.43	-.69	-.96	-.86	-.58	-.43	-.20	-.01	.14
	15.0	0	-.06	-.08	-.23	-.44	-.65	-.87	-.70	-.52	-.35	-.05	.08
	20.0	0	-.13	-.29	-.45	-.62	-.81	-.75	-.41	-.27	-.17	-.04	.06
	30.0	-.06	-.17	-.29	-.41	-.54	-.60	-.38	-.29	-.20	-.13	-.04	.04
	40.0	-.10	-.18	-.29	-.38	-.47	-.52	-.26	-.20	-.14	-.08	-.02	.04
	50.0	-.12	-.19	-.26	-.34	-.47	-.53	---	---	---	---	---	---
	60.0	-.10	-.16	-.23	-.29	-.30	-.33	-.10	-.06	-.03	.01	.03	.06
	70.0	-.10	-.16	-.20	-.21	-.24	-.29	-.04	-.01	.01	.04	.06	.06
0.94 b/2	80.0	-.09	-.12	-.14	-.16	-.16	-.15	0	.01	.04	.05	.07	.10
	90.0	-.01	-.02	-.02	-.03	-.02	-.01	.05	.07	.08	.08	.09	.09
	95.0	.03	.05	.05	.05	.06	.05	.07	.11	.10	.09	.08	.08



TABLE VII.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING.
 $M_\infty = 0.60$; $R = 2,000,000$ - Continued
 (b) α_u , $8^\circ, 10^\circ, 12^\circ, 14^\circ, 16^\circ, 18^\circ$

Spanwise station	Percent chord	Upper surface						Lower surface					
		Angle of attack						Angle of attack					
		8°	10°	12°	14°	16°	18°	8°	10°	12°	14°	16°	18°
0.10 b/2	0	0.41	0.21	-0.34	-0.27	-0.47	-0.68	0.59	0.68	0.73	0.76	0.78	0.78
	1.5	-0.97	-1.42	-2.07	-2.54	-2.74	-2.84	-0.39	-0.51	-0.61	-0.69	-0.76	-0.81
	4.0	-0.99	-1.31	-1.71	-2.35	-2.63	-2.78	—	—	—	—	—	—
	7.0	-0.95	-1.21	-1.56	-2.01	-2.56	-2.51	—	—	—	—	—	—
	10.0	-0.88	-1.11	-1.19	-1.35	-1.80	-2.23	—	—	—	—	—	—
	15.0	-0.82	-0.90	-1.09	-1.22	-1.33	-1.96	—	—	—	—	—	—
	20.0	-0.72	-0.84	-0.98	-1.09	-1.15	-1.56	—	—	—	—	—	—
	30.0	-0.63	-0.72	-0.82	-0.90	-0.95	-1.17	—	—	—	—	—	—
	40.0	-0.54	-0.60	-0.68	-0.74	-0.80	-0.92	—	—	—	—	—	—
	50.0	-0.47	-0.51	-0.57	-0.62	-0.69	-0.79	—	—	—	—	—	—
	60.0	-0.39	-0.42	-0.47	-0.52	-0.58	-0.68	—	—	—	—	—	—
	70.0	-0.32	-0.34	-0.38	-0.42	-0.47	-0.57	—	—	—	—	—	—
	80.0	-0.21	-0.23	-0.26	-0.30	-0.35	-0.44	—	—	—	—	—	—
	90.0	-0.05	-0.07	-0.10	-0.15	-0.20	-0.27	—	—	—	—	—	—
	95.0	0	-0.02	-0.05	-0.10	-0.16	-0.22	—	—	—	—	—	—
0.19 b/2	0	-1.15	-1.18	-1.51	-1.79	-1.97	-1.15	—	—	—	—	—	—
	1.5	-2.08	-2.39	-2.81	-2.06	-1.82	—	—	—	—	—	—	—
	4.0	-1.33	-1.90	-2.38	-2.35	-2.05	-1.79	—	—	—	—	—	—
	7.0	-1.20	-1.65	-2.42	-2.36	-1.95	-1.74	—	—	—	—	—	—
	10.0	-1.14	-1.31	-1.73	-2.16	-1.92	-1.73	—	—	—	—	—	—
	15.0	-1.04	-1.14	-1.26	-1.93	-1.82	-1.65	—	—	—	—	—	—
	20.0	-0.88	-0.99	-1.13	-1.68	-1.77	-1.63	—	—	—	—	—	—
	30.0	-0.74	-0.83	-0.91	-1.23	-1.59	-1.52	—	—	—	—	—	—
	40.0	-0.61	-0.67	-0.74	-0.84	-1.37	-1.42	—	—	—	—	—	—
	50.0	-0.50	-0.53	-0.57	-0.64	-1.15	-1.29	—	—	—	—	—	—
	60.0	-0.39	-0.40	-0.43	-0.49	-0.91	-1.15	—	—	—	—	—	—
	70.0	-0.28	-0.26	-0.29	-0.34	-0.69	-1.00	—	—	—	—	—	—
	80.0	-0.16	-0.14	-0.16	-0.19	-0.44	-0.81	—	—	—	—	—	—
	90.0	-0.02	-0.06	-0.09	-0.10	-0.28	-0.66	—	—	—	—	—	—
	95.0	0	-0.04	-0.09	-0.07	-0.18	-0.54	—	—	—	—	—	—
0.31 b/2	0	.01	-0.35	-0.64	-0.72	-0.77	-0.85	—	—	—	—	—	—
	1.5	-1.69	-2.23	-2.17	-1.47	-1.21	-1.13	—	—	—	—	—	—
	4.0	-1.57	-2.19	-2.15	-1.87	-1.19	-1.11	—	—	—	—	—	—
	7.0	-1.42	-2.18	-2.12	-1.42	-1.17	-1.07	—	—	—	—	—	—
	10.0	-1.33	-1.39	-1.92	-1.41	-1.16	-1.07	—	—	—	—	—	—
	15.0	-1.07	-1.21	-1.68	-1.34	-1.13	-1.08	—	—	—	—	—	—
	20.0	-0.94	-1.05	-1.49	-1.33	-1.12	-1.04	—	—	—	—	—	—
	30.0	-0.77	-0.83	-1.14	-1.25	-1.06	-0.99	—	—	—	—	—	—
	40.0	-0.63	-0.65	-0.83	-1.20	-1.04	-0.98	—	—	—	—	—	—
	50.0	-0.50	-0.49	-0.60	-1.10	-1.00	-0.95	—	—	—	—	—	—
	60.0	-0.37	-0.35	-0.42	-1.01	-0.97	-0.93	—	—	—	—	—	—
	70.0	-0.26	-0.22	-0.29	-0.89	-0.91	-0.89	—	—	—	—	—	—
	80.0	-0.13	-0.12	-0.18	-0.74	-0.86	-0.84	—	—	—	—	—	—
	90.0	-0.02	-0.07	-0.11	-0.60	-0.76	-0.76	—	—	—	—	—	—
	95.0	0	-0.06	-0.09	-0.09	-0.73	-0.74	—	—	—	—	—	—
0.375 b/2	0	-0.05	-0.43	-0.67	-0.61	-0.64	-0.72	—	—	—	—	—	—
	1.5	-0.99	-2.55	-1.75	-1.07	-0.92	-0.85	—	—	—	—	—	—
	4.0	-1.72	-2.45	-1.76	-1.09	-0.91	-0.83	—	—	—	—	—	—
	7.0	-1.42	-2.31	-1.67	-1.04	-0.87	-0.80	—	—	—	—	—	—
	10.0	-1.25	-1.35	-1.61	-1.03	-0.87	-0.80	—	—	—	—	—	—
	15.0	-1.09	-1.20	-1.50	-0.99	-0.84	-0.77	—	—	—	—	—	—
	20.0	-0.97	-1.05	-1.44	-0.98	-0.83	-0.77	—	—	—	—	—	—
	30.0	-0.75	-0.80	-1.27	-0.92	-0.79	-0.74	—	—	—	—	—	—
	40.0	-0.63	-0.63	-1.08	-0.91	-0.79	-0.75	—	—	—	—	—	—
	50.0	-0.49	-0.46	-0.89	-0.87	-0.77	-0.72	—	—	—	—	—	—
	60.0	-0.37	-0.32	-0.68	-0.85	-0.78	-0.76	—	—	—	—	—	—
	70.0	-0.29	-0.20	-0.52	-0.80	-0.76	-0.74	—	—	—	—	—	—
	80.0	-0.12	-0.12	-0.35	-0.76	-0.74	-0.72	—	—	—	—	—	—
	90.0	-0.03	-0.09	-0.23	-0.67	-0.66	-0.66	—	—	—	—	—	—
	95.0	0	-0.08	-0.18	-0.63	-0.63	-0.63	—	—	—	—	—	—
0.44 b/2	0	-0.01	-0.39	-0.43	-0.33	-0.34	-0.38	—	—	—	—	—	—
	1.5	-2.00	-2.46	-1.31	-0.91	-0.73	-0.62	—	—	—	—	—	—
	4.0	-1.69	-2.33	-1.32	-0.82	-0.67	-0.59	—	—	—	—	—	—
	7.0	-1.55	-2.34	-1.22	-0.79	-0.63	-0.57	—	—	—	—	—	—
	10.0	-1.29	-1.52	-1.17	-0.77	-0.63	-0.57	—	—	—	—	—	—
	15.0	-1.10	-1.15	-1.09	-0.73	-0.60	-0.56	—	—	—	—	—	—
	20.0	-0.97	-1.02	-1.03	-0.72	-0.60	-0.57	—	—	—	—	—	—
	30.0	-0.77	-0.82	-0.96	-0.66	-0.58	-0.57	—	—	—	—	—	—
	40.0	-0.61	-0.59	-0.93	-0.65	-0.59	-0.59	—	—	—	—	—	—
	50.0	-0.48	-0.43	-0.85	-0.63	-0.60	-0.60	—	—	—	—	—	—
	60.0	-0.36	-0.29	-0.79	-0.64	-0.62	-0.61	—	—	—	—	—	—
	70.0	-0.24	-0.18	-0.70	-0.62	-0.60	-0.60	—	—	—	—	—	—
	80.0	-0.11	-0.12	-0.62	-0.62	-0.59	-0.59	—	—	—	—	—	—
	90.0	-0.03	-0.09	-0.51	-0.55	-0.55	-0.56	—	—	—	—	—	—
	95.0	0	-0.01	-0.09	-0.44	-0.53	-0.54	-0.55	—	—	—	—	—

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TABLE VII. - PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING.
 $M_\infty = 0.60$; $R = 2,000,000$ - Concluded
 (b) $\alpha_u = 8^\circ, 10^\circ, 12^\circ, 14^\circ, 16^\circ, 18^\circ$ - Concluded

Spanwise station	Per-cent chord	Upper surface						Lower surface					
		Angle of attack						Angle of attack					
		8°	10°	12°	14°	16°	18°	8°	10°	12°	14°	16°	18°
0.56 b/2	0	-0.16	-0.13	-0.36	-0.23	-0.21	-0.30	---	---	---	---	---	---
	1.5	-1.94	-2.32	-1.12	-0.73	-0.57	-0.52	0.58	0.57	0.58	0.58	0.58	0.57
	4.0	-1.69	-2.28	-1.03	-0.58	-0.48	-0.50	0.49	0.53	0.53	0.53	0.53	0.51
	7.0	-1.58	-2.36	-0.80	-0.51	-0.46	-0.49	---	---	---	---	---	---
	10.0	-1.27	-1.53	-0.73	-0.49	-0.45	-0.49	0.27	0.35	0.35	0.36	0.39	0.42
	15.0	-1.08	-1.13	-0.65	-0.46	-0.45	-0.49	0.19	0.28	0.26	0.27	0.30	0.34
	20.0	-0.92	-0.95	-0.62	-0.45	-0.45	-0.49	0.16	0.22	0.22	0.22	0.25	0.28
	30.0	-0.74	-0.72	-0.53	-0.43	-0.46	-0.49	0.10	0.15	0.14	0.14	0.16	0.19
	40.0	-0.60	-0.54	-0.47	-0.43	-0.46	-0.49	0.09	0.13	0.10	0.10	0.11	0.14
	50.0	-0.47	-0.38	-0.43	-0.43	-0.46	-0.49	0.09	0.11	0.07	0.07	0.08	0.13
	60.0	-0.34	-0.29	-0.42	-0.42	-0.46	-0.49	---	---	---	---	---	---
	70.0	-0.23	-0.16	-0.40	-0.41	-0.46	-0.48	0.10	0.10	0.03	0.01	0.01	0.01
	80.0	-0.10	-0.12	-0.41	-0.41	-0.45	-0.48	0.10	0.09	0.03	0.03	0.04	0.04
	90.0	-0.02	-0.10	-0.38	-0.39	-0.43	-0.47	0.06	0.03	0.11	0.13	0.15	0.16
	95.0	-0.01	-0.10	-0.37	-0.38	-0.42	-0.46	0.05	0.01	0.17	0.19	0.21	0.24
0.68 b/2	0	.02	.02	.03	.01	.01	0	---	---	---	---	---	---
	1.5	-1.70	-2.24	-1.09	-0.80	-0.60	-0.50	.57	.58	.57	.57	.58	.57
	4.0	-1.63	-2.08	-.94	-.65	-.49	-.47	.43	.51	.48	.51	.51	.54
	7.0	-1.47	-2.05	-.62	-.51	-.45	-.45	---	---	---	---	---	---
	10.0	-1.39	-1.42	-.61	-.54	-.45	-.44	.26	.34	.31	.32	.35	.39
	15.0	-0.96	-1.03	-.49	-.46	-.44	-.44	.18	.26	.23	.24	.27	.30
	20.0	-0.91	-0.93	-.48	-.46	-.43	-.44	.14	.21	.18	.18	.21	.23
	30.0	-0.72	-0.69	-.38	-.41	-.42	-.43	.10	.15	.11	.12	.14	.17
	40.0	-0.58	-0.50	-.36	-.41	-.41	-.43	.08	.12	.07	.08	.09	.11
	50.0	-0.46	-0.34	-.32	-.39	-.40	-.42	---	---	---	---	---	---
	60.0	-0.33	-0.21	-.32	-.39	-.42	-.42	.08	.10	.05	.04	.03	.04
	70.0	-0.23	-0.14	-.30	-.37	-.40	-.42	.09	.08	.02	.01	0	0
	80.0	-0.11	-0.10	-.30	-.36	-.40	-.42	.09	.07	-.01	-.02	-.03	-.03
	90.0	-0.01	-0.09	-.26	-.34	-.39	-.40	.07	.02	-.08	-.10	-.14	-.15
	95.0	0	-0.09	-.27	-.33	-.38	-.39	.04	-.02	-.14	-.18	-.22	-.23
0.80 b/2	0	-0.10	-0.43	-0.43	-.58	-.10	-.16	---	---	---	---	---	---
	1.5	-1.73	-2.24	-2.01	-1.89	-.60	-.42	.57	.59	.58	.56	.56	.56
	4.0	-1.46	-2.00	-1.78	-1.66	-.42	-.38	.40	.48	.47	.50	.50	.49
	7.0	-1.31	-1.92	-1.35	-1.19	-.38	-.37	---	---	---	---	---	---
	10.0	-1.22	-1.18	-1.06	-1.15	-.38	-.37	.23	.31	.30	.34	.31	.34
	15.0	-0.98	-1.05	-.90	-.88	-.36	-.37	.16	.23	.22	.24	.23	.26
	20.0	-0.86	-0.90	-.75	-.80	-.37	-.36	.13	.19	.18	.21	.19	.22
	30.0	-0.67	-0.66	-.53	-.61	-.35	-.35	.09	.13	.12	.14	.12	.14
	40.0	-0.55	-0.49	-.39	-.53	-.34	-.34	---	---	---	---	---	---
	50.0	-0.44	-0.36	-.31	-.46	-.33	-.34	.07	.09	.07	.08	.04	.06
	60.0	-0.33	-0.23	-.26	-.42	-.33	-.33	.08	.09	.06	.07	.03	.04
	70.0	-0.24	-0.13	-.22	-.37	-.32	-.33	.08	.08	.06	.06	.01	.01
	80.0	-0.12	-0.08	-.21	-.33	-.32	-.33	.07	.04	.03	.03	-.03	-.04
	90.0	-0.01	-0.07	-.18	-.27	-.30	-.32	.08	.04	-.01	-.11	-.11	-.16
	95.0	.02	-0.07	-.18	-.23	-.30	-.31	.07	-.02	-.14	-.15	-.15	-.16
0.94 b/2	0	-0.18	-0.11	-.28	-.35	-.51	-.56	---	---	---	---	---	---
	1.5	-1.31	-1.95	-2.23	-1.61	-.76	-.126	.52	.57	.57	.57	.55	.54
	4.0	-1.18	-1.81	-2.08	-1.29	-.58	-.113	---	---	---	---	---	---
	7.0	-1.09	-1.21	-1.17	-1.07	-.35	-.101	.25	.34	.37	.47	.41	.44
	10.0	-0.99	-1.08	-1.12	-1.07	-.30	-.103	.17	.25	.28	.31	.33	.36
	15.0	-0.84	-0.90	-.91	-.87	-.03	-.94	.11	.18	.20	.23	.25	.27
	20.0	-0.70	-0.79	-.80	-.82	-.94	-.99	.07	.13	.15	.18	.19	.21
	30.0	-0.55	-0.58	-.56	-.59	-.67	-.87	.04	.08	.09	.11	.11	.13
	40.0	-0.46	-0.45	-.42	-.49	-.54	-.90	.02	.03	.05	.06	.06	.07
	50.0	-0.37	-0.34	-.29	-.36	-.40	-.75	.03	.04	.04	.04	.04	.05
	60.0	-0.28	-0.24	-.19	-.31	-.32	-.69	---	---	---	---	---	---
	70.0	-0.20	-0.14	-.11	-.23	-.25	-.54	.05	.05	.03	.02	.02	.02
	80.0	-0.11	-.05	-.06	-.19	-.20	-.40	.07	.05	.03	0	0	0
	90.0	.01	.01	-.04	-.16	-.16	-.30	.07	.04	.02	-.04	-.04	-.04
	95.0	.06	.03	-.03	-.15	-.14	-.22	.07	.04	-.01	-.07	-.07	-.09

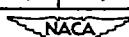

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TABLE VIII.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING.

$M_\infty = 0.80$; $R = 2,000,000$
 (a) $\alpha_u = -4^\circ, -2^\circ, 0^\circ, 2^\circ, 4^\circ, 6^\circ$

Spanwise station	Percent chord	Upper surface						Lower surface					
		Angle of attack						Angle of attack					
		-4°	-2°	0°	2°	4°	6°	-4°	-2°	0°	2°	4°	6°
0.10 b/2	0	0.19	0.37	0.51	0.60	0.65	0.64	---	---	---	---	---	---
	1.5	.47	.37	.23	.07	-.14	-.37	-.71	-.42	-.15	0.08	0.30	0.46
	4.0	.27	.15	0	-.15	-.34	-.56	-.88	-.60	-.33	-.13	.07	.23
	7.0	.14	.02	-.13	-.26	-.45	-.67	-.77	-.57	-.39	-.21	-.09	-.08
	10.0	.06	-.05	-.19	-.33	-.48	-.66	-.77	-.57	-.40	-.24	-.16	---
	15.0	-.02	-.13	-.29	-.37	-.51	-.69	-.75	-.56	-.40	-.23	-.16	0.02
	20.0	-.07	-.17	-.29	-.32	-.44	-.69	-.67	-.56	-.36	-.23	-.16	0.01
	30.0	-.13	-.21	-.32	-.31	-.42	-.67	-.54	-.46	-.34	-.20	-.16	0.01
	40.0	-.14	-.21	-.31	-.39	-.50	-.63	-.42	-.32	-.23	-.17	-.08	-.01
	50.0	-.15	-.21	-.30	-.38	-.44	-.55	-.33	-.25	-.18	-.13	-.05	.01
	60.0	-.14	-.19	-.27	-.38	-.48	-.55	-.23	-.17	-.12	-.06	-.02	.02
	70.0	-.15	-.19	-.24	-.29	-.34	-.38	-.13	-.09	-.05	-.01	-.03	.07
	80.0	-.13	-.15	-.20	-.21	-.24	-.26	---	---	---	---	---	---
	90.0	-.01	-.01	-.03	-.03	-.04	-.04	0	.02	.02	.04	.06	.07
	95.0	.05	.05	.04	.04	.04	.01	.05	.05	.04	.03	.06	.05
0.19 b/2	0	.06	.28	.47	.58	.59	.53	---	---	---	---	---	---
	1.5	.52	.42	.29	.04	-.24	-.58	-.108	-.76	-.35	.01	.26	.45
	4.0	.30	.16	.02	-.23	-.30	-.83	-.124	-.92	-.50	-.19	.06	.23
	7.0	.16	.03	-.13	-.34	-.57	-.84	---	---	---	---	---	---
	10.0	.05	-.08	-.25	-.44	-.66	-.90	-.117	-.74	-.48	-.26	-.08	0.06
	15.0	-.04	-.15	-.31	-.49	-.68	-.96	-.110	-.67	-.44	-.27	.11	0.02
	20.0	-.10	-.21	-.35	-.51	-.69	-.92	-.117	-.57	-.50	-.23	-.11	0.02
	30.0	-.17	-.26	-.39	-.51	-.66	-.88	-.146	-.38	-.30	-.20	-.15	0.02
	40.0	-.19	-.27	-.39	-.49	-.61	-.82	-.134	-.28	-.20	-.15	0.07	0.02
	50.0	-.19	-.25	-.35	-.44	-.50	-.74	---	---	---	---	---	---
	60.0	-.18	-.22	-.31	-.35	-.40	-.60	-.13	-.11	-.08	-.03	-.03	0.05
	70.0	-.17	-.20	-.26	-.27	-.29	-.30	-.06	-.04	-.01	-.02	-.06	0.08
	80.0	-.18	-.14	-.17	-.19	-.18	-.18	---	---	---	---	---	---
	90.0	-.01	-.02	-.03	-.03	-.02	0	.05	.06	.07	.07	.09	.08
	95.0	.05	.06	.06	.06	.07	.05	.06	.09	.09	.10	.10	.08
0.31 b/2	0	-.01	.22	.45	.58	.58	.48	---	---	---	---	---	---
	1.5	.53	.43	.24	0	-.33	-.69	-.109	-.81	-.35	.04	.31	.48
	4.0	.30	.16	-.03	-.31	-.63	-.99	-.119	-.105	-.52	.16	.11	.29
	7.0	.16	.02	-.19	-.42	-.73	-.106	---	---	---	---	---	---
	10.0	.07	-.07	-.26	-.49	-.75	-.106	-.116	-.84	-.49	-.23	-.04	0.10
	15.0	-.04	-.18	-.36	-.58	-.84	-.116	-.97	-.62	-.44	-.23	-.09	.03
	20.0	-.11	-.22	-.39	-.57	-.82	-.115	-.78	-.45	-.38	-.21	-.08	0.03
	30.0	-.17	-.26	-.46	-.72	-.72	-.109	-.53	-.35	-.24	-.17	-.06	.01
	40.0	-.19	-.27	-.46	-.50	-.60	-.72	-.73	-.24	-.18	-.13	-.04	0.08
	50.0	-.20	-.23	-.35	-.44	-.44	-.45	-.20	-.15	-.10	-.04	0	0.03
	60.0	-.18	-.22	-.31	-.31	-.35	-.36	---	---	---	---	---	---
	70.0	-.17	-.19	-.26	-.26	-.26	-.28	-.04	-.03	-.01	0.05	0.06	0.08
	80.0	-.13	-.14	-.17	-.18	-.17	-.16	---	---	---	---	---	---
	90.0	-.02	-.01	-.03	-.03	0	.01	.06	.07	.08	.09	.09	.09
	95.0	.05	.06	.06	.06	.07	.06	.09	.10	.11	.11	.10	.09
0.375 b/2	0	-.05	.19	.45	.59	.58	.46	---	---	---	---	---	---
	1.5	.54	.42	.21	-.08	-.48	-.94	-.114	-.64	-.33	.07	.34	.49
	4.0	.35	.20	.02	-.28	-.60	-.91	-.112	-.106	-.51	.11	.11	.29
	7.0	.17	.02	-.20	-.45	-.78	-.108	---	---	---	---	---	---
	10.0	.09	-.08	-.28	-.42	-.84	-.117	-.113	-.88	-.47	-.23	-.03	0.12
	15.0	-.02	-.17	-.36	-.58	-.91	-.123	-.89	-.58	-.43	-.24	-.08	.06
	20.0	-.09	-.22	-.40	-.60	-.84	-.118	-.74	-.45	-.36	-.21	-.07	.04
	30.0	-.16	-.26	-.40	-.55	-.75	-.115	-.55	-.33	-.23	-.16	-.06	.08
	40.0	-.19	-.28	-.40	-.50	-.55	-.69	-.37	-.23	-.17	-.11	-.04	.03
	50.0	-.19	-.23	-.33	-.44	-.45	-.42	---	---	---	---	---	---
	60.0	-.18	-.22	-.31	-.32	-.36	-.35	-.14	-.08	-.04	0	0.03	0.08
	70.0	-.16	-.20	-.26	-.26	-.27	-.25	-.05	-.04	-.02	0.05	0.08	0.10
	80.0	-.13	-.15	-.17	-.18	-.15	-.14	---	---	---	---	---	---
	90.0	-.03	-.02	-.03	-.03	0	.05	.07	.08	.11	.11	.10	.09
	95.0	.05	.06	.06	.07	.07	.06	.08	.10	.11	.11	.10	.09
0.44 b/2	0	-.07	.17	.44	.59	.58	.46	---	---	---	---	---	---
	1.5	.53	.41	.20	-.10	-.50	-.90	-.109	-.89	-.34	.09	.36	.51
	4.0	.34	.19	-.03	-.31	-.66	-.99	-.115	-.111	-.55	.16	.11	.29
	7.0	.19	.04	-.19	-.46	-.81	-.108	---	---	---	---	---	---
	10.0	.09	-.06	-.28	-.53	-.88	-.118	-.103	-.94	-.47	-.22	-.08	.13
	15.0	-.08	-.16	-.36	-.59	-.90	-.125	-.85	-.95	-.43	-.23	-.06	.07
	20.0	-.08	-.21	-.39	-.59	-.89	-.118	-.71	-.44	-.36	-.19	-.05	.03
	30.0	-.16	-.27	-.41	-.56	-.75	-.114	-.58	-.38	-.23	-.16	-.05	.03
	40.0	-.17	-.26	-.38	-.50	-.77	-.108	-.55	-.29	-.17	-.12	-.04	.03
	50.0	-.18	-.25	-.34	-.43	-.62	-.112	-.52	-.22	-.14	-.09	-.03	.03
	60.0	-.18	-.23	-.32	-.33	-.35	-.34	-.13	-.07	-.04	0.01	.03	.03
	70.0	-.17	-.20	-.27	-.26	-.26	-.24	-.05	0	-.02	0.05	.08	.10
	80.0	-.13	-.14	-.16	-.17	-.15	-.13	---	---	---	---	---	---
	90.0	-.04	-.01	-.03	-.01	.01	-.01	0.04	.07	.08	.09	.08	.08
	95.0	.02	.05	.06	.07	.06	.04	.06	.10	.11	.10	.09	.08

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TABLE VIII.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING.
 $M_\infty = 0.80$; $R = 2,000,000$ - Continued
(a) α_{u_1} , $-4^\circ, -2^\circ, 0^\circ, 2^\circ, 4^\circ, 6^\circ$ - Concluded

Spanwise station	Percent chord	Upper surface						Lower surface					
		Angle of attack						Angle of attack					
		-4°	-2°	0°	2°	4°	6°	-4°	-2°	0°	2°	4°	6°
0.56 b/2	0	-0.03	0.11	0.26	0.39	0.56	0.41	---	---	---	---	0.36	0.51
	1.5	.56	.16	.26	-.04	-.43	-.86	-0.98	-1.03	-0.55	0.04	0.36	0.51
	4.0	.36	.22	0	-.28	-.64	-.10	-1.06	21.14	-.55	-.13	.12	.31
	7.0	.20	.06	-.17	-.44	-.79	-.10	---	---	---	---	---	---
	10.0	.10	-.04	-.26	-.53	-.84	-.17	-.82	-.99	-.49	-.23	-.02	.13
	15.0	0	-.14	-.34	-.58	-.92	-.21	-.74	-.54	-.43	-.23	-.06	.07
	20.0	-.06	-.17	-.35	-.54	-.85	-.16	-.62	-.44	-.36	-.19	-.04	.06
	30.0	-.13	-.23	-.37	-.52	-.71	-.08	-.50	-.34	-.23	-.13	-.04	.02
	40.0	-.17	-.25	-.36	-.47	-.49	-.60	-.35	-.21	-.14	-.10	-.02	.04
	50.0	-.18	-.25	-.34	-.42	-.45	-.41	-.28	-.14	-.09	-.03	.01	.05
	60.0	-.16	-.21	-.30	-.31	-.34	-.30	---	0	.02	.06	.09	.06
	70.0	-.16	-.18	-.24	-.24	-.23	-.19	-.12	---	---	---	.11	.10
	80.0	-.14	-.14	-.16	-.17	-.14	-.10	-.06	.06	.07	.09	.11	.10
	90.0	-.03	-.03	-.03	-.01	.01	-.02	0	.09	.10	.10	.10	.07
	95.0	.02	.06	.07	.08	.08	.01	.03	.11	.12	.12	.10	.06
0.68 b/2	0	.04	.03	.02	.02	.02	.03	---	---	---	---	.31	.47
	1.5	.57	.38	.32	.04	-.34	-.73	-.95	-.15	-.55	-.03	.10	.28
	4.0	.37	.28	.01	-.29	-.58	-.09	-.95	-.18	-.63	-.20	---	---
	7.0	.23	.11	-.13	-.41	-.78	-.15	---	---	---	---	---	---
	10.0	.13	-.02	-.21	-.49	-.85	-.20	-.91	-.07	-.54	-.24	-.02	.11
	15.0	.08	-.08	-.26	-.51	-.83	-.13	-.84	-.62	-.43	-.23	-.05	.06
	20.0	-.04	-.15	-.33	-.53	-.78	-.11	-.77	-.44	-.32	-.20	-.05	.04
	30.0	-.11	-.20	-.34	-.49	-.68	-.09	-.66	-.33	-.23	-.14	-.04	.02
	40.0	-.15	-.22	-.34	-.44	-.51	-.23	-.53	-.21	-.15	-.09	-.02	.02
	50.0	-.18	-.22	-.30	-.39	-.41	-.36	---	---	---	---	---	---
	60.0	-.16	-.19	-.26	-.33	-.31	-.26	-.27	-.06	-.03	.01	.04	.06
	70.0	-.16	-.17	-.23	-.23	-.25	-.19	-.15	-.01	.02	.05	.06	.07
	80.0	-.14	-.13	-.17	-.16	-.14	-.10	-.07	.03	.07	.08	.11	.08
	90.0	-.04	-.01	-.01	-.01	.02	-.01	0	.08	.10	.09	.11	.06
	95.0	.03	.06	.07	.07	.09	.01	.03	.11	.12	.12	.11	.05
0.80 b/2	0	.08	.17	.44	.62	.60	.44	---	---	---	---	---	---
	1.5	.58	.50	.33	.04	-.39	-.83	-.63	-.28	-.74	-.11	.27	.46
	4.0	.38	.29	.09	-.19	-.58	-.95	-.62	-.26	-.73	-.27	.06	.29
	7.0	.23	.14	-.05	-.33	-.69	-.05	---	---	---	---	---	---
	10.0	.16	.06	-.14	-.46	-.72	-.13	-.61	-.10	-.58	-.28	-.05	.09
	15.0	-.03	-.04	-.23	-.46	-.73	-.09	-.59	-.68	-.50	-.27	-.08	.04
	20.0	-.02	-.10	-.26	-.47	-.71	-.03	-.56	-.47	-.39	-.20	-.06	.03
	30.0	-.09	-.14	-.29	-.43	-.60	-.92	-.58	-.35	-.22	-.16	-.05	.01
	40.0	-.13	-.18	-.29	-.39	-.47	-.44	---	---	---	---	---	---
	50.0	-.17	-.19	-.26	-.36	-.39	-.38	-.51	-.16	-.15	-.05	0	.03
	60.0	-.17	-.18	-.24	-.31	-.30	-.26	-.46	-.08	-.05	.01	.03	.05
	70.0	-.18	-.16	-.21	-.22	-.24	-.19	-.40	-.01	.02	.03	.09	.07
	80.0	-.18	-.12	-.17	-.15	-.14	-.10	-.34	-.03	.06	.08	.10	.07
	90.0	-.14	-.08	-.01	-.01	.02	-.24	-.20	.07	.10	.10	.11	.08
	95.0	-.10	.05	.07	.08	.08	.05	-.20	.12	.12	.12	.11	.08
0.94 b/2	0	.05	-.04	.19	.49	.61	.52	---	---	---	---	---	---
	1.5	.14	.51	.39	.16	-.21	-.67	-.30	-.75	-.14	-.41	.10	.36
	4.0	.36	.35	.19	-.03	-.40	-.53	-.28	---	---	---	---	---
	7.0	.21	.19	.03	-.20	-.53	-.93	-.24	-.72	-.83	-.36	-.07	.11
	10.0	.12	.15	-.03	-.27	-.55	-.01	-.24	-.60	-.53	-.35	-.12	.04
	15.0	-.04	.01	-.13	-.32	-.55	-.88	-.24	-.60	-.48	-.30	.13	.01
	20.0	-.04	-.06	-.19	-.32	-.56	-.83	-.21	-.49	-.36	-.25	-.11	-.02
	30.0	-.13	-.15	-.24	-.36	-.49	-.79	-.20	-.41	-.25	-.17	-.09	-.03
	40.0	-.18	-.17	-.24	-.32	-.42	-.40	-.17	-.26	-.14	-.09	-.07	-.03
	50.0	-.23	-.19	-.28	-.29	-.35	-.33	-.16	-.19	-.07	-.05	-.03	0
	60.0	-.24	-.18	-.20	-.23	-.23	-.24	---	---	---	---	---	---
	70.0	-.25	-.15	-.17	-.20	-.17	-.17	-.15	-.06	.05	.05	.07	.04
	80.0	-.23	-.12	-.14	-.09	-.09	-.08	-.12	0	.09	.10	.09	.08
	90.0	-.19	-.03	.03	.03	.04	.02	-.13	.04	.12	.11	.09	.08
	95.0	-.16	.03	.08	.09	.10	.05	-.13	.05	.13	.14	.13	.10

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TABLE VIII.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING.
 $M_\infty = 0.80$; $R = 2,000,000$ - Continued
 (b) α_u , $8^\circ, 10^\circ, 12^\circ, 14^\circ, 16^\circ, 18^\circ$

Spanwise station	Percent chord	Upper surface						Lower surface					
		Angle of attack						Angle of attack					
		8°	10°	12°	14°	16°	18°	8°	10°	12°	14°	16°	18°
0.10 b/2	0	.59	.49	.40	.30	---	.09	---	---	---	---	---	---
	1.5	-.64	-.93	-.18	-.31	---	-.51	-.59	.69	.76	.81	---	.89
	4.0	-.79	-.00	-.21	-.41	---	-.57	-.38	.49	.60	.68	---	.81
	7.0	-.91	-.11	-.31	-.20	---	-.54	---	---	---	---	---	---
	10.0	-.88	-.08	-.24	-.44	---	-.53	-.20	.30	.40	.48	---	.62
	15.0	-.84	-.10	-.25	-.45	---	-.44	-.14	.23	.32	.39	---	.51
	20.0	-.81	-.07	-.07	-.22	---	-.37	-.11	.19	.27	.33	---	.46
	30.0	-.84	-.92	-.03	-.10	---	-.27	-.08	.15	.21	.27	---	.37
	40.0	-.71	-.86	-.95	-.02	---	-.16	-.07	.12	.18	.23	---	.38
	50.0	-.67	-.81	-.91	-.93	---	-.08	-.08	.12	.18	.21	---	.38
	60.0	-.58	-.71	-.84	-.75	---	-.98	-.09	.12	.17	.20	---	.23
	70.0	-.42	-.43	-.44	-.60	---	-.93	-.11	.15	.18	.19	---	.23
0.19 b/2	80.0	-.23	-.26	-.29	-.47	---	-.84	-.09	.11	.11	.10	---	.03
	90.0	-.03	-.10	-.15	-.28	---	-.67	-.06	.09	.06	.06	---	.03
	95.0	-.02	-.07	-.12	-.23	---	-.57	-.06	.03	.06	.03	---	.07
0.31 b/2	0	.41	.27	.12	-.03	---	.30	---	.36	.68	.66	---	.66
	1.5	-.89	-.08	-.23	-.38	---	-.20	-.26	.47	.55	.61	---	.69
	4.0	-.112	-.138	-.158	-.162	---	-.20	-.37	---	---	---	---	---
	7.0	-.114	-.140	-.155	-.161	---	-.19	---	---	---	---	---	---
	10.0	-.115	-.140	-.157	-.159	---	-.19	-.20	.29	.37	.44	---	.56
	15.0	-.122	-.143	-.156	-.153	---	-.16	-.12	.19	.29	.36	---	.47
	20.0	-.116	-.139	-.153	-.147	---	-.15	-.10	.23	.30	.36	---	.41
	30.0	-.113	-.137	-.151	-.131	---	-.13	-.06	.12	.19	.23	---	.32
	40.0	-.01	-.121	-.130	-.125	---	-.11	-.08	.11	.17	.20	---	.27
	50.0	-.69	-.74	-.05	-.17	---	-.07	---	---	---	---	---	---
	60.0	-.38	-.36	-.76	-.06	---	-.05	-.10	.11	.14	.15	---	.17
	70.0	-.28	-.28	-.50	-.92	---	-.01	-.11	.18	.14	.14	---	.13
0.375 b/2	80.0	-.14	-.12	-.20	-.76	---	-.96	-.06	.09	.06	.06	---	---
	90.0	0	-.03	-.06	-.59	---	-.86	-.09	.06	.06	.06	---	.09
	95.0	-.02	-.02	-.05	-.47	---	-.82	-.08	.04	.02	.05	---	.22
0.44 b/2	0	.34	.19	.04	-.10	---	.38	---	.36	.61	.63	---	.60
	1.5	-.96	-.114	-.128	-.115	---	-.93	---	.22	.30	.37	---	.63
	4.0	-.125	-.144	-.134	-.116	---	-.98	---	.14	.22	.29	---	.51
	7.0	-.135	-.145	-.130	-.14	---	-.98	---	.12	.18	.25	---	.45
	10.0	-.137	-.145	-.130	-.111	---	-.98	---	.14	.22	.29	---	.36
	15.0	-.141	-.140	-.120	-.105	---	-.90	---	.12	.18	.25	---	.36
	20.0	-.136	-.134	-.116	-.101	---	-.86	---	.10	.18	.25	---	.27
	30.0	-.134	-.134	-.116	-.106	---	-.86	---	.09	.18	.21	---	.21
	40.0	-.98	-.102	-.00	-.93	---	-.86	---	.07	.11	.15	---	.21
	50.0	-.62	-.90	-.93	-.88	---	-.84	---	.10	.12	.13	---	.16
	60.0	-.39	-.80	-.90	-.85	---	-.84	---	.12	.11	.09	---	---
	70.0	-.29	-.69	-.84	-.82	---	-.82	---	.12	.11	.09	---	.06
0.44 b/2	80.0	-.16	-.25	-.79	-.76	---	-.79	---	.11	.11	.09	---	.16
	90.0	-.03	-.40	-.69	-.71	---	-.73	---	.11	.05	.06	---	.27
	95.0	-.02	-.27	-.63	-.68	---	-.70	---	.10	.08	.10	---	.27
0.44 b/2	0	.30	.16	.01	-.10	---	.32	---	.37	.60	.62	---	.61
	1.5	-.118	-.127	-.01	-.78	-.69	-.70	---	.57	.60	.62	---	.60
	4.0	-.130	-.124	-.02	-.78	-.69	-.71	---	.41	.46	.54	---	.62
	7.0	-.135	-.120	-.97	-.75	-.68	-.70	---	.21	.30	.36	---	.41
	10.0	-.136	-.114	-.94	-.76	-.68	-.70	---	.15	.22	.28	---	.36
	15.0	-.130	-.104	-.90	-.74	-.65	-.68	---	.12	.17	.23	---	.33
	20.0	-.129	-.98	-.89	-.74	-.65	-.68	---	.08	.12	.16	---	.24
	30.0	-.112	-.87	-.83	-.69	-.63	-.66	---	.09	.12	.16	---	.24
	40.0	-.94	-.79	-.79	-.69	-.65	-.67	---	.10	.12	.13	---	.18
	50.0	-.82	-.71	-.74	-.69	-.65	-.67	---	.10	.12	.13	---	.07
	60.0	-.68	-.65	-.72	-.70	-.67	-.69	---	.11	.12	.13	---	.03
	70.0	-.50	-.58	-.69	-.69	-.66	-.68	---	.11	.08	.06	---	.07
	80.0	-.33	-.24	-.59	-.68	-.62	-.68	---	.09	.04	.03	---	.03
	90.0	-.16	-.46	-.61	-.62	-.61	-.65	---	.09	-.05	-.14	---	.18
	95.0	-.04	-.42	-.58	-.60	-.63	-.63	---	.07	-.14	-.24	---	.29

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TABLE VIII.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING,
 $M_\infty = 0.80$; $R = 2,000,000$ - Concluded
 (b) α_u , $8^\circ, 10^\circ, 12^\circ, 14^\circ, 16^\circ, 18^\circ$ - Concluded

Spanwise station	Per-cent chord	Upper surface						Lower surface					
		Angle of attack						Angle of attack					
		8°	10°	12°	14°	16°	18°	8°	10°	12°	14°	16°	18°
0.56 b/2	0	.26	.16	.15	.05	-0.04	-0.17	---	.58	.59	0.60	0.60	0.59
	1.5	-1.06	-.83	-.51	-.52	-.54	---	.44	0.44	0.46	.50	.54	.57
	4.0	-1.10	-.83	-.49	-.53	-.53	---	.40	0.44	0.46	.50	---	---
	7.0	-1.11	-.79	-.48	-.53	-.51	-.54	---	0.21	0.23	0.26	.32	.37
	10.0	-1.00	-.74	-.45	-.51	-.50	-.53	0.21	0.23	0.26	.32	.37	.42
	15.0	-.84	-.65	-.44	-.50	-.50	-.52	0.14	0.17	0.20	.24	.29	.33
	20.0	-.72	-.62	-.43	-.50	-.49	-.52	0.11	0.14	0.16	.19	.24	.28
	30.0	-.37	-.54	-.43	-.49	-.49	-.51	0.08	0.08	0.08	.11	.15	.18
	40.0	-.50	-.51	-.43	-.49	-.48	-.51	0.05	0.05	0.05	.07	.10	.13
	50.0	-.46	-.47	-.42	-.48	-.48	-.51	0.04	0.04	0.04	.03	.06	.09
	60.0	-.35	-.45	-.42	-.48	-.48	-.51	---	---	---	---	---	---
	70.0	-.29	-.41	-.41	-.46	-.47	-.50	0.03	0.02	0.02	0.02	0	.01
	80.0	-.26	-.39	-.41	-.46	-.46	-.50	0.02	0	0	0.05	0.06	0.04
	90.0	-.23	-.36	-.40	-.45	-.45	-.49	0.04	0.09	0.15	0.17	0.16	0.16
	95.0	-.22	-.32	-.39	-.45	-.45	-.48	0.09	0.14	0.21	0.24	0.24	0.23
0.68 b/2	0	.03	.03	.02	.01	.01	0	---	.56	.55	.58	.59	.60
	1.5	-.95	-.62	-.51	-.48	-.48	0	0.23	0.40	0.40	0.46	0.51	.54
	4.0	-1.21	-.07	-.51	-.49	-.49	0	0.36	0.36	0.36	0.36	0.36	0.36
	7.0	-1.19	-.09	-.46	-.48	-.45	0	0.17	0.22	0.22	0.26	0.34	.39
	10.0	-1.16	-.03	-.45	-.45	-.44	0	0.17	0.16	0.15	0.19	0.23	.30
	15.0	-1.09	-.92	-.41	-.44	-.43	0	0.11	0.16	0.15	0.20	0.24	.24
	20.0	-.83	-.77	-.40	-.43	-.43	0	0.08	0.11	0.10	0.15	0.19	.16
	30.0	-.60	-.62	-.38	-.42	-.41	0	0.04	0.06	0.04	0.07	0.12	.10
	40.0	-.52	-.57	-.37	-.41	-.41	0	0.03	0.03	0.03	0.04	0.07	.10
	50.0	-.41	-.49	-.35	-.41	-.41	0	0.03	0.01	0.01	0.01	0.02	.04
	60.0	-.36	-.44	-.35	-.41	-.41	0	0.03	0.03	0.04	0.04	0.02	.01
	70.0	-.29	-.36	-.34	-.40	-.41	0	0.03	0.02	0.02	0.03	0.02	.03
	80.0	-.24	-.33	-.33	-.40	-.41	0	0.04	0.04	0.05	0.06	0.06	.05
	90.0	-.18	-.26	-.32	-.41	-.40	0	0.04	0.13	0.13	0.16	0.15	.15
	95.0	-.14	-.24	-.31	-.39	-.40	0	0.05	0.09	0.20	0.23	0.24	.24
0.80 b/2	0	.31	.19	.12	.08	.03	0	---	.56	.55	.55	.57	.59
	1.5	-1.06	-.14	-.23	-.23	-.23	0	0.51	0.51	0.51	0.40	0.44	.49
	4.0	-1.21	-.15	-.23	-.47	-.43	0	0.38	0.39	0.39	0.40	0.44	.49
	7.0	-1.22	-.16	-.26	-.41	-.38	0	0.40	0.40	0.40	0.40	0.41	.45
	10.0	-1.15	-.08	-.15	-.40	-.37	0	0.39	0.21	0.22	0.23	0.29	.33
	15.0	-1.15	-.99	-.04	-.37	-.35	0	0.09	0.14	0.13	0.15	0.21	.25
	20.0	-.04	-.84	-.84	-.37	-.35	0	0.07	0.11	0.11	0.11	0.16	.20
	30.0	-.67	-.64	-.61	-.35	-.34	0	0.04	0.06	0.04	0.05	0.09	.12
	40.0	-.49	-.57	-.57	-.35	-.34	0	0.04	0.04	0.04	0.04	0.04	0.04
	50.0	-.36	-.45	-.46	-.34	-.34	0	0.03	0.03	0	0.01	0.02	.01
	60.0	-.28	-.39	-.36	-.38	-.34	0	0.04	0.05	0	0.02	0	.01
	70.0	-.19	-.30	-.32	-.33	-.33	0	0.06	0.05	0	0.03	0.01	0
	80.0	-.13	-.26	-.28	-.33	-.33	0	0.06	0.04	0.02	0.07	0.06	.06
	90.0	-.07	-.24	-.24	-.31	-.32	0	0.04	0.01	0.06	0.14	0.14	.13
	95.0	-.06	-.24	-.24	-.31	-.32	0	0.02	0.01	0.10	0.18	0.17	.19
0.94 b/2	0	.42	.31	.20	.14	.02	0	---	.52	.53	.53	.53	.55
	1.5	-.99	-.21	-.14	-.33	-.23	0	0.46	0.27	0.29	.30	.33	.39
	4.0	-1.07	-.09	-.02	-.21	-.12	0	0.02	0.19	0.18	0.20	0.26	.30
	7.0	-1.16	-.11	-.06	-.22	-.05	0	0.05	0.11	0.13	0.13	0.18	.22
	10.0	-1.12	-.99	-.06	-.11	-.03	0	0.09	0.11	0.10	0.12	0.16	.20
	15.0	-1.07	-.85	-.74	-.94	-.87	0	0.06	0.11	0.13	0.13	0.18	.22
	20.0	-1.07	-.75	-.72	-.92	-.83	0	0.03	0.08	0.09	0.08	0.12	.16
	30.0	-.50	-.54	-.58	-.71	-.75	0	0.01	0.02	0.03	0.01	0.06	.08
	40.0	-.37	-.45	-.52	-.70	-.82	0	0.01	0.01	0.01	0.03	0.04	.02
	50.0	-.26	-.34	-.42	-.53	-.68	0	0	0	0	0.01	0.04	.02
	60.0	-.18	-.26	-.38	-.44	-.67	0	0	0	0	0	0	0
	70.0	-.16	-.18	-.30	-.33	-.53	0	0.03	0.01	0.01	0.03	0.04	.03
	80.0	-.03	-.14	-.26	-.24	-.43	0	0.05	0.01	0.02	0.04	0.06	.07
	90.0	-.03	-.09	-.22	-.18	-.34	0	0.05	0.01	0.06	0.08	0.11	.11
	95.0	-.06	-.08	-.21	-.14	-.27	0	0.05	0.03	0.11	0.09	0.13	.17

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TABLE IX.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING.
 $M_\infty = 0.86$; $R = 2,000,000$
(a) $\alpha_u = -4^\circ, -2^\circ, 0^\circ, 2^\circ, 4^\circ, 6^\circ$

Spanwise station	Percent chord	Upper surface						Lower surface					
		Angle of attack						Angle of attack					
		-4°	-2°	0°	2°	4°	6°	-4°	-2°	0°	2°	4°	6°
0.10 b/2	0	0.26	0.40	0.52	0.61	0.65	0.66	---	---	---	---	---	---
	1.5	.46	.37	.24	.09	-.07	-.25	-.08	-.12	0.10	0.26	0.46	---
	4.0	.27	.16	.02	-.13	-.29	-.45	-.18	-.34	-.13	.06	.23	---
	7.0	.13	.04	-.11	-.27	-.42	-.58	---	---	---	---	---	---
	10.0	.06	-.04	-.18	-.30	-.45	-.59	-.09	-.26	-.22	-.08	.07	---
	15.0	-.02	-.13	-.24	-.37	-.49	-.59	---	---	---	---	---	---
	20.0	-.09	-.16	-.29	-.41	-.52	-.60	-.10	-.20	-.11	-.06	.02	---
	30.0	-.14	-.24	-.34	-.46	-.55	-.65	-.16	-.31	-.24	-.12	0	---
	40.0	-.15	-.24	-.33	-.42	-.53	-.63	-.17	-.32	-.23	-.13	-.01	---
	50.0	-.17	-.24	-.33	-.43	-.54	-.66	-.19	-.31	-.20	-.10	-.01	0
	60.0	-.17	-.22	-.30	-.40	-.50	-.55	-.21	-.30	-.18	-.09	-.03	0.03
	70.0	-.18	-.23	-.29	-.35	-.50	-.61	-.21	-.31	-.20	-.10	-.05	0.05
	80.0	-.15	-.16	-.23	-.25	-.31	-.39	---	---	---	---	---	---
	90.0	-.03	-.04	-.03	-.05	-.05	-.05	0	0.01	0.04	0.04	0.05	0.05
	95.0	.05	.04	.04	.03	0	-.03	.05	.05	.04	.04	.04	.04
0.19 b/2	0	.15	.31	.47	.57	.60	.58	---	---	---	---	---	---
	1.5	.49	.41	.26	.07	-.16	-.42	-.06	-.69	-.32	0	.23	.52
	4.0	.25	.19	0	-.21	-.43	-.67	-.10	-.94	-.51	-.20	-.02	.21
	7.0	.14	.08	-.14	-.32	-.52	-.71	---	---	---	---	---	---
	10.0	.03	-.09	-.25	-.43	-.61	-.78	-.05	-.85	-.52	-.29	-.11	.05
	15.0	-.05	-.17	-.32	-.49	-.67	-.88	-.10	-.78	-.49	-.29	-.14	0
	20.0	-.12	-.23	-.38	-.53	-.68	-.85	-.16	-.74	-.44	-.27	-.14	-.02
	30.0	-.19	-.29	-.41	-.55	-.73	-.88	-.26	-.74	-.44	-.23	-.13	-.01
	40.0	-.22	-.31	-.43	-.55	-.71	-.85	-.30	-.73	-.41	-.21	-.10	-.01
	50.0	-.22	-.29	-.40	-.52	-.70	-.84	---	---	---	---	---	---
	60.0	-.20	-.29	-.35	-.47	-.66	-.79	-.14	-.72	-.40	-.20	-.03	.05
	70.0	-.19	-.22	-.26	-.35	-.53	-.65	-.09	-.64	-.32	-.12	.04	.08
	80.0	-.14	-.16	-.18	-.19	-.19	-.12	---	---	---	---	---	---
	90.0	-.02	-.02	-.03	-.03	-.03	.02	-.05	-.04	-.07	.07	.06	.06
	95.0	.05	.05	.06	.06	.06	.05	.07	.06	.09	.10	.10	.08
0.31 b/2	0	.10	.29	.45	.57	.59	.54	---	---	---	---	---	---
	1.5	.51	.42	.26	.03	-.24	-.50	-.05	-.72	-.35	.02	.27	.44
	4.0	.27	.15	-.04	-.26	-.54	-.78	-.10	-.61	-.35	-.19	.06	.24
	7.0	.14	.01	-.19	-.42	-.66	-.87	---	---	---	---	---	---
	10.0	.05	-.06	-.27	-.49	-.72	-.99	-.03	-.98	-.54	-.26	-.09	.07
	15.0	-.08	-.19	-.38	-.60	-.80	-.100	-.10	-.98	-.50	-.26	-.13	.02
	20.0	-.14	-.24	-.42	-.64	-.83	-.104	-.09	-.98	-.43	-.24	-.11	.01
	30.0	-.20	-.29	-.44	-.64	-.89	-.107	-.13	-.93	-.36	-.20	-.09	.01
	40.0	-.23	-.30	-.43	-.59	-.85	-.107	-.19	-.92	-.29	-.19	-.07	.01
	50.0	-.23	-.28	-.39	-.53	-.83	-.102	-.20	-.90	-.29	-.17	-.04	.02
	60.0	-.20	-.25	-.31	-.31	-.29	-.49	---	---	---	---	---	---
	70.0	-.19	-.21	-.26	-.27	-.24	-.26	-.01	-.03	0	.04	.07	.10
	80.0	-.13	-.16	-.17	-.18	-.16	-.15	---	---	---	---	---	---
	90.0	-.02	-.01	-.02	-.01	-.01	-.03	.06	.06	.06	.06	.06	.11
	95.0	.06	.06	.06	.05	.03	.03	.08	.08	.10	.10	.10	.11
0.375 b/2	0	.05	.22	.43	.58	.59	.52	---	---	---	---	---	---
	1.5	.51	.42	.23	.04	-.36	-.71	-.01	-.75	-.33	.06	.30	.46
	4.0	.32	.21	0	-.25	-.50	-.72	---	---	---	---	---	---
	7.0	.16	.03	-.19	-.44	-.64	-.89	---	---	---	---	---	---
	10.0	.07	-.07	-.26	-.53	-.74	-.98	-.03	-.94	-.32	-.17	-.06	.09
	15.0	-.04	-.17	-.38	-.62	-.84	-.105	-.08	-.93	-.47	-.26	-.10	.03
	20.0	-.12	-.23	-.43	-.66	-.89	-.107	-.15	-.72	-.41	-.22	-.09	.02
	30.0	-.17	-.27	-.43	-.63	-.93	-.105	-.16	-.74	-.35	-.17	-.08	0
	40.0	-.21	-.30	-.43	-.68	-.89	-.103	-.24	-.75	-.35	-.12	.04	.02
	50.0	-.21	-.26	-.38	-.55	-.80	-.087	---	---	---	---	---	---
	60.0	-.19	-.23	-.31	-.33	-.32	-.68	-.14	-.74	-.23	-.04	.08	.07
	70.0	-.18	-.20	-.24	-.26	-.26	-.49	---	---	---	0.05	.08	.07
	80.0	-.13	-.14	-.15	-.15	-.14	-.22	---	---	---	---	---	---
	90.0	-.03	-.01	-.02	0	-.02	-.01	.01	.01	.09	.10	.10	.10
	95.0	.06	.07	.07	.08	.07	.09	.05	.11	.11	.11	.11	.11
0.44 b/2	0	.05	.23	.46	.59	.59	.43	---	---	---	---	---	---
	1.5	.51	.42	.22	-.07	-.37	-.68	-.09	-.79	-.33	.08	.34	.49
	4.0	.32	.20	-.02	-.29	-.54	-.79	-.10	-.80	-.39	.19	.08	.26
	7.0	.16	.04	-.18	-.35	-.70	-.89	---	---	---	---	---	---
	10.0	.06	-.05	-.28	-.53	-.80	-.99	-.07	-.70	-.32	-.18	-.04	.10
	15.0	-.04	-.16	-.38	-.64	-.88	-.107	-.16	-.74	-.47	-.24	-.09	.03
	20.0	-.10	-.22	-.41	-.68	-.92	-.103	-.20	-.76	-.40	-.20	-.08	.02
	30.0	-.19	-.28	-.45	-.64	-.88	-.99	-.29	-.77	-.33	-.17	-.07	.02
	40.0	-.20	-.28	-.42	-.68	-.90	-.79	---	---	---	---	---	---
	50.0	-.20	-.26	-.38	-.41	-.63	-.66	---	---	---	---	---	---
	60.0	-.20	-.23	-.32	-.33	-.33	-.56	---	---	---	0.03	.06	.06
	70.0	-.20	-.20	-.25	-.26	-.22	-.47	---	---	---	0.03	.06	.10
	80.0	-.17	-.14	-.17	-.16	-.13	-.39	---	---	---	0.06	.06	.06
	90.0	-.10	-.02	-.01	0	-.01	-.29	-.06	.07	.09	.06	.06	.06
	95.0	-.05	.06	.07	.08	.05	.23	-.06	.10	.11	.09	.09	-.02

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TABLE IX.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING.
 $M_\infty = 0.86$; $R = 2,000,000$ - Continued
(a) α_u , -4° , -2° , 0° , 2° , 4° , 6° - Concluded

Spanwise station	Percent chord	Upper surface						Lower surface					
		Angle of attack						Angle of attack					
		-4°	-2°	0°	2°	4°	6°	-4°	-2°	0°	2°	4°	6°
0.56 b/2	0	0.08	0.25	0.47	0.60	0.58	0.48	---	---	---	---	---	---
	1.5	.55	.46	.27	-.01	-.34	-.64	-.89	-.88	-.44	0.05	0.32	0.47
	4.0	.33	.23	.01	-.28	-.54	-.83	-.89	1.02	-.58	-.15	.10	.26
	7.0	.17	.07	-.16	-.44	-.69	-.89	---	---	---	---	---	---
	10.0	.06	-.04	-.27	-.53	-.77	-.84	-.85	-.96	-.54	-.24	-.04	.09
	15.0	-.04	-.14	-.36	-.65	-.92	-.85	-.79	-.90	-.47	-.24	-.09	.03
	20.0	-.09	-.18	-.37	-.63	-.93	-.82	-.71	-.66	-.42	-.20	-.07	0
	30.0	-.17	-.24	-.40	-.59	-.88	-.63	-.63	-.34	-.23	-.15	-.07	0
	40.0	-.20	-.26	-.40	-.53	-.84	-.51	-.54	-.23	-.15	-.11	-.04	0
	50.0	-.23	-.26	-.35	-.44	-.74	-.42	-.42	-.15	-.10	-.03	-.01	0
	60.0	-.21	-.22	-.32	-.31	-.26	-.35	---	---	---	---	---	---
	70.0	-.21	-.18	-.24	-.24	-.19	-.29	-.04	0	-.08	-.06	-.07	.01
	80.0	-.18	-.14	-.16	-.15	-.10	-.25	-.01	-.05	-.08	-.09	-.09	.01
	90.0	-.07	-.03	-.02	0	0	-.05	-.06	-.09	-.10	-.11	-.07	-.04
	95.0	.02	.06	.08	.09	.05	.21	.08	.11	.12	.12	.07	-.06
0.68 b/2	0	.04	.03	.04	.05	.04	-.05	---	---	---	---	---	---
	1.5	.57	.51	.34	-.08	-.25	-.51	-.72	-.95	-.53	-.02	.28	.42
	4.0	.35	.25	.02	-.28	-.59	-.83	-.73	1.04	-.68	-.20	.07	.22
	7.0	.21	.10	-.13	-.43	-.72	-.92	---	---	---	---	---	0
	10.0	.11	.01	-.22	-.53	-.81	-.97	-.69	-.98	-.58	-.25	-.04	.07
	15.0	.01	-.09	-.29	-.55	-.89	-.93	-.63	-.74	-.51	-.25	-.09	0
	20.0	-.06	-.15	-.35	-.60	-.91	-.91	-.60	-.54	-.32	-.21	-.09	0
	30.0	-.13	-.21	-.35	-.55	-.84	-.78	-.57	-.37	-.24	-.13	-.06	-.03
	40.0	-.19	-.24	-.36	-.50	-.74	-.43	-.50	-.23	-.15	-.09	-.03	-.02
	50.0	-.20	-.23	-.33	-.43	-.73	-.31	---	---	---	---	---	---
	60.0	-.18	-.19	-.28	-.30	-.23	-.24	-.38	-.10	-.08	-.08	-.04	.02
	70.0	-.19	-.18	-.23	-.23	-.18	-.19	-.31	-.03	-.08	-.06	.01	.01
	80.0	-.19	-.14	-.15	-.15	-.09	-.14	-.23	-.08	-.07	-.08	.08	.03
	90.0	-.10	-.01	0	0	-.01	-.10	-.15	.07	.11	.11	.08	0
	95.0	-.07	.06	.07	.09	.05	-.08	-.12	.10	.13	.12	.07	-.02
0.80 b/2	0	.21	.26	.48	.63	.62	.55	---	---	---	---	---	---
	1.5	.35	.50	.34	.03	-.31	-.58	-.51	1.00	-.70	-.10	.25	.38
	4.0	.36	.29	.15	-.20	-.64	-.84	---	---	---	---	0	.17
	7.0	.23	.15	-.03	-.34	-.67	---	---	---	---	---	---	0
	10.0	.15	.06	-.15	-.42	-.74	-.98	-.49	-.89	-.63	-.29	-.08	.05
	15.0	.02	-.04	-.23	-.51	-.82	-.98	-.47	-.67	-.55	-.27	-.10	-.04
	20.0	-.05	-.12	-.29	-.54	-.84	-.91	-.44	-.53	-.39	-.22	-.08	-.03
	30.0	-.12	-.16	-.30	-.48	-.76	-.90	---	---	---	---	---	0
	40.0	-.18	-.19	-.30	-.44	-.57	-.56	---	---	---	---	---	0
	50.0	-.22	-.20	-.29	-.38	-.32	-.33	-.40	-.22	-.18	-.04	-.02	0
	60.0	-.22	-.19	-.25	-.32	-.28	-.27	-.36	-.14	-.08	.01	.01	.03
	70.0	-.24	-.17	-.22	-.21	-.21	-.15	-.34	-.06	.03	.05	.08	.03
	80.0	-.26	-.13	-.16	-.14	-.11	-.06	-.30	-.01	.07	.08	.09	.07
	90.0	-.20	-.03	-.01	0	-.03	-.01	-.25	.05	.11	.11	.10	.07
	95.0	-.17	.05	.03	.08	.09	.04	-.22	.06	.13	.13	.11	.07
0.94 b/2	0	.10	.06	.25	.51	.61	.58	---	---	---	---	---	---
	1.5	.50	.50	.40	-.16	-.19	-.47	-.33	-.37	1.07	-.39	-.09	.30
	4.0	.36	.35	.20	-.05	-.40	-.61	---	---	---	---	---	0
	7.0	.20	.19	.03	-.22	-.37	-.78	---	---	---	---	---	0
	10.0	.11	.10	-.03	-.29	-.61	-.89	-.25	-.49	-.83	-.36	-.14	0
	15.0	.02	0	-.14	-.35	-.61	-.88	-.25	-.49	-.83	-.33	-.15	0
	20.0	-.06	-.06	-.20	-.46	-.66	-.83	-.22	-.46	-.83	-.27	-.14	-.05
	30.0	-.16	-.15	-.26	-.41	-.77	---	-.21	-.38	-.25	-.18	-.10	-.05
	40.0	-.22	-.19	-.27	-.36	-.50	-.74	-.18	-.28	-.14	-.10	-.09	-.03
	50.0	-.28	-.22	-.26	-.32	-.29	-.21	-.18	-.24	-.05	-.03	-.04	-.02
	60.0	-.29	-.21	-.23	-.28	-.20	-.15	---	---	---	---	---	0
	70.0	-.29	-.18	-.19	-.15	-.15	-.15	-.14	-.11	.05	.07	.07	.04
	80.0	-.26	-.14	-.14	-.08	-.08	-.08	-.12	-.06	.11	.10	.09	.09
	90.0	-.18	-.04	-.05	0	0	-.07	-.12	-.02	.14	.13	.11	.10
	95.0	-.13	0	.11	.09	.12	.11	-.10	.01	.15	.15	.13	.11

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TABLE IX. - PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING.
 $M_\infty = 0.86$; $R = 2,000,000$ - Continued
(b) α_u , $8^\circ, 10^\circ, 12^\circ, 14^\circ, 16^\circ$

Spanwise station	Percent chord	Upper surface					Lower surface				
		Angle of attack					Angle of attack				
		8°	10°	12°	14°	16°	8°	10°	12°	14°	16°
0.10 b/2	0	0.63	0.57	0.49	0.41	0.32	---	---	---	---	---
	1.5	-.46	-.71	-.98	-1.08	-1.16	0.97	0.68	0.75	0.82	0.87
	4.0	-.63	-.80	-.99	-1.18	-1.27	-.37	-.48	-.58	-.67	-.74
	7.0	-.77	-.93	-1.10	-1.27	-1.36	---	---	---	---	---
	10.0	-.78	-.94	-1.09	-1.24	-1.35	.19	.30	.39	.47	.55
	15.0	-.73	-.91	-1.08	-1.24	-1.34	.13	.23	.30	.38	.45
	20.0	-.72	-.87	-1.07	-1.22	-1.35	.09	.19	.25	.33	.39
	30.0	-.76	-.84	-.91	-.96	-1.09	.06	.14	.20	.26	.31
	40.0	-.71	-.79	-.88	-.93	-.95	.02	.14	.17	.22	.27
	50.0	-.68	-.77	-.86	-.96	-.98	.06	.11	.16	.21	.29
	60.0	-.66	-.75	-.83	-.86	-.86	.06	.12	.15	.20	.21
	70.0	-.71	-.79	-.85	-.85	-.90	.10	.13	.15	.17	.21
	80.0	-.51	-.69	-.79	-.85	-.90	---	---	---	---	---
	90.0	-.18	-.33	-.40	-.45	-.59	0.06	-.06	-.05	-.06	-.04
	95.0	-.15	-.29	-.37	-.42	-.53	0.02	-.01	-.01	-.03	-.01
0.19 b/2	0	.49	.38	.26	.12	-.01	---	---	---	---	---
	1.5	-.66	-.83	-.97	-1.08	-1.15	.55	.61	.66	.66	.69
	4.0	-.89	-.11	-.26	-.35	-.28	.34	.46	.53	.60	.65
	7.0	-.94	-.13	-.30	-.33	-.20	---	---	---	---	---
	10.0	-.97	-.14	-.32	-.32	-.19	.17	.26	.35	.42	.48
	15.0	-.04	-.19	-.35	-.32	-.19	.11	.20	.27	.34	.40
	20.0	-.04	-.20	-.34	-.29	-.17	.07	.16	.22	.29	.35
	30.0	-.03	-.19	-.31	-.20	-.13	.05	.11	.16	.22	.25
	40.0	-.01	-.19	-.26	-.14	-.10	.05	.11	.15	.19	.24
	50.0	-.99	-.08	-.12	-.09	-.08	0.07	-.11	-.13	-.15	---
	60.0	-.88	-.96	-.00	-.05	-.05	.08	.11	.11	.11	---
	70.0	-.30	-.84	-.84	-.98	-.00	---	---	---	---	---
	80.0	-.12	-.19	-.66	-.90	-.96	---	---	---	---	---
	90.0	-.06	-.17	-.53	-.78	-.87	.06	-.05	0	-.04	-.09
	95.0	-.07	-.19	-.44	-.67	-.81	.03	-.01	-.06	-.14	-.21
0.31 b/2	0	.44	.31	.18	.05	-.06	---	---	---	---	---
	1.5	-.72	-.88	-.02	-.10	-.10	.54	.60	.62	.64	.63
	4.0	-.99	-.15	-.24	-.14	-.03	.37	.46	.52	.57	.60
	7.0	-.09	-.23	-.20	-.03	-.02	---	---	---	---	---
	10.0	-.11	-.25	-.20	-.07	-.00	.18	.27	.34	.40	.45
	15.0	-.18	-.29	-.18	-.00	-.97	.11	.19	.25	.31	.35
	20.0	-.18	-.27	-.13	-.99	-.95	.10	.15	.21	.24	.31
	30.0	-.15	-.24	-.03	-.92	-.90	.06	.11	.15	.18	.21
	40.0	-.15	-.14	-.97	-.90	-.89	.05	.09	.10	.14	.16
	50.0	-.00	-.01	-.89	-.85	-.85	.07	.10	.10	.11	.13
	60.0	-.85	-.92	-.84	-.85	-.85	---	---	---	---	---
	70.0	-.74	-.85	-.80	-.82	-.84	.10	.10	.07	.04	.03
	80.0	-.44	-.75	-.77	-.79	-.82	---	---	---	---	---
	90.0	-.02	-.57	-.59	-.72	-.73	.11	.05	-.13	-.15	.16
	95.0	.11	-.40	-.65	-.68	-.72	.13	0	-.23	-.24	.26
0.375 b/2	0	.41	.26	.25	.02	-.10	---	---	---	---	---
	1.5	-.90	-.05	-.02	-.77	-.75	.56	.60	.61	.63	.62
	4.0	-.02	-.18	-.02	-.78	-.76	.38	.45	.51	.56	.60
	7.0	-.05	-.19	-.05	-.74	-.74	---	---	---	---	---
	10.0	-.12	-.19	-.00	-.74	-.74	.20	.27	.33	.39	.44
	15.0	-.16	-.17	-.84	-.72	-.73	.12	.19	.25	.30	.35
	20.0	-.13	-.11	-.82	-.72	-.73	.10	.13	.11	.25	.28
	30.0	-.07	-.94	-.73	-.67	-.70	.06	.10	.13	.17	.20
	40.0	-.92	-.86	-.72	-.67	-.68	.06	.09	.08	.13	.15
	50.0	-.80	-.78	-.68	-.66	-.63	---	---	---	---	---
	60.0	-.71	-.73	-.68	-.67	-.70	.09	.07	.04	.06	.06
	70.0	-.64	-.69	-.66	-.67	-.69	.10	.07	.01	.01	.02
	80.0	-.58	-.68	-.65	-.67	-.68	---	---	---	---	---
	90.0	-.50	-.61	-.61	-.63	-.65	.02	-.09	-.15	-.15	.16
	95.0	-.44	-.56	-.59	-.60	-.64	.07	-.19	-.25	-.26	-.27
0.44 b/2	0	.42	.27	.11	.11	-.01	---	---	---	---	---
	1.5	-.84	-.93	-.68	-.55	-.58	.56	.60	.61	.62	---
	4.0	-.04	-.95	-.70	-.56	-.60	.36	.44	.51	.54	.57
	7.0	-.03	-.94	-.67	-.55	-.60	---	---	---	---	---
	10.0	-.01	-.90	-.66	-.55	-.59	.20	.27	.30	.36	.41
	15.0	-.00	-.80	-.62	-.54	-.59	.12	.18	.21	.22	.26
	20.0	-.94	-.76	-.61	-.54	-.59	.10	.15	.18	.22	---
	30.0	-.73	-.68	-.59	-.55	-.59	.06	.09	.11	.15	.18
	40.0	-.68	-.65	-.58	-.56	-.59	.04	.05	.06	.09	.11
	50.0	-.62	-.58	-.56	-.56	-.59	.06	.06	.05	.06	.08
	60.0	-.58	-.56	-.56	-.57	-.59	.05	.03	-.01	.03	.02
	70.0	-.53	-.55	-.56	-.56	-.59	.05	.02	-.01	-.01	-.01
	80.0	-.50	-.55	-.56	-.57	-.59	.09	-.14	-.19	-.20	-.19
	90.0	-.47	-.51	-.53	-.55	-.58	.17	-.22	-.28	-.28	-.28
	95.0	-.44	-.49	-.52	-.54	-.57	0.05	-.17	-.25	-.26	-.26

NACA

TABLE IX.-- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING.

 $M_\infty = 0.86$; $R = 2,000,000$ - Concluded(b) α_u , 8° , 10° , 12° , 14° , 16° - Concluded

Spanwise station	Percent chord	Upper surface					Lower surface				
		Angle of attack					Angle of attack				
		8°	10°	12°	14°	16°	8°	10°	12°	14°	16°
0.56 b/2	0	0.37	0.27	0.20	0.10	0	0.55	0.58	0.59	0.61	0.66
	1.5	-0.19	-0.67	-0.56	-0.48	-0.34	-0.36	-0.41	-0.45	-0.50	-0.54
	4.0	-0.75	-0.62	-0.53	-0.48	-0.38	-	-	-	-	-
	7.0	-0.73	-0.60	-0.54	-0.48	-0.38	-	-	-	-	-
	10.0	-0.67	-0.58	-0.53	-0.46	-0.38	-0.18	-0.23	-0.26	-0.32	-0.36
	13.0	-0.53	-0.52	-0.51	-0.51	-0.53	-0.09	-0.15	-0.17	-0.22	-0.27
	20.0	-0.49	-0.51	-0.50	-0.50	-0.53	-0.08	-0.11	-0.13	-0.19	-0.23
	30.0	-0.40	-0.48	-0.49	-0.50	-0.52	-0.02	-0.05	-0.06	-0.11	-0.15
	40.0	-0.37	-0.48	-0.49	-0.50	-0.52	-0.01	-0.02	-0.02	-0.07	-0.09
	50.0	-0.34	-0.46	-0.47	-0.48	-0.51	0	-0.01	-0.01	-0.03	-0.06
	60.0	-0.34	-0.45	-0.46	-0.48	-0.51	-	-	-	-	-
	70.0	-0.32	-0.43	-0.45	-0.49	-0.51	-0.01	-0.02	-0.04	-0.03	-0.01
	80.0	-0.32	-0.41	-0.46	-0.49	-0.50	-0.03	-0.04	-0.08	-0.03	-0.05
	90.0	-0.31	-0.38	-0.44	-0.47	-0.49	-0.11	-0.13	-0.18	-0.16	-0.17
	95.0	-0.30	-0.36	-0.43	-0.47	-0.49	-0.16	-0.19	-0.23	-0.26	-0.23
0.68 b/2	0	.05	.04	.03	.02	.02	---	---	---	---	---
	1.5	-0.67	-0.83	-0.60	-0.48	-0.39	-0.49	.54	.55	.58	.58
	4.0	-0.98	-0.99	-0.51	-0.46	-0.49	-0.30	.37	.39	.45	.50
	7.0	-1.03	-1.02	-0.51	-0.47	-0.49	-	-	-	-	-
	10.0	-0.99	-0.99	-0.49	-0.46	-0.48	-0.13	.19	.21	.27	.33
	13.0	-0.96	-0.93	-0.45	-0.44	-0.46	-0.06	.10	.13	.19	.24
	20.0	-0.83	-0.84	-0.44	-0.44	-0.46	-0.03	.08	.08	.14	.19
	30.0	-0.59	-0.70	-0.43	-0.43	-0.45	-0.01	.02	.03	.07	.11
	40.0	-0.48	-0.64	-0.41	-0.43	-0.46	-0.02	.01	0	.03	.05
	50.0	-0.39	-0.56	-0.40	-0.42	-0.44	0	0	0	0	0
	60.0	-0.33	-0.47	-0.39	-0.42	-0.44	-0.01	-0.02	-0.05	-0.02	0
	70.0	-0.28	-0.40	-0.39	-0.42	-0.44	0	-0.03	-0.06	-0.03	-0.04
	80.0	-0.24	-0.34	-0.37	-0.42	-0.44	0	-0.05	-0.08	-0.08	-0.08
	90.0	-0.20	-0.29	-0.35	-0.40	-0.44	-0.05	-0.09	-0.16	-0.17	-0.18
	95.0	-0.19	-0.27	-0.35	-0.41	-0.43	-0.09	-0.14	-0.24	-0.26	-0.27
0.80 b/2	0	.44	.31	.25	.22	.11	---	---	---	---	---
	1.5	-0.79	-0.94	-0.88	-0.50	-0.52	-0.47	.52	.53	.56	.57
	4.0	-0.94	-1.01	-0.83	-0.44	-0.44	-0.26	.35	.35	.39	.43
	7.0	-1.00	-1.03	-0.83	-0.43	-0.41	-	-	-	-	-
	10.0	-1.03	-0.99	-0.75	-0.41	-0.41	-0.11	.17	.16	.22	.27
	13.0	-0.98	-0.94	-0.58	-0.38	-0.40	-0.03	.10	.09	.15	.19
	20.0	-0.95	-0.88	-0.64	-0.36	-0.39	-0.03	.08	.07	.10	.15
	30.0	-0.91	-0.75	-0.56	-0.36	-0.39	0	.02	.01	.04	.06
	40.0	-0.69	-0.69	-0.56	-0.36	-0.36	-	-	-	-	-
	50.0	-0.54	-0.59	-0.51	-0.36	-0.37	0	0	0	0	0
	60.0	-0.45	-0.54	-0.46	-0.36	-0.37	-0.02	.01	0	-0.04	-0.01
	70.0	-0.35	-0.46	-0.42	-0.34	-0.37	-0.05	.02	.02	-0.04	-0.04
	80.0	-0.23	-0.40	-0.40	-0.35	-0.36	-0.06	.01	-0.07	-0.09	-0.10
	90.0	-0.14	-0.31	-0.34	-0.34	-0.36	-0.06	-0.02	-0.13	-0.15	-0.16
	95.0	-0.08	-0.25	-0.33	-0.33	-0.36	-0.05	-0.04	-0.16	-0.20	-0.21
0.94 b/2	0	.50	.41	.33	.25	.11	---	---	---	---	---
	1.5	-0.70	-0.85	-1.05	-1.10	-1.13	-0.41	.48	.50	.52	.54
	4.0	-0.80	-0.74	-0.99	-1.01	-1.09	-	-	-	-	-
	7.0	-0.84	-0.76	-0.99	-1.02	-1.09	-0.15	.21	.24	.26	.31
	10.0	-0.79	-0.69	-0.94	-0.95	-1.03	-0.07	.13	.15	.19	.23
	13.0	-0.78	-0.58	-0.89	-0.85	-0.94	-0.02	.06	.01	.11	.15
	20.0	-0.58	-0.55	-0.84	-0.85	-0.99	-0.05	.03	.04	.06	.10
	30.0	-0.44	-0.44	-0.68	-0.70	-0.87	-0.05	-0.02	-0.03	-0.01	.01
	40.0	-0.35	-0.40	-0.64	-0.73	-0.95	-0.05	-0.05	-0.05	-0.07	-0.04
	50.0	-0.24	-0.32	-0.57	-0.59	-0.84	-0.05	-0.06	-0.06	-0.09	-0.09
	60.0	-0.20	-0.30	-0.53	-0.57	-0.88	-	-	-	-	-
	70.0	-0.13	-0.24	-0.44	-0.46	-0.79	-0.03	-0.05	-0.05	-0.10	-0.10
	80.0	-0.11	-0.23	-0.38	-0.40	-0.68	-0.01	-0.05	-0.03	-0.10	-0.09
	90.0	-0.07	-0.19	-0.25	-0.28	-0.34	-0.02	-0.08	-0.06	-0.12	-0.11
	95.0	-0.07	-0.19	-0.25	-0.28	-0.34	-0.04	-0.12	-0.12	-0.10	-0.15



TABLE X.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING.
 $M_\infty = 0.90$; $R = 2,000,000$
(a) α_u , $-4^\circ, -2^\circ, 0^\circ, 2^\circ, 4^\circ, 6^\circ$

Spanwise station	Percent chord	Upper surface						Lower surface					
		Angle of attack						Angle of attack					
		-4°	-2°	0°	2°	4°	6°	-4°	-2°	0°	2°	4°	6°
0.10 b/2	0	0.32	0.85	0.56	0.63	0.69	0.70	-	-	-	-	-	-
	1.5	.49	.40	.28	.16	0	-.16	-0.48	-0.30	-0.09	0.11	0.30	0.46
	4.0	.29	.19	.06	-.07	-.22	-.35	-.69	-.52	-.30	-.12	-.01	.22
	7.0	.15	.06	-.08	-.20	-.34	-.50	-	-	-	-	-	-
	10.0	.07	-.03	-.14	-.24	-.38	-.52	-.63	-.90	-.36	-.22	-.05	.07
	15.0	-.01	-.10	-.23	-.32	-.42	-.53	-	-	-	-	-	-
	20.0	-.07	-.15	-.27	-.36	-.46	-.54	-.63	-.53	-.39	-.25	-.10	.01
	30.0	-.13	-.21	-.32	-.40	-.51	-.60	-.61	-.51	-.38	-.24	-.11	-.01
	40.0	-.15	-.21	-.32	-.40	-.50	-.57	-.56	-.49	-.35	-.24	-.12	-.03
	50.0	-.17	-.23	-.34	-.41	-.50	-.59	-.50	-.39	-.26	-.16	-.08	-.01
	60.0	-.17	-.22	-.32	-.41	-.50	-.54	-.48	-.29	-.14	-.09	-.04	.01
	70.0	-.19	-.23	-.33	-.42	-.52	-.59	-.32	-.12	-.06	-.02	-.02	.05
	80.0	-.17	-.18	-.25	-.37	-.55	-.64	-	-	-	-	-	-
	90.0	-.03	-.01	-.03	-.03	-.09	-.18	0	.02	.03	.03	.04	.03
	95.0	.05	.06	.05	.02	-.04	-.13	-.05	.06	.05	.05	.02	-.01
0.19 b/2	0	.23	.37	.50	.59	.64	.61	-	-	-	-	-	-
	1.5	.51	.43	.29	.14	-.07	-.28	-.73	-.58	-.29	-.02	.23	.40
	4.0	.29	.18	.02	-.14	-.34	-.54	-.89	-.83	-.50	-.24	-.01	.19
	7.0	.15	.04	-.11	-.25	-.43	-.59	-	-	-	-	-	-
	10.0	.04	-.07	-.23	-.35	-.53	-.66	-.94	-.79	-.54	-.32	-.12	.02
	15.0	-.03	-.15	-.30	-.43	-.60	-.76	-.91	-.75	-.53	-.33	-.14	-.03
	20.0	-.12	-.21	-.36	-.48	-.61	-.79	-.89	-.71	-.50	-.31	-.15	-.04
	30.0	-.19	-.28	-.42	-.53	-.69	-.81	-.69	-.65	-.42	-.26	-.14	-.05
	40.0	-.23	-.31	-.44	-.54	-.67	-.79	-.63	-.49	-.21	-.19	-.10	-.04
	50.0	-.24	-.32	-.44	-.55	-.68	-.78	-	-	-	-	-	-
	60.0	-.22	-.24	-.40	-.52	-.67	-.78	-.18	-.10	-.08	-.04	.01	.02
	70.0	-.20	-.22	-.27	-.45	-.64	-.74	-.04	-.02	-.01	-.02	.05	.06
	80.0	-.13	-.14	-.16	-.13	-.20	-.19	-	-	-	-	-	-
	90.0	-.01	0	-.01	0	.02	-.05	.07	.07	.06	.09	.08	.05
	95.0	.07	.08	.08	.08	.07	-.05	.10	.10	.11	.12	.10	.03
0.31 b/2	0	.17	.20	.46	.57	.61	.58	-	-	-	-	-	-
	1.5	.51	.42	.28	.11	-.13	-.34	-.71	-.60	-.36	-.04	.25	.41
	4.0	.26	.15	.02	-.19	-.42	-.62	-.94	-.90	-.60	-.26	-.03	.21
	7.0	.13	.02	-.15	-.33	-.55	-.71	-	-	-	-	-	-
	10.0	.04	-.08	-.24	-.40	-.62	-.76	-.99	-.97	-.63	-.36	-.11	.03
	15.0	-.09	-.20	-.37	-.52	-.70	-.86	-.99	-.98	-.68	-.34	-.15	-.02
	20.0	-.15	-.24	-.42	-.57	-.74	-.89	-.97	-.92	-.70	-.38	-.13	-.03
	30.0	-.23	-.29	-.48	-.62	-.81	-.95	-.93	-.75	-.56	-.20	-.10	-.03
	40.0	-.24	-.31	-.51	-.67	-.86	-.98	-.71	-.51	-.34	-.14	-.08	-.02
	50.0	-.24	-.29	-.40	-.61	-.82	-.98	-.33	-.10	-.11	-.04	-.02	.02
	60.0	-.20	-.24	-.28	-.49	-.80	-.98	-	-	-	-	-	-
	70.0	-.18	-.20	-.25	-.22	-.32	-.49	.01	0	.01	.06	.06	.07
	80.0	-.13	-.13	-.17	-.14	-.11	-.29	-	-	-	-	-	-
	90.0	.01	.01	0	.01	.08	-.13	.07	.08	.09	.10	.11	.10
	95.0	.08	.08	.08	.09	.06	-.03	.09	.11	.11	.12	.11	.11
0.375 b/2	0	.13	.26	.46	.58	.61	.57	-	-	-	-	-	-
	1.5	.51	.42	.25	.03	-.24	-.51	-.79	-.66	-.33	-.01	.27	.42
	4.0	.31	.20	0	-.18	-.41	-.58	-.96	-.90	-.61	-.24	-.05	.21
	7.0	.15	.01	-.18	-.37	-.58	-.75	-	-	-	-	-	-
	10.0	-.05	-.08	-.27	-.46	-.65	-.83	-.99	-.98	-.68	-.30	-.09	.04
	15.0	-.06	-.18	-.38	-.56	-.75	-.90	-.95	-.91	-.62	-.31	-.13	-.01
	20.0	-.14	-.25	-.46	-.62	-.81	-.94	-.92	-.90	-.68	-.27	-.11	-.02
	30.0	-.19	-.29	-.49	-.69	-.88	-.96	-.73	-.53	-.25	-.21	-.09	-.03
	40.0	-.22	-.31	-.45	-.72	-.90	-.96	-.63	-.23	-.18	-.13	-.05	-.02
	50.0	-.22	-.28	-.35	-.63	-.86	-.95	-	-	-	-	-	-
	60.0	-.21	-.24	-.32	-.55	-.72	-.77	-.45	-.06	-.04	0	.03	.03
	70.0	-.18	-.20	-.24	-.20	-.31	-.62	-.20	0	.02	.09	.08	.08
	80.0	-.12	-.13	-.15	-.13	-.22	-.53	-	-	-	-	-	-
	90.0	.01	0	0	.01	.05	-.13	.11	.08	.09	.10	.11	.09
	95.0	.09	.08	.09	.09	.05	-.13	.12	.10	.11	.11	.11	.09
0.44 b/2	0	.11	.27	.45	.58	.61	.56	-	-	-	-	-	-
	1.5	.51	.41	.23	0	-.26	-.51	-.76	-.69	-.33	-.01	.30	.45
	4.0	.31	.20	0	-.21	-.44	-.62	-.86	-.95	-.64	-.23	-.04	.21
	7.0	.15	.04	-.17	-.37	-.59	-.74	-	-	-	-	-	-
	10.0	-.05	-.06	-.26	-.46	-.70	-.85	-.83	-.90	-.59	-.30	-.08	.05
	15.0	-.06	-.17	-.39	-.58	-.78	-.93	-.74	-.89	-.51	-.30	-.11	-.01
	20.0	-.13	-.23	-.43	-.64	-.83	-.96	-.67	-.77	-.46	-.29	-.10	-.01
	30.0	-.20	-.30	-.46	-.70	-.89	-.92	-.57	-.42	-.25	-.19	-.09	-.02
	40.0	-.23	-.29	-.44	-.67	-.84	-.85	-.51	-.27	-.19	-.13	-.05	-.02
	50.0	-.21	-.27	-.38	-.60	-.81	-.68	-.48	-.17	-.10	-.04	-.01	.01
	60.0	-.22	-.25	-.32	-.55	-.77	-.57	-.41	-.10	-.04	0	.03	.04
	70.0	-.19	-.20	-.24	-.21	-.41	-.50	-.34	-.03	-.03	.06	.09	.07
	80.0	-.14	-.14	-.15	-.13	-.29	-.44	-	-	-	-	-	-
	90.0	-.06	-.01	0	.01	-.13	-.38	-.15	.06	.09	.09	.10	-.02
	95.0	-.02	.07	.09	.08	-.01	-.34	-.12	.09	.11	.11	.10	-.10

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TABLE X. - PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING.
 $M_\infty = 0.90$; $R = 2,000,000$ - Continued
(a) $\alpha_u = -4^\circ, -2^\circ, 0^\circ, 2^\circ, 4^\circ, 6^\circ$ - Concluded

Spanwise station	Percent chord	Upper surface						Lower surface						
		Angle of attack					Angle of attack	Angle of attack						
		-4°	-2°	0°	2°	4°		-4°	-2°	0°	2°	4°	6°	
0.56 b/2	0	0.16	0.28	0.47	0.59	0.60	0.53	---	---	-0.46	-0.46	-0.04	0.29	0.42
	1.5	.53	.46	.29	.06	-.23	-.47	-0.50	-0.78	-0.46	-0.24	.07	.21	
	4.0	.32	.23	.03	-.19	-.45	-.65	-.63	-.93	-.64	-.24	-.08	.04	
	7.0	.17	.06	-.13	-.35	-.59	-.73	---	---	---	---	---	---	
	10.0	.06	-.04	-.26	-.45	-.67	-.74	-.56	-.89	-.59	-.32	-.08	.04	
	15.0	-.06	-.15	-.36	-.60	-.82	-.75	-.52	-.83	-.52	-.30	-.11	-.03	
	20.0	-.11	-.19	-.39	-.61	-.80	-.72	-.49	-.69	-.48	-.24	-.08	-.03	
	30.0	-.19	-.26	-.42	-.64	-.78	-.57	-.44	-.42	-.24	-.18	-.08	-.03	
	40.0	-.23	-.26	-.41	-.60	-.58	-.46	-.38	-.23	-.15	-.11	-.03	-.04	
	50.0	-.25	-.28	-.38	-.51	-.43	-.39	-.34	-.18	-.09	-.04	-.03	-.03	
	60.0	-.24	-.23	-.31	-.24	-.32	-.35	---	---	---	---	---	---	
	70.0	-.27	-.20	-.23	-.21	-.22	-.31	-.27	-.02	-.03	-.03	-.03	-.02	
0.68 b/2	0	-.27	-.15	-.15	-.13	-.17	-.30	-.22	-.03	-.08	-.09	-.03	-.08	
	1.5	0	-.04	-.01	-.02	-.01	-.11	-.27	-.06	-.11	-.11	-.02	-.08	
	4.0	0	-.02	-.09	-.30	-.54	-.80	-.56	-.90	-.64	-.30	-.09	0	
	7.0	0	-.08	0	-.22	-.48	-.71	-.80	-.52	-.68	-.56	-.29	-.13	
	10.0	0	-.10	-.17	-.36	-.61	-.78	-.73	-.47	-.54	-.35	-.12	-.06	
	15.0	0	-.02	-.09	-.30	-.54	-.80	-.78	-.52	-.68	-.56	-.23	-.12	
	20.0	0	-.10	-.17	-.36	-.61	-.78	-.73	-.47	-.54	-.35	-.12	-.06	
	30.0	0	-.18	-.22	-.38	-.60	-.75	-.60	-.43	-.42	-.23	-.16	-.08	
	40.0	0	-.24	-.25	-.38	-.53	-.58	-.47	-.40	-.29	-.15	-.09	-.07	
	50.0	0	-.27	-.25	-.34	-.40	-.37	-.36	---	---	---	---	---	
	60.0	0	-.26	-.20	-.29	-.27	-.28	-.31	-.29	-.13	-.02	-.02	-.01	
	70.0	0	-.28	-.19	-.22	-.22	-.18	-.23	-.22	-.05	-.02	-.03	-.04	
0.80 b/2	0	-.28	-.14	-.14	-.13	-.12	-.21	-.21	-.17	0	-.08	-.10	-.05	
	1.5	0	-.16	0	-.01	-.02	-.05	-.18	-.12	-.07	-.11	-.11	-.03	
	4.0	0	-.11	0	-.06	-.09	-.10	-.03	-.13	0	-.13	0	-.06	
	7.0	0	-.09	-.12	-.30	-.36	-.79	-.88	-.55	-.61	-.43	-.16	-.09	
	10.0	0	-.16	-.17	-.32	-.41	-.50	-.73	-.48	-.48	-.23	-.17	-.09	
	15.0	0	-.01	-.05	-.25	-.49	-.74	-.88	-.55	-.61	-.43	-.16	-.09	
	20.0	0	-.09	-.12	-.30	-.36	-.79	-.88	-.50	-.51	-.50	-.26	-.13	
	30.0	0	-.16	-.17	-.32	-.41	-.50	-.73	-.48	-.48	-.23	-.17	-.09	
	40.0	0	-.21	-.20	-.32	-.41	-.58	-.74	---	---	---	---	---	
	50.0	0	-.25	-.22	-.30	-.36	-.30	-.44	-.40	-.28	-.09	-.04	-.04	
	60.0	0	-.24	-.20	-.27	-.26	-.21	-.31	-.34	-.18	-.02	-.01	-.01	
	70.0	0	-.23	-.17	-.22	-.22	-.15	-.20	-.26	-.10	-.04	-.05	.01	
0.94 b/2	0	-.23	-.13	-.13	-.13	-.08	-.12	-.21	-.21	-.04	-.16	-.09	.07	
	1.5	0	-.15	-.01	0	-.02	-.03	-.02	-.13	-.04	-.11	-.12	.08	
	4.0	0	-.10	-.01	0	-.09	-.10	-.06	-.11	-.06	-.14	-.14	.09	
	7.0	0	-.07	-.10	-.17	-.19	-.11	-.33	-.46	-.59	-.98	-.52	-.02	
	10.0	0	-.52	-.51	-.40	-.19	-.11	-.33	---	---	---	---	---	
	15.0	0	-.37	-.35	-.21	-.02	-.32	-.49	---	---	---	---	---	
	20.0	0	-.05	-.07	-.21	-.38	-.64	-.73	---	---	---	---	---	
	30.0	0	-.15	-.15	-.27	-.41	-.60	-.65	---	---	---	---	---	
	40.0	0	-.21	-.20	-.28	-.38	-.57	-.50	---	---	---	---	---	
	50.0	0	-.29	-.24	-.30	-.34	-.31	-.26	---	---	---	---	---	
	60.0	0	-.30	-.22	-.24	-.29	-.15	-.18	---	---	---	---	---	
	70.0	0	-.28	-.18	-.19	-.10	-.12	-.09	---	---	---	---	---	
	80.0	0	-.23	-.14	-.11	-.05	-.05	-.04	---	---	---	---	---	
	90.0	0	-.13	-.03	-.07	-.07	-.07	-.02	---	---	---	---	---	
	95.0	0	-.10	-.01	-.12	-.13	-.12	-.03	---	---	---	---	---	

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TABLE X.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING.
 $M_\infty = 0.90$; 2,000,000 - Continued

(b) a_u , 8° , 10° , 12°

Spanwise station	Percent chord	Upper surface			Lower surface		
		Angle of attack			Angle of attack		
		8°	10°	12°	8°	10°	12°
0.10 b/2	0	0.68	0.62	0.57	-	-	-
	1.5	-.36	-.36	-.36	0.59	0.67	0.76
	4.0	-.52	-.69	-.85	-.37	.48	.59
	7.0	-.67	-.82	-.98	-	-	-
	10.0	-.66	-.84	-.98	-.19	.29	.40
	15.0	-.66	-.81	-.93	-.13	.22	.31
	20.0	-.66	-.78	-.94	-.10	.18	.27
	30.0	-.69	-.79	-.82	-.06	.13	.21
	40.0	-.67	-.73	-.80	-.03	.11	.18
	50.0	-.62	-.71	-.78	-.03	.11	.17
	60.0	-.62	-.69	-.74	-.06	.11	.15
	70.0	-.66	-.73	-.79	-.07	.12	.16
	80.0	-.72	-.79	-.83	-	-	-
	90.0	-.30	-.43	-.49	-.02	.02	.03
	95.0	-.25	-.37	-.43	-.03	-.06	-.06
0.19 b/2	0	.55	.46	.40	-	-	-
	1.5	-.92	-.69	-.63	-.53	.61	.68
	4.0	-.75	-.96	-.12	-.32	.44	.54
	7.0	-.81	-.98	-.15	-	-	-
	10.0	-.84	-.100	-.18	-.16	.28	.36
	15.0	-.93	-.107	-.22	-.08	.18	.27
	20.0	-.94	-.108	-.22	-.08	.15	.22
	30.0	-.94	-.109	-.21	-.03	.09	.16
	40.0	-.93	-.109	-.21	-.04	.09	.15
	50.0	-.92	-.106	-.17	-	-	-
	60.0	-.85	-.90	-.01	-.05	.07	.11
	70.0	-.82	-.88	-.89	-.07	.07	.10
	80.0	-.26	-.31	-.56	-	-	-
	90.0	-.20	-.26	-.48	-.01	-.01	-.03
	95.0	-.22	-.29	-.46	-.03	-.07	-.10
0.31 b/2	0	.50	.40	.28	-	-	-
	1.5	-.38	-.73	-.88	-.53	.59	.64
	4.0	-.84	-.99	1.14	-.35	.44	.51
	7.0	-.93	-.108	-.18	-	-	-
	10.0	-.96	-.110	-.19	-.15	.25	.32
	15.0	-.103	-.116	-.17	-.06	.17	.25
	20.0	-.104	-.117	-.15	-.06	.13	.20
	30.0	-.110	-.117	-.08	-.04	.09	.13
	40.0	-.109	-.117	-.02	-.03	.07	.10
	50.0	-.107	-.108	-.93	-	-	-
	60.0	-.103	-.97	-.87	-	-	-
	70.0	-.85	-.85	-.80	-.07	.07	.09
	80.0	-.77	-.84	-.78	-	-	-
	90.0	-.18	-.70	-.72	-.07	.01	.12
	95.0	.13	-.60	-.69	-.11	-.07	-.20
0.375 b/2	0	.48	.37	.25	-	-	-
	1.5	-.75	-.90	-.00	-.52	.59	.61
	4.0	-.83	-.101	-.06	-.34	.42	.49
	7.0	-.90	-.107	-.03	-	-	-
	10.0	-.98	-.111	-.02	-.16	.25	.31
	15.0	-.106	-.111	-.97	-.09	.16	.23
	20.0	-.110	-.112	-.92	-.06	.12	.18
	30.0	-.107	-.103	-.85	-.04	.08	.12
	40.0	-.106	-.97	-.82	-.04	.06	.08
	50.0	-.90	-.85	-.73	-	-	-
	60.0	-.81	-.78	-.74	-.06	.03	.04
	70.0	-.70	-.71	-.71	-.09	.03	.01
	80.0	-.68	-.71	-.71	-.01	-.10	-.16
	90.0	-.62	-.65	-.67	-.10	-.20	-.24
	95.0	-.54	-.58	-.63	-	-	-
0.44 b/2	0	.48	.37	.27	-	-	-
	1.5	-.72	-.83	-.83	-.55	.59	.61
	4.0	-.86	-.98	-.83	-.33	.41	.46
	7.0	-.92	-.97	-.86	-	-	-
	10.0	-.100	-.96	-.78	-.16	.24	.30
	15.0	-.100	-.93	-.73	-.09	.15	.21
	20.0	-.99	-.88	-.71	-.07	.12	.16
	30.0	-.88	-.75	-.67	-.03	.07	.09
	40.0	-.76	-.71	-.64	-.02	.03	.03
	50.0	-.67	-.65	-.63	-.04	.03	.04
	60.0	-.60	-.62	-.60	-.04	.02	0
	70.0	-.57	-.60	-.61	-.03	.01	-
	80.0	-.58	-.59	-.61	-	-	-
	90.0	-.52	-.55	-.57	-.11	-.16	-.19
	95.0	-.48	-.58	-.56	-.18	-.23	-.27

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TABLE X.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING.
 $M_\infty = 0.90$; $R = 2,000,000$ - Concluded
 (b) $\alpha_u = 8^\circ, 10^\circ, 12^\circ$ - Concluded

Spanwise station	Per-cent chord	Upper surface			Lower surface		
		Angle of attack			Angle of attack		
		8°	10°	12°	8°	10°	12°
0.56 b/2	0	0.43	0.33	0.23	-	-	-
	1.5	-.67	-.71	-.63	0.51	0.56	0.58
	4.0	-.70	-.83	-.59	.32	.39	.44
	7.0	-.69	-.63	-.59	-	-	-
	10.0	-.66	-.59	-.58	.14	.20	.26
	15.0	-.54	-.52	-.53	.07	.12	.16
	20.0	-.48	-.51	-.54	.05	.09	.13
	30.0	-.43	-.48	-.53	-.01	.02	.05
	40.0	-.41	-.46	-.52	-.01	0	.02
	50.0	-.40	-.45	-.51	-.03	-.02	0
	60.0	-.39	-.44	-.51	-	-	-
	70.0	-.37	-.42	-.51	-.03	-.04	-.04
	80.0	-.36	-.41	-.50	-.04	-.06	-.08
	90.0	-.35	-.40	-.48	-.14	-.15	-.18
	95.0	-.34	-.38	-.46	-.20	-.22	-.25
0.68 b/2	0	.05	.05	.03	-	-	-
	1.5	-.57	-.72	-.57	.46	.50	.54
	4.0	-.86	-.89	-.58	.26	.33	.39
	7.0	-.89	-.91	-.57	-	-	-
	10.0	-.87	-.88	-.53	.09	.16	.21
	15.0	-.82	-.82	-.52	.01	.07	.12
	20.0	-.71	-.77	-.50	-.01	.05	.08
	30.0	-.59	-.69	-.49	-.04	-.08	.01
	40.0	-.54	-.68	-.48	-.06	-.03	-.02
	50.0	-.47	-.63	-.47	-	-	-
	60.0	-.41	-.57	-.47	-.04	-.04	-.03
	70.0	-.35	-.48	-.45	-.03	-.05	-.08
	80.0	-.32	-.41	-.45	-.04	-.07	-.09
	90.0	-.28	-.36	-.43	-.10	-.14	-.19
	95.0	-.26	-.33	-.42	-.14	-.19	-.26
0.80 b/2	0	.48	.37	.31	-	-	-
	1.5	-.64	-.80	-.71	.43	.50	.51
	4.0	-.80	-.91	-.64	.21	.30	.33
	7.0	-.89	-.94	-.63	-	-	-
	10.0	-.94	-.90	-.61	.06	.13	.16
	15.0	-.94	-.88	-.55	.02	.05	.08
	20.0	-.91	-.81	-.54	-.02	.03	.05
	30.0	-.90	-.70	-.50	-.03	-.03	-.02
	40.0	-.75	-.65	-.50	-	-	-
	50.0	-.62	-.58	-.47	-.04	-.04	-.06
	60.0	-.54	-.56	-.45	-.02	-.03	-.07
	70.0	-.44	-.49	-.42	.01	-.02	-.07
	80.0	-.34	-.45	-.40	.02	-.01	-.10
	90.0	-.23	-.36	-.37	.01	-.08	-.14
	95.0	-.16	-.32	-.35	-.01	-.12	-.20
0.94 b/2	0	.53	.43	.38	-	-	-
	1.5	-.56	-.73	-.93	.36	.44	.47
	4.0	-.66	-.68	-.92	-	-	-
	7.0	-.67	-.68	-.93	.10	.17	.21
	10.0	-.62	-.64	-.93	.02	.07	.12
	15.0	-.62	-.59	-.83	.03	.08	.04
	20.0	-.53	-.55	-.85	.04	-.01	.01
	30.0	-.38	-.46	-.75	.09	-.05	-.04
	40.0	-.34	-.43	-.71	.10	-.09	-.09
	50.0	-.25	-.37	-.64	.10	-.09	-.12
	60.0	-.22	-.35	-.62	-	-	-
	70.0	-.18	-.30	-.53	.07	-.09	-.13
	80.0	-.17	-.28	-.44	.05	-.08	-.09
	90.0	-.14	-.24	-.34	.07	-.10	-.10
	95.0	-.14	-.24	-.27	.09	-.15	-.13

TABLE XI.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING.

 $M_\infty = 0.25$; $R = 8,000,000$ (a) $\alpha_u = -4^\circ, -2^\circ, 0^\circ, 2^\circ, 4^\circ, 6^\circ$

Spanwise station	Percent chord	Upper surface						Lower surface					
		Angle of attack						Angle of attack					
		-4°	-2°	0°	2°	4°	6°	-4°	-2°	0°	2°	4°	6°
0.10 b/2	0	-0.25	0.16	0.43	0.59	0.57	0.47	---	-1.12	---	-0.31	-0.01	0.24
	1.5	.45	.23	.17	-.04	-.31	-.62	---	-.90	-.68	-.36	-.14	.06
	4.0	.28	.14	-.02	-.21	-.42	-.67	---	---	---	---	---	.25
	7.0	.15	.01	-.13	-.29	-.46	-.65	---	---	---	---	---	---
	10.0	.04	-.10	-.22	-.37	-.51	-.66	---	-.71	-.54	-.37	-.22	-.07
	15.0	-.07	-.17	-.28	-.40	-.52	-.65	---	-.64	-.52	-.37	-.24	-.12
	20.0	-.12	-.22	-.32	-.41	-.51	-.62	---	-.53	-.41	-.29	-.19	-.09
	30.0	-.14	-.23	-.39	-.47	-.53	-.63	---	-.41	-.34	-.24	-.16	-.08
	40.0	-.18	-.20	-.36	-.43	-.59	-.65	---	-.33	-.23	-.19	-.13	-.06
	50.0	-.10	-.16	-.20	-.25	-.30	-.35	---	-.25	-.20	-.14	-.10	-.04
	60.0	-.10	-.16	-.20	-.23	-.27	-.30	---	-.16	-.12	-.08	0	.06
	70.0	-.10	-.14	-.17	-.20	-.23	-.26	---	-.10	-.06	0	.04	.08
	80.0	-.10	-.11	-.13	-.16	-.18	-.19	---	---	---	---	---	---
	90.0	-.03	-.03	-.03	-.06	-.04	-.04	---	-.02	-.02	.04	.03	.06
	95.0	.05	.04	.04	.03	.03	.03	---	.04	.05	.05	.05	.07
0.19 b/2	0	.45	.06	.40	.55	.53	.32	---	---	---	---	---	---
	1.5	.20	.37	.17	-.13	-.50	-.96	---	-.27	-.74	-.30	.04	.30
	4.0	.27	.08	-.12	-.37	-.64	-.95	---	-.99	-.66	-.36	-.11	.21
	7.0	.16	.01	-.15	-.34	-.54	-.77	---	---	---	---	---	---
	10.0	.10	-.06	-.20	-.37	-.55	-.74	---	-.77	-.52	-.33	-.17	.01
	15.0	-.03	-.16	-.29	-.43	-.58	-.73	---	-.59	-.44	-.30	-.17	.05
	20.0	-.02	-.14	-.24	-.35	-.47	-.59	---	-.49	-.36	-.26	-.15	.05
	30.0	-.13	-.22	-.30	-.39	-.48	-.56	---	-.36	-.24	-.20	-.13	.03
	40.0	-.17	-.24	-.30	-.37	-.44	-.51	---	-.26	-.21	-.15	-.09	.03
	50.0	-.14	-.19	-.24	-.31	-.35	-.40	---	---	---	---	---	---
	60.0	-.12	-.18	-.21	-.25	-.29	-.31	---	-.11	-.09	-.04	-.02	.02
	70.0	-.12	-.16	-.18	-.21	-.23	-.25	---	-.04	-.02	-.01	.02	.05
	80.0	-.09	-.11	-.13	-.14	-.16	-.16	---	---	---	---	---	---
	90.0	-.01	-.03	-.04	-.03	-.03	-.02	---	.04	.05	.06	.06	.09
	95.0	.04	.05	.05	.04	.04	.05	---	.06	.05	.06	.06	.06
0.31 b/2	0	-.51	.05	.41	.55	.51	.27	---	---	---	---	---	---
	1.5	.35	.43	.23	-.08	-.44	-.92	---	-.136	-.79	-.50	.06	.33
	4.0	.35	.17	-.03	-.31	-.59	-.92	---	-.108	-.70	-.36	.08	.31
	7.0	.20	.04	-.16	-.36	-.60	-.86	---	---	---	---	---	---
	10.0	.12	-.09	-.20	-.36	-.58	-.80	---	-.71	-.52	-.31	-.14	.01
	15.0	.02	-.12	-.23	-.40	-.56	-.73	---	-.60	-.45	-.30	-.16	.04
	20.0	-.03	-.16	-.26	-.39	-.52	-.66	---	-.47	-.36	-.24	-.14	.03
	30.0	-.10	-.19	-.28	-.37	-.46	-.55	---	-.35	-.26	-.19	-.11	.05
	40.0	-.12	-.21	-.27	-.35	-.43	-.50	---	-.25	-.20	-.13	-.07	.01
	50.0	-.15	.21	-.26	-.34	-.43	-.53	---	-.15	-.13	-.07	-.03	.01
	60.0	-.13	-.17	-.21	-.26	-.30	-.33	---	---	---	---	---	---
	70.0	-.11	-.15	-.18	-.21	-.24	-.26	---	-.02	-.01	.02	.04	.10
	80.0	-.08	-.11	-.14	-.15	-.16	-.17	---	---	---	---	---	---
	90.0	-.01	-.02	-.01	-.02	-.02	-.02	---	.06	.06	.07	.06	.10
	95.0	.05	.05	.06	.05	.05	.06	---	.09	.08	.09	.09	.10
0.375 b/2	0	-.61	0	.34	.54	.51	.23	---	---	---	---	---	---
	1.5	.24	.41	.10	-.15	-.56	-.99	---	-.136	-.79	-.30	.07	.35
	4.0	.37	.20	-.01	-.28	-.57	-.90	---	-.107	-.69	-.36	.14	.32
	7.0	.22	.04	-.14	-.39	-.60	-.87	---	---	---	---	---	---
	10.0	.12	-.04	-.20	-.41	-.59	-.81	---	-.72	-.51	-.31	-.14	.16
	15.0	.02	-.12	-.25	-.40	-.57	-.74	---	-.60	-.44	-.26	-.15	.02
	20.0	-.03	-.10	-.26	-.40	-.53	-.67	---	-.49	-.36	-.24	-.13	.07
	30.0	-.04	-.14	-.22	-.31	-.40	-.50	---	-.35	-.27	-.19	-.10	.02
	40.0	-.13	-.20	-.30	-.35	-.42	-.50	---	-.29	-.21	-.13	-.07	.05
	50.0	-.13	-.19	-.24	-.30	-.35	-.41	---	---	---	---	---	---
	60.0	-.12	-.17	-.21	-.25	-.30	-.35	---	-.10	-.07	-.03	0	.05
	70.0	-.12	-.16	-.19	-.22	-.25	-.27	---	-.03	-.01	.01	.04	.09
	80.0	-.10	-.12	-.14	-.16	-.17	-.19	---	---	---	---	---	---
	90.0	-.01	-.02	-.03	-.04	-.04	-.04	---	.05	.05	.06	.07	.09
	95.0	.05	.04	.04	.04	.04	.04	---	.06	.08	.08	.08	.09
0.44 b/2	0	-.65	-.02	.38	.55	.51	.29	---	---	---	---	---	---
	1.5	.23	.40	.17	.15	.56	-.07	---	-.149	-.85	-.32	.09	.37
	4.0	.36	.20	-.02	-.30	-.61	-.92	---	-.111	-.72	-.40	.09	.33
	7.0	.22	.05	-.15	-.25	-.41	-.62	---	---	---	---	---	---
	10.0	.14	-.02	-.20	-.41	-.60	-.83	---	-.13	-.78	-.33	-.14	.03
	15.0	.04	-.11	-.25	-.41	-.56	-.75	---	-.60	-.44	-.29	-.14	.02
	20.0	-.02	-.15	-.27	-.39	-.52	-.68	---	-.49	-.36	-.23	-.12	.02
	30.0	-.10	-.19	-.29	-.39	-.48	-.60	---	-.35	-.27	-.18	-.10	.02
	40.0	-.11	-.19	-.27	-.35	-.42	-.50	---	-.26	-.20	-.14	-.06	.05
	50.0	-.12	-.19	-.24	-.30	-.35	-.41	---	-.17	-.12	-.07	.02	.03
	60.0	-.12	-.17	-.21	-.26	-.30	-.34	---	-.10	-.07	-.03	.05	.07
	70.0	-.11	-.15	-.19	-.21	-.24	-.26	---	-.03	0	.02	.05	.10
	80.0	-.09	-.11	-.13	-.15	-.16	-.17	---	---	---	---	---	---
	90.0	0	-.01	-.02	-.03	-.03	-.03	---	.04	.03	.06	.07	.09
	95.0	.06	.05	.05	.05	.05	.05	---	.08	.08	.08	.09	.09

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TABLE XI.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING.
 $M_\infty = 0.25$; $R = 8,000,000$ - Continued
(a) α_u , $-4^\circ, -2^\circ, 0^\circ, 2^\circ, 4^\circ, 6^\circ$, - Concluded

Spanwise station	Per-cent chord	Upper surface						Lower surface					
		Angle of attack						Angle of attack					
		-4°	-2°	0°	2°	4°	6°	-4°	-2°	0°	2°	4°	6°
0.56 b/2	0	-0.77	-0.10	0.35	0.53	0.49	0.16	---	---	-1.01	-0.42	0.04	0.35
	1.5	.54	.43	.21	-.12	-.54	-1.08	-1.71	---	-.74	-.42	-.08	.15
	4.0	.39	.22	.01	-.28	-.59	-.93	-.12	---	-.46	-.29	-.15	.34
	7.0	.24	.08	-.12	-.34	-.59	-.88	---	---	---	---	---	---
	10.0	.15	-.01	-.18	-.39	-.59	-.82	-.77	-.54	-.35	-.14	.02	.16
	15.0	.06	-.09	-.23	-.39	-.55	-.74	-.62	-.46	-.29	-.15	.02	.09
	20.0	0	-.11	-.24	-.36	-.49	-.64	-.50	-.36	-.22	-.12	-.01	.06
	30.0	-.05	-.13	-.24	-.34	-.42	-.54	-.36	-.26	-.16	-.10	-.02	.06
	40.0	-.10	-.18	-.25	-.33	-.40	-.48	-.24	-.19	-.11	-.05	.01	.06
	50.0	-.11	-.18	-.23	-.30	-.35	-.41	-.16	-.12	-.07	-.02	.02	.07
	60.0	-.10	-.15	-.20	-.25	-.29	-.32	---	---	---	---	---	---
	70.0	-.10	-.13	-.17	-.20	-.23	-.25	-.03	0	.02	.05	.07	.16
0.68 b/2	80.0	-.08	-.10	-.12	-.14	-.16	-.17	-.03	.04	.06	.07	.09	.11
	90.0	-.01	-.01	-.02	-.03	-.03	-.03	.06	.06	.07	.08	.09	.10
	95.0	.06	.05	.06	.05	.06	.06	.09	.09	.09	.09	.10	.10
0.80 b/2	0	---	---	---	---	---	---	-1.87	-1.14	-.52	-.04	.29	.48
	1.5	.56	.49	.30	.01	-.37	-.90	-1.21	-.84	-.48	-.15	.10	.29
	4.0	.41	.29	.02	-.23	-.58	-.94	---	---	---	---	---	---
	7.0	.28	.12	-.07	-.30	-.55	-.87	---	---	---	---	---	---
	10.0	.18	.03	-.14	-.35	-.54	-.78	-.81	-.57	-.35	-.16	.01	.14
	15.0	.10	-.04	-.18	-.34	-.52	-.68	-.64	-.47	-.31	-.16	-.03	.10
	20.0	.03	-.09	-.22	-.35	-.48	-.62	-.50	-.37	-.25	-.12	-.02	.09
	30.0	-.04	-.14	-.24	-.34	-.44	-.57	-.35	-.26	-.18	-.10	-.01	.06
	40.0	-.06	-.14	-.22	-.30	-.39	-.46	-.25	-.18	-.13	-.05	0	.06
	50.0	-.09	-.15	-.21	-.27	-.34	-.40	---	---	---	---	---	---
	60.0	-.08	-.13	-.18	-.23	-.27	-.31	-.09	-.06	-.02	.01	.02	.08
	70.0	-.08	-.12	-.15	-.18	-.21	-.24	-.03	-.01	.01	.02	.06	.09
0.94 b/2	80.0	-.06	-.09	-.11	-.12	-.15	-.16	-.02	.03	.05	.07	.08	.10
	90.0	-.01	0	0	-.01	-.02	-.03	.06	.06	.07	.08	.09	.10
	95.0	.06	.06	.06	.05	.05	.05	.09	.09	.09	.10	.10	.11

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TABLE XI.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING.

 $M_\infty = 0.25; R = 8,000,000$ - Continued(b) $\alpha_u = 8^\circ, 10^\circ, 12^\circ, 14^\circ, 16^\circ, 18^\circ$

Spanwise station	Per-cent chord	Upper surface						Lower surface						
		Angle of attack						Angle of attack						
		8°	10°	12°	14°	16°	18°	8°	10°	12°	14°	16°	18°	
0.10 b/2	0	0.22	-0.12	-0.61	-1.20	-1.89	-2.43	---	0.56	0.63	0.65	0.62	0.56	0.48
	1.5	-1.02	-1.42	-1.94	-2.48	-3.04	-3.43	---	.39	.31	.31	.38	.32	.24
	4.0	-.94	-1.22	-1.58	-1.92	-2.27	-2.49	---	---	---	---	---	---	---
	7.0	-.88	-1.10	-1.35	-1.60	-1.84	-2.00	---	---	---	---	---	---	---
	10.0	-.85	-1.03	-1.23	-1.42	-1.61	-1.72	---	.19	.29	.40	.50	.57	.62
	15.0	-.80	-0.93	-1.08	-1.22	-1.35	-1.44	---	.11	.21	.31	.38	.46	.51
	20.0	-.74	-.85	-.97	-1.08	-1.16	-1.24	---	.11	.19	.27	.35	.42	.47
	30.0	-.61	-.69	-.76	-.83	-.90	-.96	---	.06	.15	.21	.27	.34	.38
	40.0	-.50	-.56	-.61	-.66	-.70	-.72	---	.07	.13	.19	.25	.29	.33
	50.0	-.40	-.44	-.48	-.51	-.54	-.55	---	.07	.12	.17	.22	.26	.29
	60.0	-.34	-.38	-.39	-.42	-.43	-.43	---	.10	.13	.19	.22	.26	.29
	70.0	-.30	-.30	-.31	-.33	-.33	-.33	---	.11	.13	.19	.22	.23	.27
	80.0	-.21	-.21	-.21	-.22	-.21	-.22	---	---	---	---	---	---	---
	90.0	-.05	-.07	-.05	-.06	-.07	-.09	---	.10	.11	.12	.14	.16	.18
	95.0	.02	.02	0	-.01	-.01	-.02	---	.07	.09	.10	.10	.11	.12
0.19 b/2	0	-.08	-.64	-1.41	-2.33	-3.39	-4.21	---	---	---	---	---	---	---
	1.5	-1.52	-2.19	-2.95	-3.76	-4.61	-5.18	---	.57	.58	.59	.66	.76	.83
	4.0	-1.34	-1.72	-2.16	-2.63	-3.06	-3.35	---	.42	.52	.58	.60	.69	.77
	7.0	-1.05	-1.30	-1.63	-1.95	-2.25	-2.45	---	---	---	---	---	---	---
	10.0	-.98	-1.20	-1.45	-1.71	-1.94	-2.09	---	.24	.34	.43	.51	.56	.60
	15.0	-.91	-1.08	-1.27	-1.45	-1.61	-1.71	---	.18	.27	.35	.42	.48	.54
	20.0	-.74	-0.88	-1.02	-1.16	-1.26	-1.37	---	.14	.22	.30	.37	.43	.48
	30.0	-.67	-.76	-.85	-.94	-.101	-.106	---	.09	.16	.23	.29	.36	.40
	40.0	-.58	-.65	-.70	-.75	-.80	-.83	---	.09	.15	.20	.26	.30	.33
	50.0	-.45	-.49	-.52	-.56	-.56	-.60	---	---	---	---	---	---	---
	60.0	-.35	-.39	-.40	-.42	-.43	-.42	---	.10	.14	.18	.21	.23	.26
	70.0	-.26	-.28	-.29	-.29	-.29	-.27	---	.11	.14	.17	.20	.23	.25
	80.0	-.18	-.16	-.15	-.15	-.14	-.14	---	---	---	---	---	---	---
	90.0	-.08	-.02	-.02	-.03	-.06	-.09	---	.10	.10	.12	.12	.13	.14
	95.0	.04	.03	.01	-.02	-.04	-.07	---	.07	.07	.07	.07	.07	.06
0.31 b/2	0	-.19	-.84	-1.70	-2.75	-3.92	-4.84	---	---	---	---	---	---	---
	1.5	-1.50	-2.15	-2.92	-3.75	-4.61	-5.19	---	.57	.54	.42	.51	.67	.71
	4.0	-1.32	-1.74	-2.26	-2.71	-3.20	-3.60	---	.46	.55	.59	.63	.73	.77
	7.0	-1.16	-1.48	-1.82	-2.17	-2.50	-2.71	---	---	---	---	---	---	---
	10.0	-1.05	-1.30	-1.57	-1.83	-2.08	-2.24	---	.27	.36	.46	.52	.56	.59
	15.0	-.93	-1.12	-1.32	-1.52	-1.68	-1.79	---	.19	.29	.37	.43	.49	.53
	20.0	-.82	-.96	-1.13	-1.27	-1.40	-1.47	---	.16	.24	.32	.38	.44	.49
	30.0	-.67	-.76	-.87	-.95	-.102	-.105	---	.12	.17	.23	.30	.36	.39
	40.0	-.57	-.63	-.69	-.74	-.78	-.79	---	.11	.16	.21	.26	.30	.33
	50.0	-.48	-.52	-.56	-.58	-.58	-.56	---	.11	.15	.20	.23	.27	.30
	60.0	-.36	-.39	-.40	-.40	-.38	-.34	---	---	---	---	---	---	---
	70.0	-.27	-.29	-.27	-.25	-.21	-.19	---	.12	.15	.17	.20	.21	.24
	80.0	-.17	-.15	-.13	-.10	-.10	-.12	---	---	---	---	---	---	---
	90.0	-.01	0	.01	-.02	-.05	-.08	---	.10	.11	.12	.12	.11	.12
	95.0	.05	.05	.03	0	-.05	-.10	---	.10	.10	.10	.09	.08	.08
0.375 b/2	0	-.28	-1.00	-1.95	-3.10	-4.40	-5.39	---	---	---	---	---	---	---
	1.5	-1.74	-2.44	-3.32	-4.23	-5.16	-5.78	---	.57	.52	.39	.47	.51	.56
	4.0	-1.30	-1.72	-2.21	-2.71	-3.21	-3.53	---	.46	.54	.57	.63	.73	.77
	7.0	-1.18	-1.50	-1.87	-2.22	-2.53	-2.76	---	---	---	---	---	---	---
	10.0	-1.07	-1.32	-1.62	-1.88	-2.14	-2.29	---	.28	.38	.46	.52	.56	.59
	15.0	-.94	-1.13	-1.34	-1.54	-1.72	-1.81	---	.20	.29	.37	.44	.50	.53
	20.0	-.83	-.98	-1.15	-1.30	-1.42	-1.49	---	.17	.23	.32	.39	.44	.48
	30.0	-.62	-.73	-.83	-.92	-.99	-.103	---	.12	.19	.25	.31	.36	.40
	40.0	-.57	-.64	-.70	-.73	-.79	-.80	---	.11	.16	.21	.26	.31	.34
	50.0	-.46	-.51	-.55	-.58	-.60	-.60	---	---	---	---	---	---	---
	60.0	-.36	-.40	-.44	-.45	-.46	-.46	---	.11	.14	.18	.21	.25	.27
	70.0	-.29	-.31	-.32	-.34	-.36	-.36	---	.12	.14	.17	.20	.23	.24
	80.0	-.20	-.20	-.21	-.22	-.24	-.27	---	---	---	---	---	---	---
	90.0	-.04	-.04	-.05	-.07	-.10	-.13	---	.11	.11	.13	.14	.16	.17
	95.0	.04	.03	.01	0	-.02	-.04	---	.10	.10	.10	.11	.12	.13
0.44 b/2	0	-.26	-.97	-1.97	-3.14	-4.45	-5.41	---	---	---	---	---	---	---
	1.5	-1.71	-2.40	-3.23	-4.11	-5.00	-5.60	---	.57	.53	.35	.40	.44	.48
	4.0	-1.34	-1.78	-2.28	-2.79	-3.29	-3.61	---	.46	.55	.58	.62	.70	.74
	7.0	-1.22	-1.55	-1.92	-2.29	-2.63	-2.85	---	.28	.38	.46	.52	.56	.58
	10.0	-1.10	-1.36	-1.66	-1.93	-2.21	-2.36	---	.20	.30	.36	.44	.50	.53
	15.0	-.95	-1.15	-1.37	-1.57	-1.76	-1.85	---	.17	.23	.32	.39	.44	.48
	20.0	-.84	-1.00	-1.17	-1.32	-1.45	-1.53	---	.13	.20	.28	.31	.36	.40
	30.0	-.70	-.80	-.91	-1.00	-1.08	-1.13	---	.13	.18	.22	.26	.30	.34
	40.0	-.57	-.64	-.71	-.77	-.82	-.84	---	.10	.15	.18	.21	.25	.27
	50.0	-.46	-.52	-.56	-.60	-.62	-.62	---	.11	.15	.18	.21	.24	.26
	60.0	-.37	-.40	-.43	-.44	-.45	-.44	---	.11	.15	.18	.21	.25	.27
	70.0	-.28	-.29	-.30	-.29	-.28	-.28	---	.13	.15	.17	.20	.22	.25
	80.0	-.18	-.17	-.16	-.14	-.14	-.17	---	.10	.11	.12	.12	.12	.12
	90.0	-.02	-.02	-.02	-.04	-.07	-.11	---	.09	.09	.09	.09	.08	.08
	95.0	.05	.03	.01	0	-.02	-.04	---	.10	.10	.10	.11	.12	.13

TABLE XI.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING.

 $M_\infty = 0.25$; $R = 8,000,000$ - Concluded(b) $a_u = 8^\circ, 10^\circ, 12^\circ, 14^\circ, 16^\circ, 18^\circ$ - Concluded

Spanwise station	Per-cent chord	Upper surface						Lower surface					
		Angle of attack						Angle of attack					
		8°	10°	12°	14°	16°	18°	8°	10°	12°	14°	16°	18°
0.56 b/2	0	-0.44	-1.27	-2.39	-3.71	-5.17	-6.23	----	----	----	----	----	----
	1.5	-1.75	-2.50	-3.37	-4.31	-5.24	-5.85	0.57	0.53	0.34	0.06	-0.26	-0.58
	4.0	-1.35	-1.80	-2.32	-2.84	-3.36	-3.68	-4.7	-5.6	-5.8	-5.8	-5.4	-4.5
	7.0	-1.21	-1.53	-1.93	-2.31	-2.66	-2.87	----	----	----	----	----	----
	10.0	-1.09	-1.36	-1.66	-1.95	-2.21	-2.37	----	----	4.7	.52	.56	.58
	15.0	-.94	-1.14	-1.36	-1.57	-1.74	-1.84	.21	.30	.38	.44	.50	.53
	20.0	-.79	-.96	-1.12	-1.28	-1.41	-1.49	.18	.26	.33	.40	.45	.48
	30.0	-.66	-.77	-.87	-.97	-1.04	-1.08	.13	.19	.26	.31	.36	.39
	40.0	-.56	-.63	-.69	-.75	-.80	-.82	.12	.17	.22	.27	.31	.34
	50.0	-.46	-.52	-.55	-.59	-.62	-.63	.11	.15	.19	.23	.27	.30
	60.0	-.35	-.40	-.42	-.44	-.46	-.49	----	----	----	----	----	----
	70.0	-.27	-.29	-.30	-.31	-.32	-.36	.13	.15	.17	.20	.22	.25
	80.0	-.17	-.17	-.18	-.18	-.21	-.25	.13	.14	.16	.18	.20	.21
	90.0	-.01	-.03	-.03	-.06	-.10	-.14	.11	.11	.12	.13	.14	.15
	95.0	.05	-.03	0	-.02	-.05	-.09	.10	.09	.09	.09	.09	.10
0.68 b/2	0	----	----	----	----	----	----	----	----	----	----	----	----
	1.5	-1.55	-2.25	-3.11	-3.87	-4.76	-5.33	-.25	.53	.38	.15	-.17	-.45
	4.0	-1.34	-1.78	-2.32	-2.85	-3.36	-5.67	-.43	.53	.58	.58	.53	.46
	7.0	-1.16	-1.49	-1.89	-2.27	-2.61	-2.81	----	----	----	----	----	----
	10.0	-1.05	-1.32	-1.62	-1.93	-2.18	-2.33	.28	----	.46	.32	.56	.58
	15.0	-.91	-1.12	-1.35	-1.56	-1.74	-1.84	.20	----	.38	.44	.49	.53
	20.0	-.82	-.98	-1.17	-1.33	-1.46	-1.53	.17	----	.33	.39	.44	.47
	30.0	-.69	----	-1.90	-1.00	-1.08	-1.11	.13	----	.26	.33	.35	.39
	40.0	-.55	----	-.70	-.75	-.78	-.77	.12	----	.22	.28	.30	.32
	50.0	-.45	----	-.54	-.56	-.55	-.52	----	----	----	----	----	----
	60.0	-.34	----	-.39	-.40	-.33	-.30	.12	----	.19	.21	.23	.25
	70.0	-.26	----	-.26	-.24	-.20	-.18	.10	----	.16	.18	.20	.20
	80.0	-.16	----	-.13	-.10	-.10	-.13	.11	----	.15	.16	.16	.17
	90.0	0	----	-.01	-.01	-.04	-.11	.11	----	.12	.11	.11	.10
	95.0	.05	----	-.03	0	-.06	-.14	.09	----	.08	.08	.09	.04
0.80 b/2	0	-.36	-1.22	-2.39	-3.81	-5.35	-6.48	----	----	----	----	----	----
	1.5	-1.50	-2.21	-3.05	-3.76	-4.61	-5.15	-.53	.57	.46	.27	.01	-.24
	4.0	-1.18	-1.59	-2.10	-2.61	-3.08	-3.38	-.42	.53	.57	.56	.49	----
	7.0	-1.05	-1.37	-1.74	-2.11	-2.44	-2.63	----	----	----	----	----	----
	10.0	-.96	-1.22	-1.52	-1.80	-2.04	-2.19	.25	.37	.43	.49	.57	.57
	15.0	-.84	-1.04	-1.26	-1.47	-1.64	-1.74	.17	----	.36	.42	.47	.51
	20.0	-.74	-.90	-1.07	-1.22	-1.34	-1.41	.16	----	.31	.37	.43	.46
	30.0	-.59	-.69	-.81	-.90	-.98	-1.01	.11	----	.28	.29	.34	.37
	40.0	-.51	----	-.65	-.71	-.76	-.77	----	----	.18	.21	.24	----
	50.0	-.42	----	-.52	-.55	-.58	-.56	.09	----	.16	.19	.22	----
	60.0	-.33	----	-.39	-.40	-.40	-.39	.10	----	.16	.17	.20	.21
	70.0	-.25	----	-.28	-.27	-.23	-.25	.11	----	.13	.14	.15	.15
	80.0	-.15	----	-.14	-.13	-.13	-.13	.10	----	.13	.14	.15	.15
	90.0	-.02	----	-.01	-.04	-.08	-.13	.10	----	.11	.11	.11	.10
	95.0	.05	----	-.02	-.01	-.06	-.11	.10	----	.10	.09	.07	.07
0.94 b/2	0	.14	-.49	-1.42	-2.80	-3.93	-4.95	----	----	----	----	----	----
	1.5	-1.09	-1.66	-2.16	-2.86	-3.56	-4.00	-.50	.57	.53	.39	.18	-.04
	4.0	-.99	-1.37	-1.82	-2.26	-2.72	-2.99	-.24	.37	.45	.52	.56	----
	7.0	-.91	-1.15	-1.49	-1.61	-2.10	-2.29	----	----	----	----	----	----
	10.0	-.77	-1.03	-1.25	-1.50	-1.72	-1.85	.17	.29	.37	.43	.51	.53
	15.0	-.66	-.84	-1.02	-1.20	-1.35	-1.44	.12	----	.29	.35	.41	.45
	20.0	-.57	-.72	-.86	-1.01	-1.12	-1.19	.10	----	.28	.32	.35	.38
	30.0	-.41	-.52	-.62	-.71	-.77	-.82	.06	----	.18	.24	.26	.29
	40.0	-.40	----	-.51	-.58	-.61	-.63	0.06	----	.12	.16	.20	.21
	50.0	-.34	----	-.41	-.45	-.46	-.46	.06	----	.11	.13	.16	.17
	60.0	-.27	----	-.31	-.33	-.32	-.32	.07	----	.08	.09	.08	.10
	70.0	-.20	----	-.21	-.22	-.20	-.19	.07	----	.07	.08	.06	.06
	80.0	-.12	----	-.12	-.11	-.10	-.10	.07	----	.07	.08	.06	.06
	90.0	0	----	0	-.01	-.03	-.08	.07	----	.06	.05	.04	.02
	95.0	.06	----	-.03	.01	-.02	-.07	.09	----	.07	.05	.02	0



TABLE XII.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING.
 $M_\infty = 0.25$; $R = 2,000,000$
(a) c_{u_1} , $-2^\circ, 0^\circ, 2^\circ, 4^\circ, 6^\circ, 8^\circ$

Spanwise station	Per-cent chord	Upper surface						Lower surface					
		Angle of attack						Angle of attack					
		-2°	0°	2°	4°	6°	8°	-2°	0°	2°	4°	6°	8°
0.10 b/2	0	0.18	0.44	0.56	0.56	0.46	0.36	-	-	-	-	-	-
	1.5	.33	.16	.07	.34	.75	.05	-.61	-.26	0.04	0.27	0.43	0.58
	4.0	.12	.03	.25	.47	.72	.98	-.61	-.35	-.12	-.08	-.23	.40
	7.0	-.01	-.16	-.33	-.50	-.70	-.90	-	-	-	-	-	-
	10.0	-.07	-.21	-.33	-.50	-.65	-.83	-	-	-	-	-	-
	15.0	-.13	-.25	-.36	-.48	-.61	-.76	-	-	-	-	-	-
	20.0	-.18	-.27	-.37	-.47	-.58	-.71	-	-	-	-	-	-
	30.0	-.19	-.27	-.33	-.43	-.50	-.59	-	-	-	-	-	-
	40.0	-.19	-.25	-.31	-.36	-.43	-.48	-	-	-	-	-	-
	50.0	-.16	-.23	-.27	-.30	-.36	-.40	-	-	-	-	-	-
	60.0	-.15	-.20	-.23	-.27	-.31	-.33	-	-	-	-	-	-
	70.0	-.15	-.18	-.21	-.23	-.26	-.28	-	-	-	-	-	-
	80.0	-.12	-.14	-.16	-.18	-.19	-.19	-	-	-	-	-	-
	90.0	-.02	-.03	-.04	-.05	-.05	-.05	-	-	-	-	-	-
	95.0	.04	.04	.04	.03	.02	.01	-	-	-	-	-	-
0.19 b/2	0	.09	.42	.56	.51	.30	.10	-	-	-	-	-	-
	1.5	.38	.17	.13	.51	.96	.10	-.76	-.31	.03	.30	.50	.57
	4.0	.12	.06	.33	.60	.91	.12	-.69	-.36	-.11	.10	.37	.43
	7.0	-.01	-.17	-.37	.59	.84	.12	-	-	-	-	-	-
	10.0	-.07	-.26	-.41	.60	.81	.00	-.54	-.35	-.18	-.02	.11	.24
	15.0	-.13	-.28	-.43	.59	.78	.08	-.45	-.26	-.18	-.06	.06	.17
	20.0	-.18	-.30	-.42	.53	.68	.73	-.35	-.26	-.17	-.07	.04	.13
	30.0	-.28	-.31	-.40	.49	.56	.66	-.26	-.21	-.13	-.07	.08	.09
	40.0	-.22	-.30	-.37	.43	.50	.57	-.20	-.14	-.10	-.04	.03	.08
	50.0	-.21	-.27	-.32	.35	.40	.44	-	-	-	-	-	-
	60.0	-.19	-.24	-.25	.30	.32	.35	-.08	-.04	0	-.03	.07	.10
	70.0	-.16	-.18	-.21	.24	.26	.26	-	-	-	-	.06	.11
	80.0	-.13	-.14	-.15	.16	.16	.15	-	-	-	-	.06	.11
	90.0	-.03	-.04	-.04	.04	.02	.02	-.03	-.06	-.06	-.07	.07	.08
	95.0	.04	.04	.04	.04	.03	.03	-.07	-.07	-.06	-.07	.07	.08
0.31 b/2	0	.07	.42	.55	.49	.23	.23	-	-	-	-	-	-
	1.5	.41	.18	.13	.54	.93	.10	-.77	-.39	.09	.35	.53	.57
	4.0	.14	.09	.35	.66	.98	.11	-.72	-.37	-.08	.35	.53	.57
	7.0	-.02	-.18	-.41	.66	.93	.12	-	-	-	-	-	-
	10.0	-.06	-.24	-.43	.64	.86	.06	-.54	-.34	-.16	0	.14	.19
	15.0	-.14	-.30	-.45	.62	.80	.04	-.47	-.31	-.17	-.04	.07	.18
	20.0	-.18	-.31	-.44	.58	.73	.04	-.34	-.26	-.15	-.04	.06	.15
	30.0	-.21	-.31	-.41	.51	.57	.68	-.27	-.19	-.12	-.04	.04	.11
	40.0	-.22	-.30	-.38	.42	.50	.57	-.19	-.12	-.07	0	.03	.09
	50.0	-.21	-.27	-.33	.38	.43	.47	-.12	-.07	-.02	0	.03	.11
	60.0	-.19	-.25	-.26	.31	.34	.36	-	-	-	-	-	-
	70.0	-.17	-.20	-.23	.23	.29	.27	-.01	-.01	-.04	-.02	.03	.11
	80.0	-.13	-.15	-.18	.18	.17	.15	-	-	-	-	-	-
	90.0	-.03	-.04	-.04	.03	.02	0	-.06	-.06	-.08	-.06	.06	.08
	95.0	.04	.04	.04	.04	.03	.04	-.09	-.09	-.09	-.09	.08	.08
0.375 b/2	0	.03	.42	.56	.47	.18	.35	-	-	-	-	-	-
	1.5	.80	.15	.20	.63	1.19	1.84	-.78	-.26	-.11	-.37	.28	.37
	4.0	.17	.05	.33	.68	.99	1.41	-.72	-.37	-.08	.16	.34	.39
	7.0	-.01	-.19	-.42	.68	.96	1.27	-	-	-	-	-	-
	10.0	-.06	-.25	-.45	.66	.90	1.10	-.54	-.34	-.15	-.03	.16	.26
	15.0	-.14	-.30	-.46	.63	.82	.96	-.44	-.30	-.16	-.09	.09	.20
	20.0	-.18	-.32	-.45	.59	.74	.86	-.34	-.25	-.13	-.03	.08	.17
	30.0	-.20	-.31	-.41	.51	.54	.66	-.26	-.16	-.12	-.03	.09	.13
	40.0	-.22	-.30	-.37	.42	.51	.57	-.19	-.12	-.08	-.01	.03	.10
	50.0	-.20	-.27	-.33	.36	.41	.46	-	-	-	-	-	-
	60.0	-.18	-.23	-.29	.30	.34	.37	-.06	-.03	-.01	-.04	.06	.11
	70.0	-.17	-.20	-.22	.23	.27	.29	-.01	-.01	-.04	-.01	.04	.11
	80.0	-.13	-.15	-.17	.17	.18	.18	-	-	-	-	-	-
	90.0	-.03	-.04	-.04	.03	.03	.03	-.06	-.07	-.07	-.09	.09	.10
	95.0	.04	.04	.04	.04	.03	.03	-.09	-.09	-.09	-.09	.09	.09
0.44 b/2	0	0	.40	.56	.49	.20	.33	-	-	-	-	-	-
	1.5	.39	.14	.20	.64	1.09	1.81	-.83	-.26	-.12	-.46	.34	.38
	4.0	.18	.06	.34	.68	.93	1.45	-.75	-.39	-.09	.15	.34	.47
	7.0	-.03	-.18	-.42	.68	.97	1.30	-	-	-	-	-	-
	10.0	-.04	-.23	-.45	.66	.91	1.11	-.54	-.34	-.14	-.03	.17	.39
	15.0	-.13	-.28	-.46	.63	.82	.97	-.42	-.30	-.15	-.08	.15	.21
	20.0	-.16	-.30	-.44	.59	.74	.86	-.34	-.25	-.15	-.08	.08	.18
	30.0	-.20	-.31	-.42	.52	.60	.71	-.25	-.17	-.11	-.08	.06	.13
	40.0	-.21	-.29	-.37	.44	.51	.56	-.19	-.13	-.08	-.02	.03	.11
	50.0	-.20	-.27	-.33	.36	.42	.47	-.11	-.06	-.01	-.04	.04	.11
	60.0	-.18	-.24	-.26	.29	.34	.37	-.06	-.03	-.01	-.04	.04	.12
	70.0	-.16	-.20	-.21	.24	.26	.26	0	-.02	-.01	-.03	.04	.14
	80.0	-.12	-.14	-.15	.16	.16	.15	-	-	-	-	-	-
	90.0	-.01	-.03	-.03	.03	.02	.01	-.06	-.07	-.07	-.09	.09	.09
	95.0	.06	.05	.05	.06	.05	.04	-.09	-.09	-.09	-.09	.09	.08

NACA

TABLE XII.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING-
 M_∞ , 0.25; R, 2,000,000 - Continued
(a) c_{u_1} , -2° , 0° , 2° , 4° , 6° , 8° - Concluded

Spanwise station	Per-cent chord	Upper surface						Lower surface					
		Angle of attack						Angle of attack					
		-2°	0°	2°	4°	6°	8°	-2°	0°	2°	4°	6°	8°
0.56 b/2	0	-0.04	0.39	0.55	0.46	0.10	-0.54	-	-	-	-	-	-
	1.5	.43	.20	-.15	-.60	-1.04	-1.79	-0.96	-0.37	0.08	0.37	0.53	0.57
	4.0	.21	-.03	-.31	-.64	-1.02	-1.45	-.77	-.41	-.09	.16	.35	.48
	7.0	.06	-.15	-.40	-.67	-.97	-1.30	-.57	-.35	-.15	.02	.17	.29
	10.0	-.03	-.22	-.43	-.65	-.90	-1.11	-.44	-.30	-.16	-.02	.11	.22
	15.0	-.11	-.26	-.44	-.62	-.81	-.95	-.35	-.26	-.13	-.02	.08	.18
	20.0	-.13	-.26	-.40	-.55	-.70	-.81	-.27	-.16	-.11	-.02	.06	.13
	30.0	-.17	-.27	-.39	-.49	-.56	-.67	-.18	-.11	-.07	0	0.06	.12
	40.0	-.19	-.27	-.35	-.42	-.49	-.55	-.11	-.06	-.01	-.02	.06	.11
	50.0	-.19	-.25	-.32	-.35	-.41	-.47	-.11	-.06	-.01	-.02	.06	.11
	60.0	-.16	-.22	-.25	-.29	-.32	-.35	-.11	-.06	-.01	-.02	.06	.11
	70.0	-.15	-.19	-.20	-.24	-.25	-.26	-.01	.02	.09	.09	.09	.14
	80.0	-.13	-.13	-.15	-.16	-.16	-.15	.04	.06	.08	.10	.12	.13
	90.0	-.03	-.03	-.03	-.03	-.02	-.01	.08	.06	.09	.09	.10	.10
	95.0	.06	.05	.06	.06	.05	.04	.10	.11	.11	.11	.10	.09
0.68 b/2	0	---	---	---	---	---	---	---	---	---	---	---	---
	1.5	.49	.29	-.03	-.46	-.99	-.16	-.11	-.49	-.02	.32	.50	.56
	4.0	.24	0	-.28	-.62	-.01	-.45	-.86	-.47	-.14	.12	.32	.47
	7.0	.10	-.10	-.35	-.62	-.92	-.26	---	---	---	---	---	---
	10.0	.02	-.17	-.39	-.62	-.87	-.11	-.53	-.37	-.17	.01	.16	.29
	15.0	-.05	-.22	-.39	-.58	-.78	-.92	-.46	-.30	-.17	-.03	.10	.21
	20.0	-.10	-.25	-.40	-.56	-.72	-.85	-.37	-.24	-.14	-.03	.08	.17
	30.0	-.15	-.26	-.37	-.49	-.56	-.69	-.26	-.17	-.10	-.02	.06	.13
	40.0	-.16	-.25	-.34	-.43	-.48	-.56	-.18	-.12	-.06	0	0.06	.11
	50.0	-.16	-.23	-.30	-.38	-.40	-.45	---	---	---	---	---	---
	60.0	-.14	-.20	-.23	-.27	-.30	-.34	-.05	-.02	.02	.04	.07	.11
	70.0	-.13	-.16	-.19	-.22	-.24	-.29	-.01	.01	.04	.03	.06	.11
	80.0	-.09	-.11	-.14	-.15	-.15	-.14	.04	.05	.07	.08	.09	.11
	90.0	0	-.02	-.02	-.02	-.01	0	.07	.07	.08	.09	.09	.09
	95.0	.05	.04	.04	.05	.06	.04	.09	.09	.09	.09	.09	.08
0.80 b/2	0	-.18	.35	.57	.52	.19	-.44	---	---	---	---	---	---
	1.5	.50	.31	0	-.45	-.94	-.15	-.13	.64	-.12	.23	.47	.57
	4.0	.30	.09	-.18	-.50	-.87	-.29	-.100	-.56	-.22	.06	.37	.43
	7.0	.16	-.04	-.27	-.53	-.82	-.15	---	---	---	---	---	---
	10.0	.07	-.11	-.31	-.54	-.78	-.101	---	-.62	-.43	-.22	-.03	.13
	15.0	-.02	-.17	-.34	-.52	-.72	-.86	-.50	-.36	-.20	-.05	.07	.18
	20.0	-.07	-.20	-.34	-.50	-.65	-.76	-.39	-.28	-.16	-.04	.06	.15
	30.0	-.10	-.21	-.32	-.43	-.52	-.61	-.28	-.19	-.12	-.04	.04	.11
	40.0	-.13	-.21	-.30	-.43	-.51	---	---	---	---	---	---	---
	50.0	-.14	-.20	-.27	-.38	-.43	-.44	-.13	-.08	-.03	0	.05	.09
	60.0	-.13	-.18	-.23	-.25	-.30	-.34	-.08	-.03	.01	.03	.07	.10
	70.0	-.11	-.16	-.19	-.20	-.24	-.25	-.01	.02	.04	.08	.08	.10
	80.0	-.09	-.12	-.12	-.14	-.15	-.14	.03	.05	.05	.08	.09	.10
	90.0	-.04	-.01	-.02	-.02	-.02	-.01	.07	.08	.08	.09	.10	.09
	95.0	.05	.05	.05	.05	.04	.09	.09	.10	.11	.11	.09	.09
0.94 b/2	0	-.79	-.04	.41	.56	.45	-.04	---	---	---	---	---	---
	1.5	.52	.38	.13	-.21	-.63	-.19	-.158	-.94	-.36	.08	.38	.53
	4.0	.36	.18	-.06	-.34	-.67	-.103	---	---	---	---	---	---
	7.0	.22	.04	-.17	-.40	-.66	-.95	---	-.74	-.49	-.28	-.05	.12
	10.0	-.13	-.03	-.21	-.40	-.61	-.85	---	-.64	-.45	-.27	-.10	.07
	15.0	-.04	-.09	-.24	-.39	-.55	-.73	-.52	-.36	-.23	-.10	.01	.13
	20.0	-.01	-.13	-.26	-.39	-.52	-.99	-.40	-.28	-.20	-.09	.01	.09
	30.0	-.07	-.16	-.26	-.34	-.44	-.47	-.27	-.20	-.13	-.07	0	.06
	40.0	-.10	-.16	-.23	-.30	-.35	-.41	-.17	-.13	-.07	-.04	0	.04
	50.0	-.12	-.17	-.22	-.27	-.29	-.34	-.10	-.07	-.03	-.02	.03	.03
	60.0	-.11	-.15	-.19	-.22	-.24	-.26	---	---	---	---	---	---
	70.0	-.10	-.13	-.16	-.16	-.18	-.20	-.02	.02	.04	.05	.07	.07
	80.0	-.06	-.10	-.10	-.10	-.13	-.11	.06	.06	.07	.07	.08	.08
	90.0	-.03	.02	.01	0	.01	-.01	.07	.09	.09	.08	.09	.08
	95.0	.07	.07	.06	.06	.06	.06	.11	.11	.11	.10	.10	.09

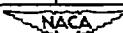


TABLE XIII.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING,
 $M_\infty = 0.25$; $R = 2,000,000$ - Continued
 (b) α_u , $10^\circ, 12^\circ, 14^\circ, 16^\circ, 18^\circ, 20^\circ$

Spanwise station	Percent chord	Upper surface						Lower surface					
		Angle of attack						Angle of attack					
		10°	12°	14°	16°	18°	20°	10°	12°	14°	16°	18°	20°
0.10 b/2	0	-0.12	-0.57	-1.13	-1.79	-2.49	-3.30	-	-	-	-	-	-
	1.5	-1.49	-1.96	-2.49	-3.09	-3.75	-4.53	0.64	0.67	0.64	0.58	0.48	0.35
	4.0	-1.29	-1.58	-1.85	-2.19	-2.56	-2.88	.52	.61	.68	.72	.75	.76
	7.0	-1.16	-1.31	-1.56	-1.80	-2.04	-2.27	-	-	-	-	-	-
	10.0	-0.99	-1.18	-1.35	-1.53	-1.70	-1.88	.32	.42	.50	.58	.64	.69
	15.0	-0.91	-1.04	-1.17	-1.30	-1.41	-1.54	.24	.33	.41	.48	.53	.58
	20.0	-0.83	-0.92	-1.02	-1.11	-1.20	-1.29	.21	.29	.37	.43	.48	.53
	30.0	-0.67	-0.73	-0.80	-0.86	-0.92	-0.98	.16	.23	.29	.35	.39	.43
	40.0	-0.54	-0.59	-0.63	-0.68	-0.72	-0.76	.14	.20	.25	.31	.34	.38
	50.0	-0.45	-0.48	-0.51	-0.53	-0.57	-0.61	.13	.18	.23	.27	.30	.34
	60.0	-0.37	-0.39	-0.41	-0.43	-0.46	-0.51	.13	.17	.22	.26	.28	.33
	70.0	-0.30	-0.31	-0.32	-0.33	-0.37	-0.39	.14	.17	.21	.24	.26	.29
	80.0	-0.21	-0.21	-0.22	-0.23	-0.26	-0.29	-	-	-	-	-	-
	90.0	-0.06	-0.07	-0.09	-0.10	-0.13	-0.15	.10	.12	.14	.16	.17	.18
	95.0	0	-0.03	-0.05	-0.05	-0.05	-0.09	.07	.08	.09	.11	.11	.11
0.19 b/2	0	-0.67	-1.39	-2.29	-3.34	-4.46	-5.73	-	-	-	-	-	-
	1.5	-2.11	-2.76	-3.48	-4.26	-5.15	-6.05	.57	.59	.57	.58	.60	.61
	4.0	-1.65	-2.08	-2.49	-2.96	-3.39	-3.83	.52	.58	.61	.60	.56	.49
	7.0	-1.30	-1.59	-1.90	-2.20	-2.50	-2.81	-	-	-	-	-	-
	10.0	-1.22	-1.45	-1.67	-1.91	-2.14	-2.37	.34	.44	.50	.57	.61	.64
	15.0	-1.08	-1.24	-1.40	-1.57	-1.72	-1.88	.26	.35	.43	.50	.55	.60
	20.0	-0.89	-1.02	-1.14	-1.27	-1.39	-1.52	.21	.29	.37	.44	.49	.54
	30.0	-0.76	-0.83	-0.91	-0.99	-1.05	-1.13	.16	.23	.29	.35	.41	.45
	40.0	-0.63	-0.68	-0.72	-0.76	-0.81	-0.87	.15	.20	.25	.31	.35	.39
	50.0	-0.49	-0.51	-0.54	-0.56	-0.60	-0.66	-	-	-	-	-	-
	60.0	-0.38	-0.38	-0.39	-0.41	-0.45	-0.53	.13	.17	.21	.24	.27	.30
	70.0	-0.27	-0.27	-0.29	-0.27	-0.34	-0.42	.13	.16	.19	.23	.24	.27
	80.0	-0.15	-0.13	-0.14	-0.19	-0.27	-0.34	-	-	-	-	-	-
	90.0	-0.03	-0.03	-0.04	-0.10	-0.16	-0.24	.09	.09	.10	.12	.12	.14
	95.0	0	-0.03	-0.09	-0.16	-0.22	-0.25	.03	.04	.04	.05	.05	.06
0.31 b/2	0	-0.91	-1.73	-2.78	-3.97	-5.11	-6.38	-	-	-	-	-	-
	1.5	-2.29	-2.99	-3.80	-4.80	-5.84	-6.70	.53	.61	.68	.77	.87	.92
	4.0	-1.87	-2.08	-2.38	-3.12	-3.55	-3.94	.55	.58	.53	.47	.39	-
	7.0	-1.46	-1.79	-2.12	-2.44	-2.72	-2.94	-	-	-	-	-	-
	10.0	-1.31	-1.55	-1.79	-2.04	-2.24	-2.38	.36	.42	.51	.60	.63	.68
	15.0	-1.14	-1.31	-1.48	-1.64	-1.77	-1.82	.28	.36	.43	.50	.54	.58
	20.0	-0.99	-1.11	-1.24	-1.35	-1.44	-1.46	.23	.31	.38	.43	.49	.53
	30.0	-0.77	-0.85	-0.91	-0.97	-1.00	-1.09	.17	.24	.30	.36	.40	.44
	40.0	-0.63	-0.67	-0.70	-0.69	-0.73	-0.93	.16	.20	.25	.30	.33	.37
	50.0	-0.51	-0.51	-0.49	-0.46	-0.55	-0.81	.14	.18	.23	.27	.32	-
	60.0	-0.38	-0.35	-0.32	-0.32	-0.45	-0.64	-	-	-	-	-	-
	70.0	-0.25	-0.28	-0.19	-0.24	-0.38	-0.47	.13	.16	.18	.20	.21	.22
	80.0	-0.11	-0.09	-0.13	-0.19	-0.31	-0.35	.08	.08	.09	.09	.06	.04
	90.0	-0.01	-0.04	-0.10	-0.11	-0.21	-0.25	.07	.09	.04	.04	.01	.04
	95.0	0	-0.04	-0.04	-0.15	-0.26	-0.30	-	-	-	-	-	-
0.375 b/2	0	-1.08	-2.00	-3.12	-4.38	-5.38	-6.45	-	-	-	-	-	-
	1.5	-2.51	-3.23	-4.12	-5.10	-5.84	-6.44	.52	.59	.67	.73	.81	.86
	4.0	-1.96	-2.04	-2.38	-3.06	-3.34	-3.92	.55	.58	.53	.51	.45	-
	7.0	-1.53	-1.84	-2.16	-2.45	-2.61	-2.61	-	-	-	-	-	-
	10.0	-1.36	-1.60	-1.84	-2.06	-2.16	-2.07	.39	.46	.58	.57	.62	.64
	15.0	-1.16	-1.33	-1.49	-1.63	-1.69	-1.41	.30	.38	.45	.51	.56	.60
	20.0	-1.02	-1.13	-1.25	-1.34	-1.34	-1.12	.23	.32	.39	.46	.50	.54
	30.0	-0.76	-0.84	-0.90	-0.93	-0.98	-0.98	.19	.25	.32	.37	.41	.44
	40.0	-0.63	-0.68	-0.71	-0.72	-0.91	-1.12	.15	.22	.28	.31	.33	.36
	50.0	-0.51	-0.51	-0.56	-0.61	-1.02	-1.36	-	-	-	-	-	-
	60.0	-0.39	-0.41	-0.44	-0.53	-1.01	-1.12	.15	.17	.21	.24	.28	.33
	70.0	-0.30	-0.32	-0.36	-0.46	-0.76	-0.82	.15	.17	.21	.22	.28	.30
	80.0	-0.20	-0.22	-0.28	-0.31	-0.41	-0.67	-	-	-	-	-	-
	90.0	-0.06	-0.10	-0.15	-0.14	-0.26	-0.49	.11	.12	.14	.15	.15	0
	95.0	0	-0.03	-0.04	-0.01	-0.17	-0.39	.09	.10	.12	.13	.05	-.07
0.44 b/2	0	-1.07	-1.99	-3.12	-4.39	-5.09	-6.81	-	-	-	-	-	-
	1.5	-2.48	-3.24	-4.09	-5.05	-5.48	-6.21	.51	.58	.68	.72	.84	.89
	4.0	-1.99	-2.21	-2.71	-3.18	-3.48	-4.20	.55	.58	.57	.53	.48	.55
	7.0	-1.65	-1.90	-2.23	-2.59	-2.91	-3.24	-	-	-	-	-	-
	10.0	-1.45	-1.64	-1.89	-2.20	-2.51	-2.53	.39	.47	.53	.58	.61	.64
	15.0	-1.17	-1.33	-1.53	-1.67	-1.90	-1.87	.30	.38	.47	.52	.53	.56
	20.0	-1.03	-1.15	-1.58	-1.37	-1.50	-1.27	.23	.33	.42	.46	.47	.50
	30.0	-0.81	-0.93	-0.96	-0.99	-1.39	-1.19	.20	.26	.32	.37	.38	.40
	40.0	-0.64	-0.69	-0.73	-0.73	-1.28	-1.11	.16	.21	.27	.31	.30	.31
	50.0	-0.51	-0.54	-0.55	-0.56	-1.03	-1.00	.16	.20	.24	.26	.26	.26
	60.0	-0.39	-0.39	-0.40	-0.45	-0.97	-0.95	.15	.18	.22	.23	.21	.20
	70.0	-0.26	-0.24	-0.26	-0.36	-0.83	-0.90	.15	.18	.20	.23	.19	.16
	80.0	-0.13	-0.13	-0.19	-0.31	-0.68	-0.80	-	-	-	-	-	-
	90.0	-0.03	-0.06	-0.14	-0.26	-0.51	-0.64	.09	.09	.10	.11	.01	-.08
	95.0	0	-0.06	-0.14	-0.22	-0.42	-0.56	.06	.05	.05	.04	-.09	-.19

TABLE XII.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING.
 $M_\infty = 0.25$; $R = 2,000,000$ - Concluded
 (b) $\alpha_u = 10^\circ, 12^\circ, 14^\circ, 16^\circ, 18^\circ, 20^\circ$ - Concluded

Spanwise station	Per-cent chord	Upper surface						Lower surface						
		Angle of attack						Angle of attack						
		10°	12°	14°	16°	18°	20°	10°	12°	14°	16°	18°	20°	
0.56 b/2	0	-1.36	-2.41	-3.70	-5.11	-1.23	-1.12	-	0.49	0.32	0.05	-0.30	-0.32	-0.29
	1.5	-2.51	-3.27	-4.18	-5.79	-1.02	-0.88	-	.56	.58	.57	.51	.58	.57
	4.0	-1.84	-2.31	-2.79	-3.27	-1.03	-0.88	-	-	-	-	-	-	-
	7.0	-1.56	-1.91	-2.27	-2.59	-1.05	-0.90	-	.40	.47	.53	.58	.53	.55
	10.0	-1.38	-1.64	-1.91	-2.14	-1.05	-0.90	-	.31	.39	.46	.51	.46	.47
	15.0	-1.16	-1.34	-1.52	-1.63	-1.03	-0.91	-	.26	.35	.40	.46	.40	.42
	20.0	-0.97	-1.11	-1.25	-1.35	-1.02	-0.89	-	.20	.26	.32	.36	.31	.33
	30.0	-0.77	-0.86	-0.93	-0.99	-0.93	-0.83	-	.16	.22	.27	.32	.25	.26
	40.0	-0.63	-0.68	-0.72	-0.79	-0.86	-0.77	-	.14	.16	.18	.21	.06	.05
	50.0	-0.51	-0.54	-0.56	-0.66	-0.77	-0.69	-	.10	.11	.12	.16	-0.06	-0.08
	60.0	-0.39	-0.40	-0.44	-0.55	-0.69	-0.63	-	.08	.08	.08	.08	-0.14	-0.16
	70.0	-0.27	-0.29	-0.33	-0.44	-0.61	-0.55	-	-	-	-	-	-	-
	80.0	-0.15	-0.17	-0.24	-0.34	-0.49	-0.48	-	-	-	-	-	-	-
	90.0	-0.03	-0.08	-0.14	-0.18	-0.42	-0.43	-	-	-	-	-	-	-
	95.0	-0.01	-0.05	-0.09	-0.09	-0.39	-0.41	-	-	-	-	-	-	-
0.68 b/2	0	-	-	-	-	-	-	-	-	-	-	-	-	-
	1.5	-2.36	-3.16	-4.24	-4.95	-0.87	-0.88	-	.52	.36	.13	-0.20	.46	.35
	4.0	-1.99	-2.29	-2.80	-3.26	-0.85	-0.89	-	.55	.58	.57	.52	.56	.56
	7.0	-1.48	-1.86	-2.22	-2.51	-0.81	-0.85	-	-	-	-	-	-	-
	10.0	-1.35	-1.61	-1.87	-2.14	-0.81	-0.82	-	.38	.47	.53	.57	.46	.48
	15.0	-1.14	-1.33	-1.51	-1.64	-0.75	-0.78	-	.30	.38	.45	.50	.42	.45
	20.0	-1.01	-1.15	-1.29	-1.36	-0.72	-0.73	-	.23	.33	.39	.47	.36	.40
	30.0	-0.80	-0.88	-0.94	-0.92	-0.62	-0.64	-	.20	.26	.31	.37	.29	.32
	40.0	-0.62	-0.66	-0.67	-0.63	-0.53	-0.59	-	.16	.21	.23	.30	.23	.26
	50.0	-0.48	-0.48	-0.44	-0.44	-0.49	-0.52	-	-	-	-	-	-	-
	60.0	-0.34	-0.31	-0.27	-0.38	-0.46	-0.48	-	.14	.16	.20	.23	.15	.16
	70.0	-0.22	-0.17	-0.16	-0.37	-0.41	-0.42	-	.13	.15	.16	.19	.11	.11
	80.0	-0.10	-0.07	-0.13	-0.32	-0.39	-0.39	-	.09	.13	.13	.15	.06	.07
	90.0	0	-0.02	-0.12	-0.24	-0.32	-0.32	-	.06	.08	.07	.07	-0.03	-0.03
	95.0	.02	-0.03	-0.15	-0.26	-0.30	-0.31	-	.05	.04	.01	.01	-0.10	-0.10
0.80 b/2	0	-1.30	-2.42	-3.76	-5.31	-2.88	-1.92	-	-	-	-	-	-	-
	1.5	-2.27	-3.03	-4.19	-4.72	-2.41	-1.50	-	.56	.43	.24	-.04	.25	.27
	4.0	-1.78	-2.05	-2.53	-3.00	-2.11	-1.54	-	.52	.57	.54	.55	.55	.55
	7.0	-1.40	-1.73	-2.06	-2.36	-1.79	-1.41	-	-	-	-	-	-	-
	10.0	-1.26	-1.51	-1.73	-1.99	-1.71	-1.42	-	.35	.45	.51	.56	.53	.53
	15.0	-1.07	-1.25	-1.42	-1.57	-1.41	-1.24	-	.28	.36	.43	.45	.42	.47
	20.0	-0.92	-1.06	-1.17	-1.28	-1.28	-1.22	-	.23	.31	.37	.44	.40	.42
	30.0	-0.71	-0.79	-0.86	-0.92	-0.99	-1.04	-	.18	.24	.29	.33	.31	.33
	40.0	-0.58	-0.62	-0.66	-0.72	-0.81	-0.94	-	-	-	-	-	-	-
	50.0	-0.47	-0.48	-0.49	-0.57	-0.64	-0.73	-	.13	.17	.21	.23	.22	.23
	60.0	-0.35	-0.34	-0.34	-0.49	-0.52	-0.61	-	.13	.16	.18	.22	.19	.19
	70.0	-0.24	-0.21	-0.24	-0.41	-0.42	-0.48	-	.13	.15	.17	.19	.16	.16
	80.0	-0.11	-0.11	-0.18	-0.33	-0.31	-0.37	-	.12	.11	.13	.14	.12	.11
	90.0	-0.02	-0.05	-0.15	-0.27	-0.22	-0.26	-	.08	.07	.07	.08	.07	.04
	95.0	0	-0.05	-0.15	-0.22	-0.17	-0.23	-	.06	.05	.03	.04	.03	-.01
0.94 b/2	0	-1.11	-1.52	-2.61	-2.58	-1.03	-1.05	-	-	-	-	-	-	-
	1.5	-1.84	-2.89	-3.85	-2.22	-0.99	-0.93	-	.57	.51	.37	.32	.50	.47
	4.0	-1.34	-1.76	-2.15	-2.21	-1.03	-0.95	-	-	-	-	-	-	-
	7.0	-1.21	-1.50	-1.76	-2.11	-0.96	-0.90	-	.36	.47	.53	.58	.53	.55
	10.0	-1.05	-1.26	-1.46	-2.15	-0.97	-0.91	-	.29	.38	.45	.50	.46	.48
	15.0	-0.87	-1.02	-1.16	-1.82	-0.92	-0.86	-	.22	.29	.36	.42	.38	.40
	20.0	-0.73	-0.87	-0.97	-1.47	-0.92	-0.86	-	.17	.23	.29	.35	.31	.33
	30.0	-0.56	-0.63	-0.69	-1.07	-0.83	-0.80	-	.12	.16	.21	.23	.23	.24
	40.0	-0.46	-0.50	-0.53	-0.73	-0.82	-0.81	-	.08	.12	.15	.18	.16	.17
	50.0	-0.37	-0.37	-0.37	-0.58	-0.74	-0.78	-	.08	.10	.13	.15	.12	.13
	60.0	-0.28	-0.27	-0.26	-0.42	-0.71	-0.73	-	-	-	-	-	-	-
	70.0	-0.19	-0.17	-0.16	-0.32	-0.62	-0.67	-	.08	.07	.08	.09	.06	.05
	80.0	-0.10	-0.09	-0.12	-0.24	-0.52	-0.59	-	.06	.06	.05	.03	0	-.01
	90.0	.01	-0.01	-0.09	-0.18	-0.46	-0.50	-	.07	.04	.02	0	-.06	-.10
	95.0	.04	0	-0.10	-0.16	-0.43	-0.46	-	.07	.03	-.02	-.04	-.17	-.20

NACA

TABLE XIII.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING.
 $M_\infty = 0.60$; $R = 2,000,000$
(a) α_u , $-4^\circ, -2^\circ, 0^\circ, 2^\circ, 4^\circ, 6^\circ$

Spanwise station	Percent chord	Upper surface						Lower surface					
		Angle of attack						Angle of attack					
		-4°	-2°	0°	2°	4°	6°	-4°	-2°	0°	2°	4°	6°
0.10 b/2	0	-0.06	0.24	0.45	0.57	0.59	0.58	----	----	----	----	----	----
	1.5	.45	.36	.18	-.01	-.28	-.58	-.94	-.64	-.38	-.15	.05	.14
	4.0	.26	.13	-.04	-.23	-.44	-.69	----	----	----	----	----	----
	7.0	.12	0	-.16	-.32	-.52	-.71	----	----	----	----	----	----
	10.0	.04	-.08	-.22	-.35	-.52	-.68	----	----	----	----	----	----
	15.0	-.04	-.14	-.26	-.39	-.58	-.63	----	----	----	----	----	----
	20.0	-.10	-.19	-.29	-.38	-.58	-.63	----	----	----	----	----	----
	30.0	-.14	-.21	-.30	-.38	-.58	-.63	----	----	----	----	----	----
	40.0	-.14	-.21	-.28	-.35	-.42	-.48	----	----	----	----	----	----
	50.0	-.13	-.19	-.26	-.31	-.35	-.40	----	----	----	----	----	----
	60.0	-.13	-.18	-.26	-.26	-.31	-.34	----	----	----	----	----	----
	70.0	-.13	-.17	-.21	-.24	-.27	-.29	----	----	----	----	----	----
0.19 b/2	0	-.10	-.14	-.17	-.19	-.20	-.20	----	----	----	----	----	----
	1.5	.26	.12	.43	.56	.55	.40	----	----	----	----	----	----
	4.0	.28	.39	.18	.08	-.46	-.90	----	----	----	----	----	----
	7.0	.16	.01	-.09	-.31	-.61	-.93	----	----	----	----	----	----
	10.0	.06	-.08	-.23	-.44	-.65	-.87	----	----	----	----	----	----
	15.0	-.03	-.16	-.31	-.45	-.64	-.81	----	----	----	----	----	----
	20.0	-.08	-.20	-.33	-.46	-.60	-.75	----	----	----	----	----	----
	30.0	-.15	-.24	-.34	-.44	-.55	-.63	----	----	----	----	----	----
	40.0	-.18	-.25	-.34	-.41	-.55	-.65	----	----	----	----	----	----
	50.0	-.16	-.24	-.30	-.36	-.44	-.51	----	----	----	----	----	----
	60.0	-.16	-.20	-.27	-.33	-.36	----	----	----	----	----	----	----
	70.0	-.15	-.18	-.21	-.24	-.27	-.28	----	----	----	----	----	----
0.31 b/2	0	-.12	-.12	.44	.56	.53	.34	----	----	----	----	----	----
	1.5	.53	.41	.20	-.08	-.49	-.10	----	----	----	----	----	----
	4.0	.31	.35	-.09	-.34	-.70	-.109	----	----	----	----	----	----
	7.0	.17	.01	-.28	-.43	-.72	-.103	----	----	----	----	----	----
	10.0	.07	-.07	-.27	-.45	-.70	-.06	----	----	----	----	----	----
	15.0	-.03	-.18	-.33	-.50	-.70	-.09	----	----	----	----	----	----
	20.0	-.08	-.20	-.35	-.49	-.65	-.08	----	----	----	----	----	----
	30.0	-.14	-.24	-.35	-.45	-.65	-.05	----	----	----	----	----	----
	40.0	-.16	-.24	-.34	-.42	-.69	-.05	----	----	----	----	----	----
	50.0	-.17	-.23	-.31	-.37	-.41	-.05	----	----	----	----	----	----
	60.0	-.15	-.20	-.28	-.29	-.34	-.05	----	----	----	----	----	----
	70.0	-.14	-.16	-.23	-.24	-.28	-.04	----	----	----	----	----	----
0.375 b/2	0	-.12	-.14	-.17	-.18	-.19	-.16	----	----	----	----	----	----
	1.5	.42	.08	.43	.57	.52	.31	----	----	----	----	----	----
	4.0	.36	.20	-.03	-.31	-.67	-.107	----	----	----	----	----	----
	7.0	.19	.02	-.21	-.45	-.74	-.108	----	----	----	----	----	----
	10.0	.10	-.05	-.25	-.49	-.74	-.108	----	----	----	----	----	----
	15.0	0	-.13	-.32	-.49	-.70	-.092	----	----	----	----	----	----
	20.0	-.07	-.19	-.34	-.49	-.66	-.084	----	----	----	----	----	----
	30.0	-.12	-.21	-.33	-.44	-.68	-.063	----	----	----	----	----	----
	40.0	-.15	-.24	-.33	-.42	-.68	-.056	----	----	----	----	----	----
	50.0	-.15	-.22	-.30	-.36	-.41	-.056	----	----	----	----	----	----
	60.0	-.15	-.19	-.26	-.28	-.34	-.056	----	----	----	----	----	----
	70.0	-.14	-.16	-.21	-.24	-.27	-.04	----	----	----	----	----	----
0.44 b/2	0	-.02	-.02	-.03	-.03	-.02	-.08	----	----	----	----	----	----
	1.5	.53	.41	.07	.42	.56	.52	.30	----	----	----	----	----
	4.0	.35	.19	-.04	-.34	-.69	-.114	----	----	----	----	----	----
	7.0	.19	.04	-.20	-.45	-.75	-.110	----	----	----	----	----	----
	10.0	.10	-.04	-.26	-.50	-.73	-.103	----	----	----	----	----	----
	15.0	0	-.13	-.32	-.50	-.70	-.094	----	----	----	----	----	----
	20.0	-.05	-.19	-.33	-.49	-.66	-.085	----	----	----	----	----	----
	30.0	-.12	-.22	-.34	-.47	-.59	-.066	----	----	----	----	----	----
	40.0	-.14	-.22	-.32	-.42	-.49	-.056	----	----	----	----	----	----
	50.0	-.14	-.21	-.30	-.38	-.40	-.047	----	----	----	----	----	----
	60.0	-.14	-.20	-.28	-.29	-.34	-.038	----	----	----	----	----	----
	70.0	-.13	-.16	-.22	-.25	-.26	-.028	----	----	----	----	----	----
	80.0	-.10	-.12	-.15	-.17	-.17	-.016	----	----	----	----	----	----
	90.0	-.01	-.01	-.08	-.03	-.02	-.004	----	----	----	----	----	----
	95.0	.06	.06	-.05	-.06	-.05	-.005	----	----	----	----	----	----

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TABLE XIII.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING.
 $M_\infty = 0.60$; $R = 2,000,000$ - Continued
(a) $\alpha_u = -4^\circ, -2^\circ, 0^\circ, 2^\circ, 4^\circ, 6^\circ$ - Concluded

Spanwise station	Percent chord	Upper surface						Lower surface						
		Angle of attack						Angle of attack						
		-4°	-2°	0°	2°	4°	6°	-4°	-2°	0°	2°	4°	6°	
0.56 b/2	0	-0.50	0.07	0.41	0.56	0.50	0.21	---	-1.78	-1.07	-0.39	0.06	0.36	0.52
	1.5	.54	.15	.21	.11	.58	-1.18	-1.69	-1.88	-1.45	-1.13	.15	.33	---
	4.0	.36	.22	-.02	-.31	-.68	-1.11	---	---	---	---	---	---	---
	7.0	.22	.07	-.16	-.43	-.74	-1.08	-.85	-.66	-.39	-.20	0	.15	---
	10.0	.13	-.02	-.24	-.47	-.78	-1.04	-.69	-.49	-.35	-.20	-.05	.09	---
	15.0	.01	-.10	-.29	-.49	-.70	-.95	-.55	-.39	-.28	-.16	-.04	.07	---
	20.0	-.01	-.14	-.29	-.46	-.63	-.84	-.38	-.29	-.18	-.13	-.04	.05	---
	30.0	-.09	-.19	-.31	-.44	-.57	-.64	-.28	-.19	-.12	-.08	-.01	.03	---
	40.0	-.10	-.20	-.30	-.40	-.46	-.54	-.16	-.11	-.07	-.02	.01	.05	---
	50.0	-.14	-.20	-.26	-.35	-.40	-.46	---	---	---	---	---	---	---
	60.0	-.11	-.19	-.24	-.29	-.33	-.35	---	---	---	---	---	---	---
	70.0	-.11	-.17	-.20	-.23	-.24	-.27	-.02	.01	.02	.03	.08	.09	---
0.68 b/2	80.0	-.09	-.12	-.14	-.17	-.17	-.15	.04	.06	.06	.08	.09	.09	1.0
	90.0	-.01	-.01	-.03	-.03	-.02	-.01	.06	.09	.07	.08	.09	.08	---
	95.0	.06	.06	.06	.06	.06	.04	.09	.11	.11	.11	.10	.08	---
0.80 b/2	0	.03	.03	.02	.01	.01	.01	---	---	---	---	---	---	---
	1.5	.57	.50	.30	0	-.44	-1.01	-1.91	-1.23	-.52	-.04	.30	.48	---
	4.0	.40	.25	0	-.29	-.68	-1.14	-1.93	-.98	-.53	-.17	.10	.30	---
	7.0	.27	.10	-.12	-.38	-.69	-1.05	---	---	---	---	---	---	---
	10.0	.16	.01	-.20	-.42	-.69	-.99	-.90	-.59	-.43	-.21	-.01	.14	---
	15.0	.07	-.06	-.25	-.44	-.65	-.90	-.73	-.52	-.35	-.20	-.05	.07	---
	20.0	.01	-.13	-.29	-.45	-.64	-.84	-.58	-.42	-.26	-.16	-.05	.05	---
	30.0	-.07	-.18	-.30	-.42	-.57	-.64	-.41	-.29	-.20	-.13	-.04	.03	---
	40.0	-.11	-.19	-.29	-.39	-.49	-.55	-.28	-.20	-.14	-.08	-.01	.04	---
	50.0	-.12	-.19	-.27	-.34	-.40	-.45	---	---	---	---	---	---	---
	60.0	-.10	-.17	-.23	-.25	-.30	-.34	-.13	-.06	-.03	.01	.03	.06	---
	70.0	-.10	-.15	-.19	-.21	-.24	-.25	-.07	-.01	-.01	.05	.06	.08	---
0.94 b/2	80.0	-.10	-.11	-.14	-.15	-.17	-.17	-.01	.04	.06	.07	.08	.10	1.0
	90.0	-.05	-.02	-.02	-.02	-.03	-.02	.01	.08	.08	.09	.10	.09	---
	95.0	0	.05	.05	.06	.06	.05	.03	.10	.11	.11	.11	.10	---

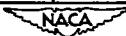

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TABLE XIII.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING.

 $M_\infty = 0.60; R = 2,000,000$ - Continued(b) α_u , $8^\circ, 10^\circ, 12^\circ, 14^\circ, 16^\circ, 18^\circ$

Spanwise station	Per-cent chord	Upper surface						Lower surface						
		Angle of attack						Angle of attack						
		8°	10°	12°	14°	16°	18°	8°	10°	12°	14°	16°	18°	
0.10 b/2	0	0.39	0.18	-0.07	-0.30	-0.52	-1.00	---	0.57	0.66	0.71	0.73	0.76	0.77
	1.5	-0.96	-1.43	-2.06	-2.54	-2.78	-2.78	---	0.57	0.50	0.59	0.68	0.75	0.81
	4.0	-0.99	-1.32	-1.72	-2.34	-2.64	-2.74	---	0.58	0.50	0.59	0.68	0.75	0.81
	7.0	-0.95	-1.23	-1.56	-1.84	-2.49	-2.41	---	0.58	0.51	0.59	0.68	0.75	0.81
	10.0	-0.88	-1.12	-1.24	-1.38	-1.74	-2.16	---	0.58	0.51	0.59	0.68	0.75	0.81
	15.0	-0.83	-0.96	-1.14	-1.23	-1.37	-1.09	---	0.58	0.51	0.59	0.68	0.75	0.81
	20.0	-0.77	-0.90	-1.04	-1.11	-1.19	-1.54	---	0.58	0.51	0.59	0.68	0.75	0.81
	30.0	-0.67	-0.75	-0.84	-0.89	-0.97	-1.16	---	0.58	0.51	0.59	0.68	0.75	0.81
	40.0	-0.56	-0.62	-0.70	-0.73	-0.88	-0.92	---	0.58	0.51	0.59	0.68	0.75	0.81
	50.0	-0.47	-0.52	-0.57	-0.61	-0.70	-0.81	---	0.58	0.51	0.59	0.68	0.75	0.81
	60.0	-0.39	-0.43	-0.48	-0.52	-0.60	-0.70	---	0.58	0.51	0.59	0.68	0.75	0.81
	70.0	-0.32	-0.34	-0.38	-0.43	-0.51	-0.60	---	0.58	0.51	0.59	0.68	0.75	0.81
	80.0	-0.23	-0.24	-0.25	-0.31	-0.38	-0.48	---	0.58	0.51	0.59	0.68	0.75	0.81
	90.0	-0.05	-0.07	-0.10	-0.15	-0.22	-0.30	---	0.58	0.51	0.59	0.68	0.75	0.81
	95.0	0	-0.02	-0.03	-0.11	-0.18	-0.24	---	0.58	0.51	0.59	0.68	0.75	0.81
0.19 b/2	0	-0.12	-0.22	-0.56	-0.81	-1.00	-1.17	---	0.56	0.60	0.60	0.66	0.76	0.82
	1.5	-1.49	-2.13	-2.48	-2.24	-1.87	-1.62	---	0.56	0.51	0.58	0.62	0.72	0.82
	4.0	-1.34	-1.90	-2.40	-2.20	-1.81	-1.59	---	0.56	0.51	0.58	0.62	0.72	0.82
	7.0	-1.18	-1.68	-2.42	-2.08	-1.75	-1.64	---	0.56	0.51	0.58	0.62	0.72	0.82
	10.0	-1.14	-1.31	-1.69	-1.92	-1.73	-1.63	---	0.56	0.51	0.58	0.62	0.72	0.82
	15.0	-1.04	-1.18	-1.30	-1.73	-1.64	-1.55	---	0.56	0.51	0.58	0.62	0.72	0.82
	20.0	-0.88	-1.04	-1.13	-1.56	-1.59	-1.54	---	0.56	0.51	0.58	0.62	0.72	0.82
	30.0	-0.75	-0.84	-0.94	-1.28	-1.44	-1.42	---	0.56	0.51	0.58	0.62	0.72	0.82
	40.0	-0.64	-0.69	-0.74	-1.00	-1.28	-1.33	---	0.56	0.51	0.58	0.62	0.72	0.82
	50.0	-0.50	-0.53	-0.57	-0.79	-1.11	-1.19	---	0.56	0.51	0.58	0.62	0.72	0.82
	60.0	-0.38	-0.41	-0.43	-0.58	-0.93	-1.07	---	0.56	0.51	0.58	0.62	0.72	0.82
	70.0	-0.29	-0.26	-0.29	-0.43	-0.77	-0.94	---	0.56	0.51	0.58	0.62	0.72	0.82
0.31 b/2	0	-0.15	-0.15	-0.16	-0.26	-0.58	-0.79	---	0.56	0.51	0.58	0.62	0.72	0.82
	1.5	-0.01	-0.06	-0.09	-0.16	-0.44	-0.67	---	0.56	0.51	0.58	0.62	0.72	0.82
	4.0	-0.01	-0.04	-0.08	-0.12	-0.35	-0.57	---	0.56	0.51	0.58	0.62	0.72	0.82
	7.0	-0.01	-0.04	-0.08	-0.12	-0.39	-0.64	---	0.56	0.51	0.58	0.62	0.72	0.82
	10.0	-0.01	-0.04	-0.08	-0.12	-0.39	-0.64	---	0.56	0.51	0.58	0.62	0.72	0.82
	15.0	-0.01	-0.04	-0.08	-0.12	-0.39	-0.64	---	0.56	0.51	0.58	0.62	0.72	0.82
	20.0	-0.01	-0.04	-0.08	-0.12	-0.39	-0.64	---	0.56	0.51	0.58	0.62	0.72	0.82
	30.0	-0.01	-0.04	-0.08	-0.12	-0.39	-0.64	---	0.56	0.51	0.58	0.62	0.72	0.82
	40.0	-0.01	-0.04	-0.08	-0.12	-0.39	-0.64	---	0.56	0.51	0.58	0.62	0.72	0.82
	50.0	-0.01	-0.04	-0.08	-0.12	-0.39	-0.64	---	0.56	0.51	0.58	0.62	0.72	0.82
	60.0	-0.01	-0.04	-0.08	-0.12	-0.39	-0.64	---	0.56	0.51	0.58	0.62	0.72	0.82
	70.0	-0.01	-0.04	-0.08	-0.12	-0.39	-0.64	---	0.56	0.51	0.58	0.62	0.72	0.82
0.375 b/2	0	-0.06	-0.15	-0.55	-0.45	-0.58	-0.63	---	0.56	0.51	0.58	0.62	0.72	0.82
	1.5	-0.00	-2.53	-1.54	-0.83	-0.76	-0.75	---	0.56	0.51	0.58	0.62	0.72	0.82
	4.0	-1.71	-2.44	-1.56	-0.79	-0.76	-0.73	---	0.56	0.51	0.58	0.62	0.72	0.82
	7.0	-1.36	-2.32	-1.45	-0.79	-0.76	-0.71	---	0.56	0.51	0.58	0.62	0.72	0.82
	10.0	-1.23	-1.37	-1.44	-0.77	-0.72	-0.71	---	0.56	0.51	0.58	0.62	0.72	0.82
	15.0	-1.11	-1.19	-1.33	-0.76	-0.70	-0.69	---	0.56	0.51	0.58	0.62	0.72	0.82
	20.0	-0.97	-1.05	-1.29	-0.74	-0.70	-0.69	---	0.56	0.51	0.58	0.62	0.72	0.82
	30.0	-0.74	-0.80	-1.17	-0.74	-0.70	-0.72	---	0.56	0.51	0.58	0.62	0.72	0.82
	40.0	-0.63	-0.64	-1.03	-0.73	-0.74	-0.78	---	0.56	0.51	0.58	0.62	0.72	0.82
	50.0	-0.50	-0.51	-0.88	-0.70	-0.75	-0.79	---	0.56	0.51	0.58	0.62	0.72	0.82
	60.0	-0.42	-0.41	-0.71	-0.70	-0.74	-0.77	---	0.56	0.51	0.58	0.62	0.72	0.82
	70.0	-0.31	-0.31	-0.57	-0.63	-0.68	-0.72	---	0.56	0.51	0.58	0.62	0.72	0.82
0.44 b/2	0	-0.20	-0.22	-0.41	-0.58	-0.64	-0.64	---	0.56	0.51	0.58	0.62	0.72	0.82
	1.5	-0.98	-2.45	-1.15	-0.84	-0.72	-0.68	---	0.56	0.51	0.58	0.62	0.72	0.82
	4.0	-1.69	-2.32	-1.14	-0.74	-0.65	-0.64	---	0.56	0.51	0.58	0.62	0.72	0.82
	7.0	-1.54	-2.33	-1.05	-0.70	-0.65	-0.64	---	0.56	0.51	0.58	0.62	0.72	0.82
	10.0	-1.24	-1.60	-1.01	-0.71	-0.65	-0.64	---	0.56	0.51	0.58	0.62	0.72	0.82
	15.0	-1.10	-1.19	-0.95	-0.69	-0.63	-0.64	---	0.56	0.51	0.58	0.62	0.72	0.82
	20.0	-0.96	-1.06	-0.90	-0.70	-0.63	-0.64	---	0.56	0.51	0.58	0.62	0.72	0.82
	30.0	-0.79	-0.84	-0.79	-0.64	-0.63	-0.63	---	0.56	0.51	0.58	0.62	0.72	0.82
	40.0	-0.63	-0.65	-0.79	-0.63	-0.62	-0.63	---	0.56	0.51	0.58	0.62	0.72	0.82
	50.0	-0.51	-0.51	-0.68	-0.60	-0.60	-0.63	---	0.56	0.51	0.58	0.62	0.72	0.82
	60.0	-0.39	-0.38	-0.64	-0.58	-0.59	-0.62	---	0.56	0.51	0.58	0.62	0.72	0.82
	70.0	-0.27	-0.25	-0.57	-0.54	-0.55	-0.59	---	0.56	0.51	0.58	0.62	0.72	0.82
	80.0	-0.13	-0.14	-0.53	-0.49	-0.51	-0.56	---	0.56	0.51	0.58	0.62	0.72	0.82
	90.0	-0.03	-0.07	-0.43	-0.42	-0.45	-0.51	---	0.56	0.51	0.58	0.62	0.72	0.82
	95.0	0	-0.05	-0.39	-0.38	-0.43	-0.50	---	0.56	0.51	0.58	0.62	0.72	0.82

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TABLE XIII.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING.
 $M_\infty = 0.60$; $R = 2,000,000$ - Concluded
 (b) α_u , $8^\circ, 10^\circ, 12^\circ, 14^\circ, 16^\circ, 18^\circ$ - Concluded

Spanwise station	Per-cent chord	Upper surface						Lower surface						
		Angle of attack						Angle of attack						
		8°	10°	12°	14°	16°	18°	8°	10°	12°	14°	16°	18°	
0.56 b/2	0	-0.20	-0.60	-0.71	-0.79	-0.80	-0.49	---	0.57	0.55	0.53	0.22	0.50	0.54
	1.5	-1.94	-2.34	-2.15	-1.98	-1.56	-0.69	0.46	0.52	0.53	0.54	0.55	0.55	0.57
	4.0	-1.58	-2.28	-2.03	-1.90	-1.40	-0.65	0.46	0.52	0.53	0.54	0.55	0.55	0.57
	7.0	-1.50	-2.26	-1.60	-1.42	-1.24	-0.64	0.46	0.52	0.53	0.54	0.55	0.55	0.57
	10.0	-1.27	-1.61	-1.37	-1.25	-1.24	-0.64	0.46	0.52	0.53	0.54	0.55	0.55	0.57
	15.0	-1.09	-1.20	-1.06	-1.00	-1.12	-0.63	0.46	0.52	0.53	0.54	0.55	0.55	0.57
	20.0	-0.91	-1.04	-0.90	-0.81	-0.95	-0.63	0.46	0.52	0.53	0.54	0.55	0.55	0.57
	30.0	-0.74	-0.79	-0.74	-0.70	-0.81	-0.61	0.46	0.52	0.53	0.54	0.55	0.55	0.57
	40.0	-0.61	-0.64	-0.66	-0.61	-0.71	-0.60	0.46	0.52	0.53	0.54	0.55	0.55	0.57
	50.0	-0.51	-0.51	-0.57	-0.56	-0.61	-0.57	0.46	0.52	0.53	0.54	0.55	0.55	0.57
	60.0	-0.38	-0.40	-0.50	-0.49	-0.51	-0.55	0.46	0.52	0.53	0.54	0.55	0.55	0.57
	70.0	-0.26	-0.30	-0.41	-0.41	-0.43	-0.51	0.46	0.52	0.53	0.54	0.55	0.55	0.57
	80.0	-0.14	-0.22	-0.32	-0.34	-0.38	-0.49	0.46	0.52	0.53	0.54	0.55	0.55	0.57
	90.0	-0.03	0	-0.12	-0.23	-0.28	-0.37	0.46	0.52	0.53	0.54	0.55	0.55	0.57
	95.0	0	-0.08	-0.14	-0.24	-0.34	-0.45	0.46	0.52	0.53	0.54	0.55	0.55	0.57
0.68 b/2	0	.02	-.01	.02	-.01	0	0	---	.56	.56	.54	.53	.51	.54
	1.5	-1.73	-2.33	-2.15	-1.71	-.95	-0.45	0.46	0.52	0.53	0.54	0.55	0.55	0.57
	4.0	-1.65	-2.18	-1.86	-1.36	-.92	-0.45	0.46	0.52	0.53	0.54	0.55	0.55	0.57
	7.0	-1.50	-2.18	-1.53	-1.25	-.88	-0.45	0.46	0.52	0.53	0.54	0.55	0.55	0.57
	10.0	-1.43	-1.55	-1.51	-1.26	-.89	-0.45	0.46	0.52	0.53	0.54	0.55	0.55	0.57
	15.0	-1.00	-1.14	-1.19	-1.11	-.80	-0.45	0.46	0.52	0.53	0.54	0.55	0.55	0.57
	20.0	-.97	-1.05	-1.10	-1.05	-.79	-0.44	0.46	0.52	0.53	0.54	0.55	0.55	0.57
	30.0	-.78	-.80	-.83	-.84	-.67	-0.42	0.46	0.52	0.53	0.54	0.55	0.55	0.57
	40.0	-.67	-.68	-.65	-.72	-.62	-0.40	0.46	0.52	0.53	0.54	0.55	0.55	0.57
	50.0	-.48	-.41	-.48	-.56	-.32	-.39	0.46	0.52	0.53	0.54	0.55	0.55	0.57
	60.0	-.34	-.27	-.36	-.49	-.30	-.38	0.46	0.52	0.53	0.54	0.55	0.55	0.57
	70.0	-.23	-.17	-.26	-.39	-.42	-.37	0.46	0.52	0.53	0.54	0.55	0.55	0.57
	80.0	-.10	-.09	-.20	-.32	-.39	-.37	0.46	0.52	0.53	0.54	0.55	0.55	0.57
	90.0	0	-.04	-.14	-.20	-.28	-.35	0.46	0.52	0.53	0.54	0.55	0.55	0.57
	95.0	.02	-.04	-.14	-.19	-.29	-.35	0.46	0.52	0.53	0.54	0.55	0.55	0.57
0.80 b/2	0	-.16	-.58	-.75	-.70	-.86	-.105	---	.56	.56	.58	.56	.51	.54
	1.5	-1.76	-2.35	-1.65	-1.20	-1.22	-1.51	0.46	0.52	0.53	0.54	0.55	0.55	0.57
	4.0	-1.48	-2.14	-1.76	-1.23	-1.25	-1.50	0.46	0.52	0.53	0.54	0.55	0.55	0.57
	7.0	-1.33	-2.10	-1.54	-1.12	-1.17	-1.41	0.46	0.52	0.53	0.54	0.55	0.55	0.57
	10.0	-1.23	-1.27	-1.41	-1.11	-1.18	-1.47	0.46	0.52	0.53	0.54	0.55	0.55	0.57
	15.0	-.98	-1.11	-1.19	-1.03	-1.09	-1.38	0.46	0.52	0.53	0.54	0.55	0.55	0.57
	20.0	-.87	-.95	-.95	-.90	-.99	-1.43	0.46	0.52	0.53	0.54	0.55	0.55	0.57
	30.0	-.68	-.74	-.81	-.90	-.99	-1.26	0.46	0.52	0.53	0.54	0.55	0.55	0.57
	40.0	-.56	-.58	-.68	-.85	-.94	-1.05	0.46	0.52	0.53	0.54	0.55	0.55	0.57
	50.0	-.46	-.44	-.54	-.77	-.83	-1.05	0.46	0.52	0.53	0.54	0.55	0.55	0.57
	60.0	-.34	-.31	-.45	-.69	-.75	-1.01	0.46	0.52	0.53	0.54	0.55	0.55	0.57
	70.0	-.24	-.20	-.35	-.59	-.65	-1.05	0.46	0.52	0.53	0.54	0.55	0.55	0.57
	80.0	-.13	-.11	-.28	-.50	-.55	-1.04	0.46	0.52	0.53	0.54	0.55	0.55	0.57
	90.0	-.01	-.02	-.28	-.40	-.44	-1.04	0.46	0.52	0.53	0.54	0.55	0.55	0.57
	95.0	.02	-.06	-.18	-.35	-.37	-1.04	0.46	0.52	0.53	0.54	0.55	0.55	0.57
0.94 b/2	0	.16	-.20	-.46	-.51	-.64	-.08	---	.57	.56	.56	.54	.55	---
	1.5	-1.31	-2.10	-2.39	-1.53	-1.23	-1.03	0.46	0.52	0.53	0.54	0.55	0.55	0.57
	4.0	-1.19	-2.00	-2.13	-1.56	-1.27	-1.08	0.46	0.52	0.53	0.54	0.55	0.55	0.57
	7.0	-1.18	-1.21	-1.46	-1.43	-1.19	-1.01	0.46	0.52	0.53	0.54	0.55	0.55	0.57
	10.0	-1.00	-1.13	-1.37	-1.38	-1.20	-1.04	0.46	0.52	0.53	0.54	0.55	0.55	0.57
	15.0	-.83	-.94	-1.01	-1.25	-1.10	-1.06	0.46	0.52	0.53	0.54	0.55	0.55	0.57
	20.0	-.69	-.82	-.89	-1.18	-1.10	-1.06	0.46	0.52	0.53	0.54	0.55	0.55	0.57
	30.0	-.24	-.60	-.65	-.96	-.97	-.87	0.46	0.52	0.53	0.54	0.55	0.55	0.57
	40.0	-.44	-.48	-.49	-.76	-.93	-.84	0.46	0.52	0.53	0.54	0.55	0.55	0.57
	50.0	-.36	-.35	-.35	-.61	-.80	-.75	0.46	0.52	0.53	0.54	0.55	0.55	0.57
	60.0	-.28	-.26	-.26	-.44	-.70	-.73	0.46	0.52	0.53	0.54	0.55	0.55	0.57
	70.0	-.21	-.16	-.17	-.34	-.55	-.64	0.46	0.52	0.53	0.54	0.55	0.55	0.57
	80.0	-.11	-.07	-.10	-.23	-.45	-.58	0.46	0.52	0.53	0.54	0.55	0.55	0.57
	90.0	-.01	0	-.06	-.11	-.28	-.46	0.46	0.52	0.53	0.54	0.55	0.55	0.57
	95.0	.06	-.01	-.04	-.11	-.28	-.46	0.46	0.52	0.53	0.54	0.55	0.55	0.57

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TABLE XIV.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING.
 $M_\infty = 0.80$; $R = 2,000,000$
(a) $\alpha_u = -4^\circ, -2^\circ, 0^\circ, 2^\circ, 4^\circ, 6^\circ$

Spanwise station	Percent chord	Upper surface						Lower surface					
		Angle of attack						Angle of attack					
		-4°	-2°	0°	2°	4°	6°	-4°	-2°	0°	2°	4°	6°
0.10 b/2	0	0.16	0.35	0.50	0.60	0.65	0.64	-0.74	-0.47	-0.20	0.05	0.26	0.44
	1.5	.46	.37	.23	.06	-.14	-.38	-.99	-.62	-.36	-.13	.06	.23
	4.0	.26	.16	.01	-.16	-.35	-.57	---	---	---	---	---	---
	7.0	.11	.02	-.13	-.29	-.46	-.68	---	---	---	---	---	---
	10.0	.06	-.05	-.20	-.34	-.49	-.67	-.78	-.58	-.40	-.22	-.07	.07
	15.0	-.03	-.13	-.25	-.39	-.53	-.67	-.77	-.56	-.40	-.24	-.11	.08
	20.0	-.09	-.19	-.30	-.42	-.56	-.70	-.67	-.50	-.36	-.22	-.11	.01
	30.0	-.14	-.22	-.32	-.42	-.54	-.67	-.55	-.41	-.32	-.20	-.11	.01
	40.0	-.14	-.22	-.31	-.40	-.50	-.62	-.42	-.32	-.25	-.17	-.09	.01
	50.0	-.14	-.21	-.30	-.39	-.45	-.56	-.33	-.25	-.19	-.13	-.06	.04
	60.0	-.14	-.20	-.27	-.33	-.39	-.47	-.23	-.18	-.12	-.05	-.01	.04
	70.0	-.15	-.19	-.25	-.29	-.34	-.39	-.14	-.09	-.05	-.01	-.03	.06
	80.0	-.13	-.16	-.20	-.22	-.25	-.26	---	---	---	---	---	---
	90.0	-.08	-.02	-.03	-.05	-.04	-.04	.01	.02	.02	.04	.05	.07
	95.0	.06	.06	.05	.04	.03	.01	.05	.05	.05	.05	.05	.06
0.19 b/2	0	.02	.23	.45	.57	.59	.52	---	---	---	---	---	---
	1.5	.50	.46	.23	.01	-.30	-.62	-.109	-.78	-.34	.01	.27	.45
	4.0	.28	.15	.04	-.26	-.53	-.84	-.127	-.93	-.50	-.19	.05	.24
	7.0	.16	.02	-.13	-.35	-.59	-.84	---	---	---	---	---	---
	10.0	.06	-.07	-.23	-.44	-.67	-.90	-.119	-.79	-.48	-.25	-.06	.07
	15.0	-.04	-.16	-.32	-.50	-.70	-.93	-.103	-.67	-.44	-.27	-.12	.02
	20.0	-.09	-.21	-.33	-.51	-.70	-.90	-.106	-.68	-.49	-.39	-.25	-.12
	30.0	-.16	-.26	-.38	-.51	-.67	-.88	-.146	-.68	-.48	-.30	-.20	-.01
	40.0	-.20	-.29	-.38	-.49	-.62	-.82	-.133	-.68	-.40	-.20	-.15	-.07
	50.0	-.19	-.25	-.35	-.44	-.51	-.54	---	---	---	---	---	---
	60.0	-.17	-.22	-.30	-.34	-.40	-.40	-.14	-.11	-.07	-.03	.02	.06
	70.0	-.16	-.20	-.25	-.27	-.30	-.31	-.06	-.04	-.01	.02	.03	.09
	80.0	-.11	-.14	-.17	-.19	-.19	-.17	---	---	---	---	---	---
	90.0	-.01	-.02	-.04	-.03	-.02	-.01	.05	.06	.07	.07	.08	.09
	95.0	.06	.06	.06	.06	.05	.05	.07	.09	.09	.09	.08	.08
0.31 b/2	0	-.01	.22	.45	.57	.58	.48	---	---	---	---	---	---
	1.5	.52	.43	.26	-.01	-.34	-.69	-.111	-.83	-.35	.04	.31	.48
	4.0	.31	.17	-.04	-.32	-.54	-.97	-.120	-.07	-.52	-.15	.10	.29
	7.0	.17	.02	-.18	-.44	-.74	-.105	---	---	---	---	---	---
	10.0	.08	-.06	-.23	-.49	-.76	-.105	-.119	-.85	-.48	-.24	-.05	.10
	15.0	-.03	-.17	-.33	-.58	-.85	-.115	-.96	-.62	-.43	-.24	-.10	.04
	20.0	-.09	-.22	-.38	-.58	-.83	-.113	-.78	-.45	-.37	-.21	-.09	.03
	30.0	-.15	-.26	-.40	-.54	-.73	-.107	-.51	-.35	-.23	-.18	-.08	.02
	40.0	-.18	-.27	-.39	-.50	-.60	-.53	-.33	-.25	-.17	-.12	-.05	.03
	50.0	-.19	-.23	-.35	-.44	-.49	-.46	-.20	-.15	-.09	-.03	-.02	-.02
	60.0	-.16	-.23	-.31	-.32	-.37	-.38	---	---	---	---	---	---
	70.0	-.17	-.20	-.25	-.28	-.29	-.28	-.04	-.01	-.01	.04	.07	.10
	80.0	-.13	-.14	-.17	-.19	-.18	-.16	---	---	---	---	---	---
	90.0	0	-.02	-.02	0	-.02	-.02	.08	.07	.09	.08	.09	.10
	95.0	.06	.07	.06	.07	.06	.06	.09	.10	.11	.10	.10	.10
0.375 b/2	0	-.07	.17	.45	.58	.57	.46	---	---	---	---	---	---
	1.5	.54	.42	.22	-.09	-.49	-.94	-.15	-.85	-.33	.06	.34	.49
	4.0	.36	.21	0	-.29	-.61	-.92	-.13	-.07	-.51	-.14	.11	.30
	7.0	.19	.02	-.19	-.45	-.78	-.108	---	---	---	---	---	---
	10.0	.09	-.07	-.28	-.54	-.84	-.118	-.13	-.89	-.46	-.22	-.03	.11
	15.0	-.02	-.17	-.38	-.58	-.90	-.122	-.89	-.57	-.42	-.23	-.08	.05
	20.0	-.08	-.22	-.39	-.59	-.84	-.118	-.73	-.46	-.37	-.20	-.07	.04
	30.0	-.14	.26	.39	-.54	-.74	-.114	-.54	-.34	-.23	-.16	-.06	.01
	40.0	-.18	.26	.39	-.50	-.76	-.63	-.36	-.24	-.18	-.11	-.03	.03
	50.0	-.18	.25	.34	-.44	-.65	-.44	---	---	---	---	---	---
	60.0	-.17	.22	.31	-.31	-.37	-.37	-.14	-.06	-.03	.01	.03	.07
	70.0	-.17	.20	.26	-.27	-.30	-.30	-.03	-.01	-.02	.05	.08	.10
	80.0	-.14	.18	.20	-.20	-.20	-.19	---	---	---	---	---	---
	90.0	-.03	-.03	-.02	-.03	-.01	-.03	.06	.07	.09	.09	.10	.10
	95.0	.03	.06	.07	.07	.06	.05	.08	.10	.12	.11	.10	.10
0.44 b/2	0	-.08	.16	.43	.59	.57	.46	---	---	---	---	---	---
	1.5	.53	.41	.21	-.10	-.50	-.91	-.113	-.90	-.39	.10	.37	.51
	4.0	.35	.19	-.02	-.31	-.67	-.99	-.115	-.111	-.54	.15	.11	.30
	7.0	.20	.04	-.20	-.46	-.81	-.108	---	---	---	---	---	---
	10.0	.10	-.06	-.26	-.53	-.88	-.118	-.103	-.94	-.46	-.21	-.02	.13
	20.0	-.08	-.21	-.39	-.58	-.84	-.118	-.71	-.45	-.37	-.19	-.06	.06
	30.0	-.15	.27	.40	-.55	-.74	-.114	-.52	-.33	-.22	-.14	-.05	.03
	40.0	-.17	.26	.38	-.50	-.78	-.65	-.35	-.29	-.18	-.11	-.04	.03
	50.0	-.18	.25	.33	-.44	-.74	-.47	-.23	-.14	-.09	-.02	-.01	.05
	60.0	-.18	.23	.31	-.32	-.37	-.36	-.14	-.07	-.03	.01	.03	.07
	70.0	-.17	.20	.26	-.26	-.28	-.26	-.05	0	-.03	.06	.09	.11
	80.0	-.13	.14	.15	-.18	-.15	-.15	---	---	---	---	---	---
	90.0	-.03	-.02	-.02	-.02	-.01	-.03	.05	.08	.09	.09	.09	.08
	95.0	.03	.06	.07	.06	.07	.06	.08	.11	.12	.11	.09	.08

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TABLE XIV.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING.

 $M_\infty = 0.80; R = 2,000,000$ - Continued(a) $\alpha_u = -4^\circ, -2^\circ, 0^\circ, 2^\circ, 4^\circ, 6^\circ$ - Concluded

Spanwise station	Percent chord	Upper surface						Lower surface					
		Angle of attack						Angle of attack					
		-4°	-2°	0°	2°	4°	6°	-4°	-2°	0°	2°	4°	6°
0.56 b/2	0	-0.06	0.16	0.14	0.59	0.56	0.39	---	---	0.46	---	0.35	0.50
	1.5	.56	.46	.26	-.05	-.44	-.88	-1.00	-1.05	---	0.05	0.12	.31
	4.0	.37	.23	.01	-.23	-.63	-1.02	-1.08	-1.14	-.56	-.15	0.12	0.13
	7.0	.21	.07	-.15	-.45	-.78	-1.08	---	---	---	---	---	---
	10.0	.11	-.04	-.25	-.53	-.84	-1.13	-.84	-.99	-.50	-.22	-.02	0.13
	15.0	.01	-.14	-.33	-.58	-.95	-1.23	-.73	-.55	-.43	-.22	-.06	.07
	20.0	-.04	-.17	-.34	-.54	-.87	-1.17	-.61	-.45	-.35	-.18	-.05	.06
	30.0	-.12	-.23	-.36	-.51	-.65	-1.12	-.49	-.34	-.22	-.14	-.05	.03
	40.0	-.16	-.24	-.35	-.56	-.52	-.75	-.36	-.22	-.14	-.09	-.02	.04
	50.0	-.17	-.25	-.33	-.42	-.46	-.48	-.27	-.13	-.09	-.02	0.01	.05
	60.0	-.16	-.25	-.29	-.31	-.35	-.35	---	---	---	---	---	---
	70.0	-.16	-.19	-.25	-.24	-.27	-.27	-.11	0	0.03	.06	.06	.09
	80.0	-.14	-.14	-.15	-.17	-.15	-.17	-.04	.06	.08	.09	.10	.12
	90.0	-.04	-.08	-.08	-.01	-.01	-.03	0.01	.09	.10	.10	.09	.11
	95.0	.02	-.06	-.07	.09	.07	.06	.04	.12	.13	.12	.10	.11
0.68 b/2	0	---	---	---	---	---	---	---	---	---	---	---	---
	1.5	.71	.51	.35	.05	-.34	-.73	-.90	-.18	-.56	-.02	.31	.48
	4.0	.37	.26	.03	-.29	-.67	-.07	-1.03	-1.20	-.62	-.19	.09	.29
	7.0	.24	.11	-.11	-.41	-.77	-.125	---	---	---	---	---	---
	10.0	.14	.01	-.20	-.43	-.84	-.139	-.76	-.08	-.53	-.23	-.02	.13
	15.0	.03	-.07	-.20	-.49	-.78	-.115	-.71	-.60	-.41	-.23	-.06	.07
	20.0	-.03	-.14	-.31	-.53	-.72	-.12	-.60	-.44	-.31	-.19	-.05	.04
	30.0	-.11	-.21	-.35	-.58	-.81	-.11	-.51	-.33	-.22	-.14	-.09	.03
	40.0	-.15	-.22	-.33	-.45	-.55	-.59	-.37	-.28	-.14	-.09	-.03	.05
	50.0	-.17	-.23	-.30	-.40	-.42	-.41	---	---	---	---	---	---
	60.0	-.15	-.19	-.25	-.27	-.31	-.31	-.21	-.07	-.02	.02	.04	.06
	70.0	-.15	-.16	-.19	-.23	-.24	-.21	-.15	-.01	-.02	.05	.07	.08
	80.0	-.13	-.13	-.14	-.16	-.14	-.10	-.09	0	-.08	.08	.10	.10
	90.0	-.04	0	0	0	0.01	0	-.02	.09	.10	.10	.10	.08
	95.0	0	-.06	-.07	.07	.08	.03	-.01	.11	.12	.12	.10	.08
0.80 b/2	0	.04	.19	.45	.62	.60	.41	---	---	---	---	---	---
	1.5	.57	.51	.35	.04	-.37	-.83	-.85	-.19	-.75	-.12	.26	.46
	4.0	.40	.30	.11	-.19	-.57	-.94	-.83	-.28	-.73	-.27	.05	.26
	7.0	.27	.16	-.04	-.32	-.67	-.05	---	---	---	---	---	---
	10.0	.18	.06	-.13	-.39	-.71	-.12	-.88	-.09	-.58	-.28	-.07	.10
	15.0	.07	-.04	-.21	-.45	-.73	-.10	-.80	-.69	-.49	-.26	-.06	.05
	20.0	0	-.10	-.25	-.47	-.70	-.04	-.77	-.47	-.37	-.23	-.06	.08
	30.0	-.07	-.14	-.27	-.42	-.59	-.00	-.72	-.37	-.23	-.16	---	---
	40.0	-.11	-.18	-.27	-.40	-.48	-.45	---	---	---	---	---	---
	50.0	-.15	-.19	-.27	-.36	-.40	-.42	-.25	-.15	-.09	-.04	-.03	.04
	60.0	-.14	-.18	-.24	-.31	-.31	-.31	-.23	-.08	-.02	.01	.02	.06
	70.0	-.14	-.16	-.20	-.23	-.24	-.22	-.26	-.01	.03	.05	.03	.09
	80.0	-.11	-.12	-.15	-.14	-.14	-.11	-.14	.05	.08	.08	.09	.09
	90.0	-.01	-.02	0	-.01	0	0	-.02	.08	.11	.10	.10	.09
	95.0	-.06	-.06	-.08	-.07	-.08	-.05	-.06	.10	.13	.13	.12	.09
0.94 b/2	0	-.02	-.06	.18	.48	.60	.56	---	---	---	---	---	---
	1.5	.32	.51	.41	.26	-.20	-.67	---	-.75	-.113	-.42	.09	.37
	4.0	.39	.35	.20	-.06	-.40	-.80	---	---	---	---	---	---
	7.0	.29	.19	.05	-.21	-.52	-.94	-.32	-.72	-.83	-.36	-.08	.12
	10.0	.16	.10	-.04	-.27	-.54	-.101	-.29	-.61	-.53	-.35	-.13	.04
	15.0	.07	.01	-.12	-.32	-.56	-.89	-.29	-.61	-.48	-.31	-.13	.01
	20.0	0	-.05	-.17	-.35	-.55	-.83	-.26	-.49	-.36	-.26	-.12	-.01
	30.0	-.10	-.13	-.22	-.35	-.49	-.59	-.24	-.41	-.28	-.17	-.09	.02
	40.0	-.14	-.16	-.23	-.32	-.42	-.40	-.20	-.26	-.14	-.09	-.07	.08
	50.0	-.20	-.19	-.23	-.29	-.34	-.32	-.19	-.20	-.06	-.04	-.03	.01
	60.0	-.20	-.17	-.19	-.24	-.22	-.24	---	---	---	---	---	---
	70.0	-.22	-.15	-.16	-.19	-.17	-.18	-.15	-.05	.06	.05	.06	.04
	80.0	-.22	-.12	-.12	-.09	-.09	-.08	-.12	0	.10	.09	.09	.09
	90.0	-.17	-.02	.05	.03	.04	.03	-.14	.04	.13	.11	.11	.10
	95.0	-.15	.04	.11	.10	.11	.10	-.12	.06	.15	.14	.11	.11

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TABLE XIV.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING.
 $M_\infty = 0.80$; $R = 2,000,000$ - Continued
 (b) α_u , $8^\circ, 10^\circ, 12^\circ, 14^\circ, 16^\circ$

Spanwise station	Percent chord	Upper surface					Lower surface				
		Angle of attack					Angle of attack				
		8°	10°	12°	14°	16°	8°	10°	12°	14°	16°
0.10 b/2	0	0.57	0.48	0.39	0.26	0.16	---	---	---	---	---
	1.5	-0.64	-0.92	-1.19	-1.34	-1.44	0.57	0.67	0.74	0.80	0.84
	4.0	-0.79	-0.98	-1.21	-1.45	-1.58	-0.58	-0.49	-0.39	-0.66	-0.74
	7.0	-0.91	-1.11	-1.32	-1.38	-1.50	---	---	---	---	---
	10.0	-0.87	-1.06	-1.25	-1.48	-1.57	-0.19	-0.30	-0.39	-0.46	-0.53
	15.0	-0.83	-1.03	-1.27	-1.49	-1.52	-0.13	-0.23	-0.30	-0.37	-0.44
	20.0	-0.81	-0.95	-1.09	-1.33	-1.34	-0.11	-0.20	-0.26	-0.33	-0.39
	30.0	-0.84	-0.92	-1.05	-1.07	-1.20	-0.07	-0.14	-0.21	-0.29	-0.31
	40.0	-0.73	-0.85	-0.96	-0.94	-1.08	-0.07	-0.13	-0.17	-0.22	-0.27
	50.0	-0.66	-0.78	-0.89	-0.72	-0.98	-0.07	-0.13	-0.16	-0.20	-0.24
	60.0	-0.58	-0.63	-0.75	-0.74	-0.87	-0.09	-0.14	-0.16	-0.19	-0.22
	70.0	-0.43	-0.38	-0.45	-0.71	-0.80	-0.11	-0.15	-0.17	-0.19	-0.21
	80.0	-0.25	-0.24	-0.34	-0.50	-0.69	---	---	---	---	---
	90.0	-0.03	-0.09	-0.16	-0.31	-0.44	-0.09	-0.10	-0.08	-0.06	0.03
	95.0	-0.02	-0.04	-0.13	-0.25	-0.36	-0.06	-0.06	-0.04	0.00	-0.03
0.19 b/2	0	.40	.26	.09	-.08	.21	---	---	---	---	---
	1.5	-0.92	-1.10	-1.26	-1.39	-1.34	-0.56	-0.62	-0.65	-0.66	-0.66
	4.0	-1.14	-1.40	-1.55	-1.41	-1.32	-0.38	-0.48	-0.55	-0.59	-0.65
	7.0	-1.14	-1.40	-1.40	-1.56	-1.38	---	---	---	---	---
	10.0	-1.15	-1.39	-1.53	-1.37	-1.29	-0.20	-0.30	-0.36	-0.44	-0.49
	15.0	-1.20	-1.42	-1.51	-1.28	-1.20	-0.12	-0.22	-0.29	-0.36	-0.41
	20.0	-1.15	-1.38	-1.50	-1.24	-1.20	-0.08	-0.13	-0.18	-0.23	-0.25
	30.0	-1.12	-1.35	-1.28	-1.15	-1.14	-0.08	-0.13	-0.16	-0.20	-0.23
	40.0	-1.02	-1.17	-1.08	-1.12	-1.16	-0.08	-0.13	-0.16	-0.20	-0.23
	50.0	-0.67	-0.58	-0.94	-1.06	-1.05	---	---	---	---	---
	60.0	-0.32	-0.38	-0.80	-1.00	-1.01	-0.10	-0.12	-0.13	-0.15	-0.15
	70.0	-0.26	-0.26	-0.64	-0.91	-0.96	-0.11	-0.12	-0.13	-0.12	-0.12
	80.0	-0.14	-0.14	-0.44	-0.78	-0.88	---	---	---	---	---
	90.0	-0.04	-0.03	-0.29	-0.63	-0.78	-0.09	-0.07	-0.04	-0.02	-0.07
	95.0	0.04	-0.02	-0.19	-0.55	-0.72	-0.06	-0.03	-0.02	-0.13	-0.21
0.31 b/2	0	.34	.20	.05	-.09	.21	---	---	---	---	---
	1.5	-0.95	-1.12	-1.20	-1.96	-0.94	0.57	0.61	0.62	0.62	0.61
	4.0	-1.25	-1.32	-1.18	-1.96	-0.94	-0.40	-0.49	0.54	0.59	0.61
	7.0	-1.33	-1.26	-1.15	-1.96	-0.93	---	---	---	---	---
	10.0	-1.36	-1.29	-1.12	-1.94	-0.92	-0.22	-0.31	-0.36	-0.42	-0.46
	15.0	-1.40	-1.19	-1.02	-1.89	-0.86	-0.15	-0.23	-0.28	-0.33	-0.37
	20.0	-1.33	-1.10	-0.99	-1.86	-0.84	-0.12	-0.18	-0.23	-0.28	-0.32
	30.0	-1.31	-0.95	-0.89	-1.81	-0.82	-0.09	-0.14	-0.16	-0.20	-0.23
	40.0	-0.98	-0.84	-0.83	-1.79	-0.82	-0.06	-0.11	-0.12	-0.15	-0.17
	50.0	-0.67	-0.76	-0.77	-0.74	-0.77	-0.09	-0.11	-0.11	-0.11	-0.13
	60.0	-0.39	-0.68	-0.70	-0.70	-0.74	---	---	---	---	---
	70.0	-0.25	-0.57	-0.60	-0.60	-0.64	-0.12	-0.09	-0.06	-0.04	-0.04
	80.0	-0.15	-0.47	-0.24	-0.59	-0.62	-0.10	-0.01	-0.10	-0.15	-0.16
	90.0	-0.08	-0.31	-0.40	-0.49	-0.51	-0.10	-0.06	-0.02	-0.19	-0.24
	95.0	0.04	-0.31	-0.42	-0.51	-0.54	-0.10	-0.06	-0.02	-0.26	-0.25
0.375 b/2	0	.31	.16	.04	-.07	.19	---	---	---	---	---
	1.5	-1.17	-1.10	-0.82	-0.63	-0.63	0.57	0.60	0.61	0.62	0.61
	4.0	-1.29	-1.07	-0.82	-0.63	-0.64	-0.41	-0.48	0.52	0.57	0.60
	7.0	-1.32	-0.97	-0.79	-0.62	-0.63	---	---	---	---	---
	10.0	-1.31	-0.92	-0.78	-0.61	-0.63	-0.23	-0.30	-0.35	-0.40	-0.44
	15.0	-1.27	-0.85	-0.74	-0.60	-0.62	-0.16	-0.18	-0.26	-0.31	-0.35
	20.0	-1.26	-0.83	-0.74	-0.61	-0.63	-0.13	-0.17	-0.21	-0.25	-0.29
	30.0	-1.05	-0.76	-0.70	-0.63	-0.63	-0.09	-0.12	-0.14	-0.18	-0.20
	40.0	-0.91	-0.71	-0.68	-0.65	-0.70	-0.06	-0.09	-0.11	-0.13	-0.15
	50.0	-0.76	-0.65	-0.67	-0.67	-0.70	---	---	---	---	---
	60.0	-0.64	-0.60	-0.65	-0.66	-0.69	-0.10	-0.07	-0.04	-0.06	-0.06
	70.0	-0.51	-0.53	-0.61	-0.62	-0.66	-0.11	-0.06	-0.02	-0.02	-0.01
	80.0	-0.36	-0.45	-0.57	-0.59	-0.65	---	---	---	---	---
	90.0	-0.20	-0.34	-0.49	-0.53	-0.60	-0.09	-0.06	-0.02	-0.14	-0.16
	95.0	-0.09	-0.30	-0.46	-0.53	-0.60	-0.07	-0.13	-0.23	-0.26	-0.26
0.44 b/2	0	.31	.19	.13	-.07	.05	---	---	---	---	---
	1.5	-1.11	-1.13	-0.66	-0.61	-0.63	0.59	0.61	0.61	0.62	0.61
	4.0	-1.29	-1.21	-0.67	-0.61	-0.63	-0.41	-0.46	0.50	0.54	0.56
	7.0	-1.21	-1.16	-0.66	-0.60	-0.62	---	---	---	---	---
	10.0	-1.21	-1.12	-0.65	-0.59	-0.61	-0.25	-0.29	0.32	0.37	0.40
	15.0	-1.17	-1.03	-0.62	-0.58	-0.61	-0.16	-0.21	0.24	0.26	0.32
	20.0	-1.01	-0.95	-0.60	-0.58	-0.61	-0.13	-0.16	0.18	0.22	0.26
	30.0	-0.84	-0.80	-0.59	-0.58	-0.61	-0.08	-0.11	0.11	0.15	0.14
	40.0	-0.73	-0.67	-0.58	-0.58	-0.61	-0.06	-0.07	0.07	0.09	0.11
	50.0	-0.62	-0.56	-0.57	-0.57	-0.61	-0.08	-0.07	0.06	0.08	0.09
	60.0	-0.54	-0.47	-0.55	-0.57	-0.61	-0.09	-0.05	0.02	0.02	0.04
	70.0	-0.47	-0.40	-0.53	-0.53	-0.59	-0.10	-0.05	0.01	0.01	0.01
	80.0	-0.39	-0.35	-0.50	-0.53	-0.58	---	---	---	---	---
	90.0	-0.31	-0.30	-0.45	-0.48	-0.53	-0.07	-0.06	-0.14	-0.15	-0.18
	95.0	-0.28	-0.28	-0.43	-0.43	-0.50	-0.07	-0.11	-0.22	-0.23	-0.26

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TABLE XIV.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING.
 $M_\infty = 0.80$; $R = 2,000,000$ - Concluded
 (b) α_u , $8^\circ, 10^\circ, 12^\circ, 14^\circ, 16^\circ$ - Concluded

Spanwise station	Per-cent chord	Upper surface					Lower surface				
		Angle of attack					Angle of attack				
		8°	10°	12°	14°	16°	8°	10°	12°	14°	16°
0.56 b/2	0	0.23	0.09	0.01	-0.13	-0.24	---	---	---	---	---
	1.5	-1.07	-1.20	-1.25	-1.34	-1.11	0.57	0.59	0.59	0.59	0.58
	4.0	-1.30	-1.48	-1.52	-1.42	-1.13	.40	.43	.47	.51	.53
	7.0	-1.33	-1.49	-1.46	-1.38	-1.08	---	---	---	---	---
	10.0	-1.34	-1.49	-1.43	-1.35	-1.09	.22	.27	.29	.33	.38
	15.0	-1.34	-1.44	-1.41	-1.26	-1.03	.15	.19	.21	.25	.29
	20.0	-1.32	-1.42	-1.40	-1.15	-1.01	.12	.16	.16	.21	.25
	30.0	-1.01	-1.20	-.71	-.84	-.89	.07	.10	.10	.13	.15
	40.0	-.58	-.83	-.57	-.62	-.79	.07	.08	.07	.10	.10
	50.0	-.48	-.51	-.49	-.55	-.68	.06	.07	.05	.07	.07
	60.0	-.39	-.35	-.45	-.50	-.57	---	---	---	---	---
	70.0	-.30	-.32	-.40	-.43	-.50	.08	.07	.08	.03	.02
	80.0	-.21	-.23	-.36	-.37	-.46	.09	.08	.01	0	-.03
	90.0	-.07	-.10	-.29	-.34	-.44	.06	.05	-.06	-.08	-.13
	95.0	-.03	-.04	-.26	-.32	-.41	.06	.04	-.09	-.13	-.19
0.68 b/2	0	---	---	---	---	---	---	---	---	---	---
	1.5	-.97	-1.07	-1.07	-1.07	-.90	.54	.58	.56	.58	.58
	4.0	-1.27	-.97	-1.07	-1.04	-.76	.38	.44	.47	.50	.52
	7.0	-1.25	-.96	-.99	-.99	-.72	---	---	---	---	---
	10.0	-1.23	-.92	-.97	-.98	-.74	.21	.27	.29	.34	.36
	15.0	-1.22	-.81	-.88	-.89	-.69	.14	.19	.21	.26	.28
	20.0	-1.00	-.78	-.86	-.86	-.59	.11	.16	.17	.20	.23
	30.0	-.83	-.58	-.76	-.76	-.82	.08	.11	.12	.13	.15
	40.0	-.67	-.63	-.71	-.74	-.60	.07	.09	.08	.10	.10
	50.0	-.53	-.56	-.63	-.68	-.53	---	---	---	---	---
	60.0	-.42	-.50	-.60	-.63	-.51	.08	.07	.06	.06	.05
	70.0	-.30	-.42	-.54	-.59	-.46	.09	.05	.04	.04	.01
	80.0	-.22	-.38	-.50	-.53	-.45	.09	.03	.01	.01	.03
	90.0	-.15	-.29	-.38	-.40	-.39	.05	.04	-.06	-.08	-.12
	95.0	-.13	-.30	-.37	-.40	-.39	.01	-.11	-.14	-.16	-.20
0.80 b/2	0	.25	.12	-.01	-.17	-.27	---	---	---	---	---
	1.5	-1.10	-1.23	-1.27	-1.11	-1.06	.54	.57	.58	.59	.59
	4.0	-1.27	-1.38	-1.27	-1.12	-1.09	.36	.41	.44	.49	.51
	7.0	-1.27	-1.29	-1.18	-1.10	-1.06	---	---	---	---	---
	10.0	-1.20	-1.28	-1.15	-1.08	-1.03	.20	.24	.28	.33	.36
	15.0	-1.18	-1.24	-1.03	-1.02	-.97	.12	.17	.20	.24	.27
	20.0	-1.17	-1.11	-1.00	-1.01	-.95	.11	.15	.17	.21	.23
	30.0	-.92	-.90	-.90	-.92	-.91	.07	.09	.11	.13	.15
	40.0	-.71	-.81	-.85	-.87	-.91	---	---	---	---	---
	50.0	-.56	-.71	-.76	-.79	-.84	.06	.06	.06	.07	.07
	60.0	-.45	-.61	-.69	-.73	-.80	.07	.07	.06	.06	.06
	70.0	-.35	-.51	-.60	-.66	-.73	.09	.08	.06	.05	.04
	80.0	-.23	-.35	-.51	-.60	-.69	.09	.07	.03	0	-.01
	90.0	-.13	-.23	-.41	-.51	-.56	.08	.06	-.03	-.08	-.09
	95.0	-.06	-.14	-.36	-.47	-.50	.06	.02	-.08	-.14	-.15
0.94 b/2	0	.39	.27	.15	.01	-.10	---	---	---	---	---
	1.5	-1.08	-1.33	-1.32	-1.14	-1.06	---	.53	.55	.56	.56
	4.0	-1.10	-1.38	-1.27	-1.20	-1.15	---	---	---	---	---
	7.0	-1.15	-1.22	-1.27	-1.11	-1.06	.23	.29	.32	.36	.40
	10.0	-1.18	-1.20	-1.20	-1.06	-1.05	.15	.21	.24	.28	.31
	15.0	-1.12	-1.17	-1.03	-.96	-.98	.08	.13	.16	.20	.23
	20.0	-1.11	-1.05	-.96	-.94	-.96	.06	.10	.11	.14	.17
	30.0	-.83	-.81	-.83	-.84	-.84	.02	.05	.05	.07	.09
	40.0	-.43	-.66	-.74	-.79	-.80	.01	.02	.02	.02	.03
	50.0	-.31	-.51	-.63	-.72	-.73	---	0	0	0	0
	60.0	-.24	-.40	-.57	-.66	-.71	---	---	---	---	---
	70.0	-.15	-.28	-.45	-.59	-.64	.05	.04	.01	-.02	-.04
	80.0	-.07	-.19	-.36	-.51	-.58	.07	.05	.01	-.04	-.08
	90.0	.02	-.10	-.26	-.42	-.50	.07	.05	-.01	-.10	-.15
	95.0	.06	-.05	-.20	-.38	-.45	.08	.03	-.06	-.17	-.23

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TABLE XV.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING.
 $M_\infty = 0.86$; $R = 2,000,000$
(a) α_{ul} , $-4^\circ, -2^\circ, 0^\circ, 2^\circ, 4^\circ, 6^\circ$

Spanwise station	Percent chord	Upper surface						Lower surface					
		Angle of attack						Angle of attack					
		-4°	-2°	0°	2°	4°	6°	-4°	-2°	0°	2°	4°	6°
0.10 b/2	0	0.24	0.40	0.53	0.61	0.67	0.67	-	-	-	-	-	-
	1.5	.47	.38	.25	.10	-.06	-.25	-	-0.60	-0.40	-0.14	0.06	0.25
	4.0	.27	.17	.04	-.11	-.29	-.45	-.80	-.56	-.33	-.12	.06	.22
	7.0	.11	.05	-.11	-.24	-.42	-.59	-	-	-	-	-	-
	10.0	.06	-.05	-.18	-.31	-.44	-.59	-.70	-.54	-.38	-.22	-.07	.07
	15.0	-.03	-.13	-.23	-.36	-.48	-.60	-.70	-.56	-.40	-.25	-.11	.01
	20.0	-.10	-.16	-.29	-.41	-.53	-.63	-.65	-.54	-.37	-.24	-.11	.01
	30.0	-.15	-.23	-.33	-.43	-.55	-.66	-.61	-.49	-.34	-.22	-.11	-.02
	40.0	-.16	-.23	-.31	-.42	-.53	-.65	-.57	-.41	-.29	-.19	-.09	-.01
	50.0	-.16	-.22	-.31	-.42	-.53	-.61	-.49	-.31	-.20	-.14	-.06	0
	60.0	-.16	-.21	-.29	-.40	-.49	-.59	-.29	-.19	-.13	-.07	-.02	.03
	70.0	-.18	-.21	-.26	-.36	-.49	-.62	-.15	-.10	-.04	-.01	-.02	.07
	80.0	-.14	-.17	-.21	-.25	-.32	-.43	-	-	-	-	-	-
0.19 b/2	0	-.02	-.02	-.03	-.03	-.04	-.06	-.01	-.01	-.03	-.04	-.03	-.06
	1.5	.06	.05	.06	.05	.03	.01	-.04	-.05	-.05	-.05	-.05	.04
	4.0	.21	.19	.15	.01	-.22	-.46	-.69	-.10	-.90	-.51	-.20	.03
	7.0	.13	.03	-.12	-.31	-.51	-.70	-	-	-	-	-	-
	10.0	-.05	-.07	-.23	-.41	-.60	-.78	-.10	-.02	-.52	-.29	-.10	.06
	15.0	-.04	-.16	-.30	-.49	-.67	-.88	-.10	-.01	-.75	-.49	-.29	.14
	20.0	-.10	-.22	-.35	-.52	-.68	-.86	-.81	-.29	-.44	-.27	-.14	-.03
	30.0	-.19	-.28	-.40	-.53	-.73	-.89	-.65	-.44	-.34	-.23	-.12	-.03
	40.0	-.23	-.31	-.42	-.53	-.71	-.87	-.49	-.28	-.20	-.16	-.09	-.01
	50.0	-.21	-.29	-.38	-.52	-.70	-.86	-	-	-	-	-	-
	60.0	-.20	-.24	-.33	-.47	-.66	-.81	-.12	-.10	-.07	-.03	-.02	.03
	70.0	-.19	-.21	-.24	-.24	-.35	-.34	-.04	-.07	0	-.04	-.03	-.03
	80.0	-.14	-.14	-.16	-.18	-.18	-.12	-	-	-	-	-	-
0.31 b/2	0	0	0	0	0	0	0	0.02	0.02	0.02	0.02	0.02	0.02
	1.5	.10	.26	.46	.58	.60	.55	-	-	-	-	-	-
	4.0	.29	.44	.28	.05	-.22	-.49	-.87	-.69	-.35	.02	.28	.45
	7.0	.12	.02	-.17	-.41	-.65	-.87	-.10	-.99	-.57	-.19	.07	.25
	10.0	-.03	-.06	-.23	-.46	-.71	-.89	-.10	-.04	-.97	-.54	-.27	.08
	15.0	-.06	-.18	-.36	-.59	-.79	-.99	-.10	-.02	-.93	-.49	-.28	.11
	20.0	-.13	-.23	-.40	-.63	-.83	-.94	-.10	-.05	-.85	-.42	-.23	.10
	30.0	-.20	-.29	-.43	-.64	-.89	-.98	-.76	-.32	-.24	-.16	-.09	0
	40.0	-.21	-.29	-.41	-.59	-.85	-.96	-.59	-.24	-.18	-.13	-.05	.01
	50.0	-.22	-.26	-.36	-.51	-.81	-.90	-.31	-.14	-.09	-.03	-.02	.03
	60.0	-.20	-.23	-.30	-.50	-.70	-.82	-.22	-.10	-.05	-.02	-.01	-
	70.0	-.19	-.20	-.24	-.28	-.35	-.32	-.01	0	-.03	-.05	-.08	-.10
	80.0	-.13	-.14	-.16	-.18	-.14	-.18	-	-	-	-	-	-
0.375 b/2	0	-.01	-.01	-.02	0	-.01	-.03	-.07	0.08	-.09	-.10	-.10	-.11
	1.5	.05	.23	.45	.59	.60	.52	-	-	-	-	-	-
	4.0	.31	.34	.23	.04	-.36	-.70	-.92	-.54	-.34	.05	.29	.46
	7.0	.17	.06	-.18	-.44	-.68	-.89	-.94	-.63	-.58	-.18	.08	.25
	10.0	-.07	-.15	-.27	-.53	-.74	-.93	-.94	-.74	-.53	-.25	-.05	.33
	15.0	-.03	-.25	-.37	-.62	-.83	-.93	-.83	-.67	-.48	-.26	-.10	.38
	20.0	-.11	-.32	-.42	-.65	-.90	-.98	-.73	-.46	-.41	-.22	-.09	.38
	30.0	-.16	-.33	-.41	-.63	-.85	-.93	-.65	-.30	-.25	-.16	-.08	.01
	40.0	-.20	-.36	-.44	-.68	-.90	-.96	-.55	-.20	-.17	-.12	-.04	.08
	50.0	-.20	-.31	-.36	-.42	-.61	-.81	-.40	-	-	-	-	-
	60.0	-.19	-.26	-.30	-.33	-.59	-.70	-.34	-.05	0	-.04	-.05	.07
	70.0	-.18	-.23	-.29	-.30	-.50	-.62	-.20	-.01	-.02	-.04	-.06	.10
	80.0	-.14	-.18	-.19	-.20	-.49	-.63	-.01	-.08	-.09	-.09	-.11	-.11
0.44 b/2	0	-.03	-.01	-.02	0	-.07	-.07	-.06	-.06	-.11	-.11	-.11	-.01
	1.5	.04	.23	.45	.58	.59	.53	-	-	-	-	-	-
	4.0	.32	.11	0	-.28	-.54	-.88	-.88	-.57	-.34	-.07	.34	.49
	7.0	.17	-.05	-.17	-.45	-.70	-.89	-	-	-	-	-	-
	10.0	-.07	-.15	-.27	-.53	-.80	-.98	-.70	-.74	-.53	-.24	-.04	.10
	15.0	-.03	-.25	-.35	-.64	-.88	-.98	-.64	-.68	-.47	-.24	-.09	.04
	20.0	-.09	-.31	-.40	-.67	-.92	-.98	-.57	-.45	-.40	-.21	-.08	.03
	30.0	-.18	-.35	-.43	-.63	-.89	-.92	-.48	-.37	-.29	-.17	-.07	.01
	40.0	-.19	-.34	-.41	-.56	-.89	-.97	-.39	-.22	-.16	-.12	-.04	.04
	50.0	-.20	-.32	-.37	-.49	-.67	-.88	-.33	-.11	-.09	-.03	0	.04
	60.0	-.20	-.28	-.32	-.33	-.59	-.79	-.25	-.05	-.04	0	.04	.07
	70.0	-.20	-.21	-.25	-.29	-.43	-.68	-.19	-.02	-.03	-.06	-.09	.10
	80.0	-.17	-.13	-.15	-.15	-.33	-.46	-	-	-	-	-	-
	90.0	-.10	-.01	-.01	-.01	-.01	-.01	-.09	-.09	-.09	-.09	-.09	.06
	95.0	-.05	.08	.08	.07	.06	.06	-.06	-.11	-.11	-.11	-.09	.01

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TABLE XV. - PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING.
 $M_\infty = 0.86$; $R = 2,000,000$ - Continued
(a) α_u , $-4^\circ, -2^\circ, 0^\circ, 2^\circ, 4^\circ, 6^\circ$ - Concluded

Spanwise station	Per-cent chord	Upper surface						Lower surface					
		Angle of attack					Angle of attack	Angle of attack					Angle of attack
		4°	-2°	0°	2°	4°		4°	-2°	0°	2°	4°	
0.56 b/2	0	0.05	0.32	0.45	0.36	0.57	0.47	-	-	-	-	-	-
	1.5	.53	.46	.27	-.01	-.34	-.66	-0.90	-0.71	-0.47	0.03	0.32	0.47
	4.0	.34	.23	.03	-.23	-.32	-.83	-0.90	-.68	-.61	-.17	.10	.27
	7.0	.18	-.03	-.14	-.43	-.67	-.90	-	-	-	-	-	-
	10.0	.08	-.14	-.25	-.34	-.74	-.96	-0.85	-.78	-.53	-.25	-.04	.10
	15.0	-.03	-.23	-.34	-.65	-.91	-.107	-0.79	-.71	-.45	-.41	-.20	.04
	20.0	-.08	-.26	-.35	-.61	-.94	-.108	-0.71	-.55	-.29	-.23	-.06	.03
	30.0	-.15	-.30	-.39	-.58	-.93	-.105	-0.64	-.55	-.18	-.14	-.10	-.01
	40.0	-.20	-.31	-.37	-.51	-.89	-.102	-0.55	-.41	-.11	-.09	-.03	.01
	50.0	-.22	-.31	-.35	-.43	-.47	-.79	-	-	-	-	-	.02
	60.0	-.20	-.26	-.30	-.33	-.29	-.39	-	-	-	-	-	-
	70.0	-.21	-.22	-.24	-.25	-.24	-.25	-0.03	.02	.02	.06	.08	.06
0.68 b/2	0	-.19	-.14	-.15	-.16	-.15	-.19	-0.02	.07	.08	.08	.11	.08
	1.5	-.07	-.01	-.01	0	0	-.03	-.03	.11	.11	.10	.11	.08
	4.0	-.02	-.08	-.09	.09	.07	.06	-.08	.13	.13	.11	.11	.10
	7.0	-.19	-.14	-.15	-.16	-.15	-.19	-	-	-	-	-	-
	10.0	-.11	-.01	-.20	-.31	-.79	-.99	-.55	-.102	-.99	-.25	-.04	.09
	15.0	-.02	-.08	-.23	-.33	-.88	-.94	-.55	-.73	-.50	-.24	-.08	.03
	20.0	-.05	-.14	-.32	-.34	-.92	-.93	-.48	-.55	-.30	-.20	-.06	.02
	30.0	-.15	-.23	-.39	-.64	-.90	-.79	-.44	-.40	-.23	-.15	-.05	.01
	40.0	-.19	-.24	-.35	-.56	-.88	-.68	-.35	-.29	-.14	-.09	-.02	.02
	50.0	-.20	-.25	-.32	-.34	-.35	-.51	-	-	-	-	-	-
	60.0	-.18	-.20	-.26	-.26	-.26	-.42	-0.24	-.10	-.01	.02	.04	.03
	70.0	-.19	-.17	-.19	-.22	-.17	-.31	-.22	-.02	.04	.05	.07	.06
0.80 b/2	0	-.19	-.14	-.14	-.15	-.09	-.29	-.16	.06	.09	.09	.09	.06
	1.5	-.12	0	-.02	-.02	-.02	-.19	-.13	-.13	.08	.11	.10	.09
	4.0	-.09	-.06	-.05	-.10	-.09	-.06	-.11	.11	.13	.12	.07	-.04
	7.0	-.10	-.16	-.28	-.35	-.51	-.77	-.100	-.71	-.14	-.24	-.17	-.06
	10.0	-.15	-.19	-.28	-.42	-.68	-.85	-.05	-.05	-.05	-.05	-.05	-.01
	15.0	-.03	-.11	-.26	-.31	-.51	-.77	-.100	-.71	-.14	-.24	-.17	-.06
	20.0	-.03	-.11	-.26	-.31	-.51	-.68	-.100	-.74	-.14	-.26	-.22	-.07
	30.0	-.10	-.16	-.28	-.35	-.51	-.77	-.100	-.71	-.14	-.24	-.17	-.06
	40.0	-.15	-.19	-.28	-.42	-.68	-.85	-.05	-.05	-.05	-.05	-.05	-.01
	50.0	-.20	-.21	-.28	-.40	-.68	-.88	-.05	-.05	-.05	-.05	-.05	-.01
	60.0	-.19	-.19	-.24	-.35	-.50	-.76	-.05	-.05	-.05	-.05	-.05	-.01
	70.0	-.18	-.16	-.21	-.39	-.50	-.70	-.05	-.05	-.05	-.05	-.05	-.01
0.94 b/2	0	-.03	-.16	-.13	-.13	-.03	-.13	-.11	-.05	-.07	.05	.12	.10
	1.5	.02	.06	.24	.50	.61	.57	-	-	-	-	-	-
	4.0	.54	.51	.41	.16	-.19	-.51	-.38	-.59	-.107	-.43	-.10	.34
	7.0	.39	.35	.21	-.05	-.40	-.66	-	-	-	-	-	-
	10.0	.16	.10	-.03	-.26	-.63	-.92	-.38	-.49	-.85	-.38	-.13	.01
	15.0	-.06	.01	-.11	-.33	-.62	-.90	-.30	-.50	-.18	-.34	-.14	-.03
	20.0	-.01	-.06	-.18	-.38	-.63	-.81	-.27	-.43	-.35	-.28	-.13	-.03
	30.0	-.12	-.15	-.24	-.40	-.56	-.81	-.25	-.39	-.27	-.18	-.10	-.04
	40.0	-.16	-.19	-.24	-.37	-.49	-.59	-.20	-.49	-.13	-.10	-.08	-.04
	50.0	-.23	-.21	-.24	-.32	-.29	-.32	-.20	-.25	-.05	-.03	-.04	-.02
	60.0	-.23	-.19	-.20	-.26	-.19	-.21	-	-	-	-	-	-
	70.0	-.24	-.17	-.16	-.15	-.15	-.11	-.16	-.13	.07	.07	.07	.04
	80.0	-.24	-.13	-.12	-.07	-.07	-.05	-.14	-.06	.12	.11	.10	.07
	90.0	-.17	-.03	.07	.05	.06	.03	-.16	-.03	.14	.13	.11	.07
	95.0	-.15	.01	.12	.08	.12	.06	-.13	.01	.17	.15	.14	.07

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TABLE XV.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING.
 $M_\infty = 0.86$; $R = 2,000,000$ - Continued
 (b) $\alpha_u = 8^\circ, 10^\circ, 12^\circ, 14^\circ$

Spanwise station	Percent chord	Upper surface				Lower surface			
		Angle of attack				Angle of attack			
		8°	10°	12°	14°	8°	10°	12°	14°
0.10 b/a	0	0.63	0.57	0.49	-	-	-	-	-
	1.5	-0.48	-0.70	-0.92	-	-	-	-	-
	4.0	-0.64	-0.80	-0.99	-	-	-	-	-
	7.0	-0.79	-0.93	-1.11	-	-	-	-	-
	10.0	-0.79	-0.94	-1.09	-	-	-	-	-
	15.0	-0.73	-0.92	-1.07	-	-	-	-	-
	20.0	-0.73	-0.87	-1.05	-	-	-	-	-
	30.0	-0.79	-0.87	-0.93	-	-	-	-	-
	40.0	-0.74	-0.80	-0.89	-	-	-	-	-
	50.0	-0.69	-0.79	-0.84	-	-	-	-	-
	60.0	-0.69	-0.76	-0.82	-	-	-	-	-
	70.0	-0.73	-0.66	-0.84	-	-	-	-	-
	80.0	-0.72	-0.23	-0.25	-	-	-	-	-
	90.0	-0.18	-0.30	-0.35	-	-	-	-	-
	95.0	-0.15	-0.24	-0.30	-	-	-	-	-
0.19 b/2	0	-0.49	-0.37	-0.24	-	-	-	-	-
	1.5	-0.70	-0.86	-1.00	-	-	-	-	-
	4.0	-0.92	-1.13	-1.27	-	-	-	-	-
	7.0	-0.94	-1.13	-1.30	-	-	-	-	-
	10.0	-0.98	-1.14	-1.31	-	-	-	-	-
	15.0	-1.08	-1.21	-1.34	-	-	-	-	-
	20.0	-1.06	-1.21	-1.30	-	-	-	-	-
	30.0	-1.05	-1.19	-1.28	-	-	-	-	-
	40.0	-1.03	-1.19	-1.13	-	-	-	-	-
	50.0	-1.01	-1.08	-1.01	-	-	-	-	-
	60.0	-0.91	-0.86	-0.93	-	-	-	-	-
	70.0	-0.89	-0.44	-0.82	-	-	-	-	-
	80.0	-0.11	-0.23	-0.66	-	-	-	-	-
	90.0	-0.05	-0.15	-0.55	-	-	-	-	-
	95.0	-0.05	-0.18	-0.48	-	-	-	-	-
0.31 b/2	0	.44	.31	.19	-	-	-	-	-
	1.5	-0.72	-0.88	-1.01	-	-	-	-	-
	4.0	-1.00	-1.16	-1.15	-	-	-	-	-
	7.0	-1.10	-1.19	-1.13	-	-	-	-	-
	10.0	-1.13	-1.20	-1.13	-	-	-	-	-
	15.0	-1.19	-1.20	-1.04	-	-	-	-	-
	20.0	-1.39	-1.14	-0.98	-	-	-	-	-
	30.0	-1.15	-0.98	-0.87	-	-	-	-	-
	40.0	-1.05	-0.90	-0.82	-	-	-	-	-
	50.0	-0.94	-0.83	-0.75	-	-	-	-	-
	60.0	-0.71	-0.74	-0.71	-	-	-	-	-
	70.0	-0.59	-0.63	-0.63	-	-	-	-	-
	80.0	-0.47	-0.55	-0.61	-	-	-	-	-
	90.0	-0.31	-0.42	-0.50	-	-	-	-	-
	95.0	-0.23	-0.42	-0.51	-	-	-	-	-
0.375 b/2	0	.41	.29	.15	.15	-	-	-	-
	1.5	-0.92	-1.04	-0.80	-0.67	-	-	-	-
	4.0	-1.01	-1.02	-0.80	-0.67	-	-	-	-
	7.0	-1.07	-1.00	-0.77	-0.65	-	-	-	-
	10.0	-1.11	-0.94	-0.74	-0.65	-	-	-	-
	15.0	-1.08	-0.85	-0.76	-0.64	-	-	-	-
	20.0	-1.09	-0.80	-0.69	-0.64	-	-	-	-
	30.0	-0.94	-0.75	-0.67	-0.64	-	-	-	-
	40.0	-0.83	-0.72	-0.66	-0.67	-	-	-	-
	50.0	-0.76	-0.68	-0.66	-0.68	-	-	-	-
	60.0	-0.70	-0.64	-0.66	-0.68	-	-	-	-
	70.0	-0.62	-0.58	-0.62	-0.65	-	-	-	-
	80.0	-0.53	-0.51	-0.59	-0.62	-	-	-	-
	90.0	-0.44	-0.42	-0.53	-0.57	-	-	-	-
	95.0	-0.33	-0.38	-0.50	-0.56	-	-	-	-
0.44 b/2	0	.41	.30	.21	.11	-	-	-	-
	1.5	-0.88	-0.96	-0.67	-0.60	-	-	-	-
	4.0	-1.04	-0.97	-0.67	-0.60	-	-	-	-
	7.0	-0.99	-0.95	-0.66	-0.60	-	-	-	-
	10.0	-1.00	-0.94	-0.65	-0.60	-	-	-	-
	15.0	-1.00	-0.84	-0.63	-0.60	-	-	-	-
	20.0	-0.89	-0.80	-0.61	-0.60	-	-	-	-
	30.0	-0.74	-0.73	-0.60	-0.59	-	-	-	-
	40.0	-0.67	-0.68	-0.59	-0.59	-	-	-	-
	50.0	-0.60	-0.61	-0.59	-0.59	-	-	-	-
	60.0	-0.57	-0.55	-0.57	-0.59	-	-	-	-
	70.0	-0.51	-0.48	-0.53	-0.58	-	-	-	-
	80.0	-0.48	-0.43	-0.53	-0.56	-	-	-	-
	90.0	-0.48	-0.38	-0.49	-0.53	-	-	-	-
	95.0	-0.39	-0.35	-0.46	-0.50	-	-	-	-

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TABLE XV.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING.
 $M_\infty = 0.86$; $R = 2,000,000$ - Concluded
 (b) α_u , $8^\circ, 10^\circ, 12^\circ, 14^\circ$ - Concluded

Spanwise station	Percent chord	Upper surface				Lower surface			
		Angle of attack				Angle of attack			
		8°	10°	12°	14°	8°	10°	12°	14°
0.56 b/2	0	0.36	0.25	0.13	0	-	-	-	-
	1.5	-0.84	-0.95	-1.04	-1.13	-	-	-	-
	4.0	-1.05	-1.19	-1.28	-1.34	-0.53	0.57	0.58	0.59
	7.0	-1.10	-1.23	-1.32	-1.38	-0.34	0.40	0.44	0.49
	10.0	-1.14	-1.26	-1.29	-1.29	-	-	-	-
	15.0	-1.19	-1.29	-1.29	-1.29	-0.15	0.22	0.27	0.31
	20.0	-1.17	-1.26	-1.27	-1.25	-0.06	0.11	0.15	0.19
	30.0	-1.02	-1.18	-1.19	-1.13	0.01	0.06	0.07	0.11
	40.0	-0.74	-1.00	-0.66	-0.58	0.01	0.04	0.04	0.07
	50.0	-0.60	-0.79	-0.78	-0.74	0	0.02	0.02	0.03
	60.0	-0.50	-0.77	-0.49	-0.53	-	-	-	-
	70.0	-0.38	-0.72	-0.41	-0.45	-0.01	0.04	0	0
	80.0	-0.28	-0.79	-0.38	-0.41	-0.03	0.04	-0.02	-0.04
	90.0	-0.13	-0.77	-0.33	-0.38	0.01	0	-0.09	-0.12
	95.0	-0.08	-0.78	-0.29	-0.36	0	0	-0.13	-0.17
0.68 b/2	0	-	-	-	-	-	-	-	-
	1.5	-0.71	-0.88	-1.00	-1.06	-0.50	0.56	0.56	0.57
	4.0	-1.04	-0.99	-1.08	-1.08	-0.31	0.42	0.43	0.47
	7.0	-1.12	-0.91	-0.99	-1.00	-	-	-	-
	10.0	-1.08	-0.93	-1.00	-1.01	-0.15	0.23	0.23	0.31
	15.0	-1.04	-0.87	-0.99	-0.98	-0.07	0.15	0.17	0.21
	20.0	-1.04	-0.81	-0.93	-0.93	-0.05	0.11	0.13	0.17
	30.0	-0.73	-0.70	-0.81	-0.82	0.01	0.07	0.07	0.10
	40.0	-0.72	-0.65	-0.73	-0.76	0.08	0.06	0.05	0.06
	50.0	-0.73	-0.58	-0.65	-0.70	-	-	-	-
	60.0	-0.62	-0.54	-0.61	-0.68	-0.01	0.03	0.03	0.04
	70.0	-0.48	-0.46	-0.54	-0.63	-0.05	0.03	0.01	0.02
	80.0	-0.37	-0.44	-0.52	-0.60	-0.05	0.01	-0.01	-0.03
	90.0	-0.25	-0.36	-0.43	-0.49	-0.01	0.08	-0.10	-0.12
	95.0	-0.24	-0.36	-0.43	-0.50	-0.07	0.17	-0.19	-0.23
0.80 b/2	0	-0.33	-0.23	-0.13	0	-	-	-	-
	1.5	-0.84	-0.98	-1.10	-1.09	-0.49	0.54	0.57	0.58
	4.0	-1.00	-1.14	-1.18	-1.14	-0.29	0.36	0.41	0.45
	7.0	-1.07	-1.19	-1.09	-1.03	-	-	-	-
	10.0	-1.12	-1.13	-1.13	-1.03	-0.13	0.20	0.25	0.29
	15.0	-1.16	-1.13	-0.99	-1.00	-0.06	0.12	0.16	0.20
	20.0	-1.12	-1.14	-0.94	-0.98	-0.03	0.11	0.13	0.17
	30.0	-1.08	-0.95	-0.84	-0.92	0.01	0.05	0.07	0.09
	40.0	-0.89	-0.84	-0.83	-0.98	-	-	-	-
	50.0	-0.70	-0.74	-0.76	-0.83	-0.02	0.03	0.02	0.03
	60.0	-0.57	-0.66	-0.71	-0.79	0.04	0.03	0.02	0.03
	70.0	-0.47	-0.58	-0.64	-0.73	0.06	0.08	0.02	0.01
	80.0	-0.34	-0.46	-0.59	-0.68	0.07	0.03	-0.01	-0.04
	90.0	-0.23	-0.35	-0.51	-0.59	0.06	0.02	-0.09	-0.12
	95.0	-0.14	-0.26	-0.48	-0.55	0.03	-0.03	-0.15	-0.19
0.94 b/2	0	-0.47	-0.38	-0.27	-0.16	-	-	-	-
	1.5	-0.79	-1.03	-1.19	-1.06	-0.43	0.50	0.53	0.55
	4.0	-0.89	-1.06	-1.17	-1.09	-	0.25	0.28	0.33
	7.0	-1.00	-1.08	-1.09	-1.04	-0.17	0.15	0.19	0.24
	10.0	-1.05	-1.06	-1.10	-0.99	-0.09	0.10	0.11	0.16
	15.0	-0.97	-1.01	-1.05	-0.88	-0.03	0.10	0.07	0.11
	20.0	-0.97	-1.01	-1.00	-0.86	-0.01	0.06	0.07	0.11
	30.0	-0.81	-0.78	-0.83	-0.79	-0.03	0	0.01	0.04
	40.0	-0.64	-0.70	-0.78	-0.75	-0.04	-0.02	-0.04	-0.02
	50.0	-0.51	-0.59	-0.68	-0.70	-0.03	-0.02	-0.04	-0.04
	60.0	-0.41	-0.53	-0.61	-0.68	-	-	-	-
	70.0	-0.31	-0.44	-0.53	-0.61	-0.01	0	-0.04	-0.09
	80.0	-0.23	-0.36	-0.47	-0.57	0.04	0.01	-0.04	-0.10
	90.0	-0.13	-0.27	-0.37	-0.51	0.02	-0.03	-0.08	-0.17
	95.0	-0.09	-0.22	-0.34	-0.47	0	-0.08	-0.15	-0.25


 NACA

TABLE XVI.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING.

 $M_\infty = 0.90; R = 2,000,000$ (a) $\alpha_u = -4^\circ, -2^\circ, 0^\circ, 2^\circ, 4^\circ, 6^\circ$

Spanwise stations	Percent chord	Upper surface						Lower surface						
		Angle of attack						Angle of attack						
		-4°	-2°	0°	2°	4°	6°	-4°	-2°	0°	2°	4°	6°	
0.10 b/2	0	0.29	0.43	0.55	0.63	0.68	0.70	---	-0.54	-0.38	-0.13	0.08	0.26	0.42
	1.5	.49	.40	.28	.15	-.01	-.18	---	-.54	-.38	-.31	-.11	.06	.21
	4.0	.29	.18	.06	-.07	-.23	-.39	---	-.74	-.58	-.31	---	---	---
	7.0	.15	.05	-.08	-.21	-.37	-.52	---	---	---	---	---	---	---
	10.0	.07	-.04	-.14	-.26	-.40	-.54	---	-.66	-.51	-.37	-.22	-.08	.06
	15.0	-.01	-.12	-.22	-.32	-.44	-.55	---	-.67	-.54	-.39	-.24	-.11	.01
	20.0	-.08	-.18	-.28	-.38	-.49	-.57	---	-.64	-.52	-.37	-.23	-.11	.01
	30.0	-.14	-.22	-.32	-.42	-.53	-.61	---	-.60	-.49	-.35	-.23	-.13	-.03
	40.0	-.15	-.24	-.32	-.40	-.51	-.59	---	-.57	-.46	-.34	-.20	-.10	-.03
	50.0	-.16	-.23	-.33	-.42	-.51	-.60	---	-.52	-.40	-.26	-.15	-.10	-.01
	60.0	-.16	-.23	-.32	-.41	-.51	-.55	---	-.50	-.30	-.14	-.06	-.04	.01
	70.0	-.18	-.24	-.33	-.44	-.54	-.61	---	-.52	-.32	-.13	-.06	-.02	.05
	80.0	-.15	-.19	-.27	-.40	-.58	-.68	---	---	---	---	---	---	---
	90.0	-.03	-.03	-.02	-.03	-.09	-.19	---	-.01	-.01	.08	-.03	.02	.02
	95.0	.06	.06	.06	.04	-.05	-.14	---	.06	.05	.05	.03	.01	-.01
0.19 b/2	0	.19	.34	.48	.60	.62	.60	---	-.80	-.58	-.29	0	.24	.11
	1.5	.50	.40	.28	.08	-.13	-.34	---	-.80	-.58	-.29	-.21	.01	.19
	4.0	.26	.14	0	-.11	-.19	-.38	---	-.98	-.84	-.49	---	---	---
	7.0	.15	.03	-.11	-.27	-.45	-.62	---	---	---	---	---	---	---
	10.0	.06	-.07	-.21	-.38	-.55	-.68	---	-.103	-.79	-.54	-.29	-.11	.03
	15.0	-.05	-.17	-.30	-.45	-.63	-.80	---	-.97	-.76	-.53	-.31	-.16	-.03
	20.0	-.11	-.23	-.35	-.50	-.64	-.79	---	-.95	-.71	-.50	-.29	-.16	-.04
	30.0	-.18	-.29	-.41	-.54	-.72	-.84	---	-.72	-.54	-.43	-.24	-.14	-.05
	40.0	-.23	-.33	-.44	-.56	-.69	-.81	---	-.68	-.50	-.22	-.19	-.10	-.03
	50.0	-.23	-.31	-.44	-.57	-.70	-.80	---	---	---	---	---	---	---
	60.0	-.21	-.26	-.40	-.54	-.69	-.76	---	-.17	-.10	-.06	-.04	.01	.02
	70.0	-.19	-.22	-.28	-.49	-.66	-.76	---	-.04	-.02	-.01	-.03	.04	.06
	80.0	-.13	-.15	-.15	-.13	-.18	-.19	---	---	---	---	---	---	---
	90.0	-.01	0	-.01	-.01	-.01	-.04	---	-.07	-.07	.09	-.09	.08	.05
	95.0	.07	.07	.07	.06	-.07	-.14	---	.09	.09	.10	.09	.09	.02
0.31 b/2	0	.15	.30	.46	.58	.61	.58	---	-.78	-.82	-.36	0	.29	.11
	1.5	.51	.42	.28	.09	-.14	-.37	---	-.103	-.91	-.60	-.22	-.03	.21
	4.0	.29	.16	.02	-.21	-.44	-.55	---	---	---	---	---	---	---
	7.0	.15	.01	-.15	-.34	-.59	-.74	---	---	---	---	---	---	---
	10.0	.08	-.06	-.29	-.42	-.65	-.79	---	-.109	-.98	-.65	-.31	-.10	.04
	15.0	-.06	-.20	-.36	-.55	-.73	-.89	---	-.110	-.98	-.57	-.31	-.14	-.02
	20.0	-.13	-.25	-.43	-.60	-.77	-.93	---	-.106	-.92	-.53	-.26	-.13	-.03
	30.0	-.20	-.30	-.48	-.65	-.85	-.99	---	-.103	-.73	-.24	-.20	-.10	-.03
	40.0	-.23	-.33	-.51	-.70	-.88	-.98	---	-.66	-.17	-.19	-.14	-.07	-.03
	50.0	-.22	-.29	-.40	-.64	-.85	-.95	---	-.44	-.12	-.11	-.04	-.04	.01
	60.0	-.20	-.27	-.27	-.54	-.83	-.76	---	---	---	---	---	---	---
	70.0	-.18	-.21	-.24	-.30	-.37	-.53	---	-.01	0	.02	.06	.07	.08
	80.0	-.13	-.14	-.17	-.13	-.09	-.36	---	---	---	---	---	---	---
	90.0	.01	.01	.01	.02	.04	-.19	---	.08	.08	.10	.11	.09	.08
	95.0	.09	.08	.06	.10	-.07	-.12	---	.11	.11	.11	.10	.09	.06
0.375 b/2	0	.10	.26	.44	.58	.62	.56	---	---	---	---	---	---	---
	1.5	.51	.41	.25	.02	-.26	-.55	---	-.87	-.65	-.33	.02	.27	.42
	4.0	.31	.20	.03	-.20	-.42	-.60	---	-.105	-.90	-.60	-.20	-.05	.21
	7.0	.16	.02	-.15	-.39	-.60	-.78	---	---	---	---	---	---	---
	10.0	.06	-.06	-.26	-.48	-.67	-.88	---	-.113	-.101	-.59	-.26	-.08	.04
	15.0	-.04	-.18	-.36	-.58	-.78	-.93	---	-.106	-.93	-.52	-.29	-.13	-.01
	20.0	-.13	-.24	-.44	-.63	-.84	-.98	---	-.104	-.93	-.47	-.24	-.12	-.02
	30.0	-.18	-.27	-.49	-.72	-.91	-.94	---	-.94	-.84	-.48	-.23	-.10	-.03
	40.0	-.22	-.34	-.53	-.72	-.94	-.95	---	-.75	-.20	-.17	-.13	-.03	-.01
	50.0	-.21	-.26	-.34	-.65	-.89	-.91	---	---	---	---	---	---	---
	60.0	-.20	-.24	-.30	-.58	-.84	-.99	---	-.07	-.07	-.03	.01	.05	.04
	70.0	-.20	-.22	-.27	-.53	-.78	-.90	---	-.06	0	.02	.06	.09	.08
	80.0	-.18	-.18	-.19	-.49	-.70	-.89	---	-.06	-.06	-.10	.11	.12	.08
	90.0	-.04	-.01	-.01	-.01	-.01	-.01	---	.08	.10	.12	.12	.14	.09
	95.0	.03	.07	.08	.08	-.08	-.07	---	.08	.10	.12	.12	.14	.09
0.44 b/2	0	.07	.26	.42	.59	.61	.57	---	-.85	-.69	-.32	.03	.31	.45
	1.5	.51	.42	.24	-.02	-.28	-.53	---	-.104	-.96	-.62	.22	.05	.21
	4.0	.31	.20	.04	-.23	-.46	-.64	---	---	---	---	---	---	---
	7.0	.16	.04	-.16	-.40	-.62	-.77	---	---	---	---	---	---	---
	10.0	.07	-.06	-.26	-.49	-.72	-.87	---	-.99	-.90	-.58	-.26	-.07	.06
	15.0	-.04	-.17	-.38	-.60	-.81	-.96	---	-.95	-.92	-.51	-.26	-.11	-.01
	20.0	-.11	-.23	-.44	-.65	-.85	-.91	---	-.83	-.80	-.46	-.23	-.09	-.01
	30.0	-.19	-.29	-.41	-.73	-.92	-.99	---	-.68	-.44	-.24	-.17	-.06	-.02
	40.0	-.20	-.29	-.41	-.70	-.87	-.98	---	-.61	-.28	-.18	-.13	-.03	-.02
	50.0	-.22	-.29	-.42	-.64	-.84	-.97	---	-.57	-.18	-.09	-.02	-.02	.03
	60.0	-.22	-.28	-.34	-.55	-.62	-.68	---	-.48	-.10	-.03	.01	.05	.03
	70.0	-.20	-.20	-.23	-.40	-.43	-.57	---	-.35	-.03	.04	.06	.09	.09
	80.0	-.15	-.14	-.13	-.14	-.26	-.49	---	-.01	0	.04	.06	.09	.09
	90.0	-.01	0	.01	.01	-.11	-.37	---	.01	-.07	.10	.10	.09	.09
	95.0	.06	.08	.10	.09	-.01	-.29	---	.06	.10	.12	.12	.09	-.01

NACA

TABLE XVI.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING
 $M_\infty = 0.90$; $R = 2,000,000$ - Continued
(a) $\alpha_u = -4^\circ, -2^\circ, 0^\circ, 2^\circ, 4^\circ, 6^\circ$ - Concluded

Spanwise stations	Percent chord	Upper surface						Lower surface					
		Angle of attack						Angle of attack					
		-4°	-2°	0°	2°	4°	6°	-4°	-2°	0°	2°	4°	6°
0.56 b/2	0	0.09	0.26	0.46	0.59	0.60	0.52	---	---	---	---	---	---
	1.5	.35	.16	.30	.02	-.25	-.52	-0.65	-0.78	-0.45	0.01	0.30	0.43
	4.0	.34	.22	.05	-.21	-.46	-.89	-.63	-.95	-.63	-.19	-.08	.22
	7.0	.18	.06	-.14	-.39	-.59	-.79	---	---	---	---	---	---
	10.0	.08	-.03	-.23	-.49	-.67	-.83	-.60	-.87	-.58	-.28	-.06	0
	15.0	-.03	-.15	-.36	-.64	-.85	-.96	-.56	-.84	-.50	-.27	-.08	0
	20.0	-.08	-.19	-.38	-.67	-.88	-.99	-.54	-.88	-.48	-.22	-.06	0
	30.0	-.17	-.26	-.40	-.68	-.95	-.99	-.50	-.93	-.23	-.16	-.08	-.03
	40.0	-.21	-.27	-.38	-.62	-.89	-.99	-.45	-.86	-.14	-.10	-.04	-.01
	50.0	-.23	-.28	-.36	-.55	-.82	-.99	-.43	-.83	-.08	-.02	-.01	-.01
	60.0	-.23	-.23	-.30	-.25	-.59	-.63	---	---	---	---	---	---
	70.0	-.26	-.21	-.24	-.24	-.32	-.36	-.34	-.03	-.04	.06	.07	.03
	80.0	-.29	-.13	-.14	-.14	-.13	-.14	-.29	-.02	-.06	.10	.11	.07
	90.0	-.22	-.02	-.01	0	-.03	-.03	-.24	-.01	-.11	.11	.11	.07
	95.0	-.18	-.03	.10	.08	.07	.08	-.21	.09	.14	.14	.14	.11
0.68 b/2	0	---	---	---	---	---	---	---	---	---	---	---	---
	1.5	.75	.51	.35	.08	-.18	-.40	-.46	-.90	-.51	-.03	.26	.40
	4.0	.38	.33	.07	-.25	-.50	-.72	-.50	-.1.03	-.70	-.21	.05	.19
	7.0	.19	.18	.10	-.40	-.64	-.83	---	---	---	---	---	---
	10.0	.09	0	-.20	-.32	-.74	-.89	-.37	-.1.00	-.64	-.27	-.06	.05
	15.0	0	-.09	-.27	-.39	-.81	-.86	-.38	-.76	-.57	-.26	-.10	-.01
	20.0	-.09	-.17	-.32	-.63	-.86	-.85	-.34	-.58	-.35	-.21	-.08	-.01
	30.0	-.20	-.26	-.44	-.70	-.84	-.72	-.32	-.42	-.25	-.15	-.07	-.03
	40.0	-.24	-.26	-.40	-.55	-.89	-.77	-.27	-.29	-.14	-.09	---	0
	50.0	-.26	-.27	-.36	-.48	-.84	-.78	---	---	---	---	---	---
	60.0	-.27	-.22	-.26	-.20	-.32	-.42	---	-.23	-.13	-.01	.02	0
	70.0	-.30	-.19	-.19	-.20	-.20	-.34	-.22	-.04	.05	.03	.06	.03
	80.0	-.32	-.13	-.13	-.13	-.13	-.29	-.18	-.02	.08	.15	.07	.02
	90.0	-.22	0	-.02	-.03	-.03	-.24	-.17	-.08	.12	.11	.04	-.04
	95.0	-.19	.06	.10	.18	.05	.24	-.13	.09	.13	.12	.01	-.10
0.80 b/2	0	.20	.32	.51	.64	.63	.55	---	---	---	---	---	---
	1.5	.54	.38	.35	.12	-.18	-.44	-.90	-.88	-.67	-.11	.21	.37
	4.0	.35	.28	.14	-.04	-.33	-.60	-.54	-.93	-.80	-.38	.01	.16
	7.0	.21	.14	.13	-.13	-.42	-.67	-.85	-.72	-.70	-.31	---	---
	10.0	.11	-.03	-.13	-.23	-.32	-.76	-.93	-.74	-.61	-.28	-.12	-.04
	15.0	0	-.06	-.23	-.28	-.60	-.83	-.95	-.67	-.51	-.33	-.24	-.03
	20.0	-.08	-.13	-.28	-.60	-.83	-.95	-.51	-.70	-.41	-.23	-.09	-.04
	30.0	-.14	-.15	-.29	-.51	-.77	-.98	-.68	-.45	-.23	-.17	---	---
	40.0	-.21	-.21	-.29	-.45	-.77	-.98	---	---	---	---	---	---
	50.0	-.25	-.24	-.32	-.39	-.54	-.68	-.51	-.30	-.09	-.03	-.02	-.01
	60.0	-.24	-.21	-.27	-.38	-.32	-.50	-.35	-.21	-.02	.01	.02	.02
	70.0	-.23	-.18	-.22	-.18	-.18	-.35	-.13	-.13	.05	.06	.08	.03
	80.0	-.20	-.14	-.13	-.12	-.08	-.28	-.04	-.06	.08	.09	.09	.03
	90.0	-.06	-.03	-.01	.02	.02	-.07	-.05	-.01	.12	.11	.10	.10
	95.0	.02	-.03	.10	.10	.06	.01	.07	.03	.14	.13	.10	.10
0.94 b/2	0	-.02	.06	.27	.31	.61	.59	---	---	---	---	---	---
	1.5	.35	.21	.41	.17	-.14	-.39	-.49	-.61	-.99	-.43	.07	.28
	4.0	.40	.34	.21	-.05	-.35	-.54	---	---	---	---	---	---
	7.0	.29	.19	.06	-.21	-.54	-.70	-.47	-.29	-.95	-.41	-.10	.03
	10.0	.16	.09	.04	-.28	-.61	-.83	-.42	-.51	-.90	-.40	-.14	-.02
	15.0	.06	-.01	-.12	-.34	-.62	-.83	-.42	-.21	-.71	-.35	-.16	-.06
	20.0	-.01	-.08	.19	-.39	-.59	-.78	-.37	-.43	-.36	-.29	-.14	-.07
	30.0	-.12	-.15	.25	-.43	-.65	-.74	-.34	-.46	-.28	-.19	-.11	-.08
	40.0	-.18	-.20	.27	-.39	-.64	-.63	-.29	-.29	-.12	-.11	-.08	-.06
	50.0	-.23	-.20	.29	-.36	-.29	-.44	-.29	-.28	-.04	-.03	-.05	-.03
	60.0	-.24	-.23	.23	-.30	-.14	-.33	---	---	---	---	---	---
	70.0	-.24	-.18	-.19	-.08	-.06	-.21	-.23	-.15	.08	.08	.07	.02
	80.0	-.21	-.14	-.09	-.03	-.09	-.13	-.21	-.09	.12	.11	.07	0
	90.0	-.14	-.03	.08	.06	-.08	-.07	-.21	-.04	.15	.14	.12	.05
	95.0	-.14	.01	.13	.12	.13	-.08	-.17	0	.17	.16	.14	.03

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TABLE XVI.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING.
 $M_\infty = 0.90$; $R = 2,000,000$ - Continued

(b) $\alpha_u = 8^\circ, 10^\circ$

Spanwise stations	Percent chord	Upper surface				Lower surface			
		Angle of attack				Angle of attack			
		8°	10°	8°	10°	8°	10°	8°	10°
0.10 b/2	0	0.67	0.63						
	1.5	-0.35	-0.59						
	4.0	-0.34	-0.69						
	7.0	-0.69	-0.82						
	10.0	-0.69	-0.86						
	15.0	-0.67	-0.88						
	20.0	-0.57	-0.79						
	30.0	-0.70	-0.80						
	40.0	-0.68	-0.75						
	50.0	-0.62	-0.71						
	60.0	-0.64	-0.69						
	70.0	-0.67	-0.74						
	80.0	-0.73	-0.79						
	90.0	-0.89	-0.40						
	95.0	-0.24	-0.35						
0.19 b/2	0	.58	.42						
	1.5	-0.56	-0.74						
	4.0	-0.79	-0.99						
	7.0	-0.82	-1.00						
	10.0	-0.85	-1.02						
	15.0	-0.93	-1.09						
	20.0	-0.94	-1.10						
	30.0	-0.95	-1.10						
	40.0	-0.93	-1.10						
	50.0	-0.93	-1.08						
	60.0	-0.84	-0.89						
	70.0	-0.82	-0.75						
	80.0	-0.23	-0.30						
	90.0	-0.17	-0.27						
	95.0	-0.19	-0.30						
0.31 b/2	0	.50	.39						
	1.5	-0.27	-0.74						
	4.0	-0.88	-1.01						
	7.0	-0.94	-1.10						
	10.0	-0.97	-1.13						
	15.0	-1.04	-1.12						
	20.0	-1.04	-1.13						
	30.0	-1.05	-1.00						
	40.0	-1.04	-0.92						
	50.0	-0.88	-0.85						
	60.0	-0.73	-0.79						
	70.0	-0.58	-0.67						
	80.0	-0.49	-0.59						
	90.0	-0.40	-0.48						
	95.0	-0.34	-0.48						
0.375 b/2	0	.48	.37						
	1.5	-0.76	-0.90						
	4.0	-0.83	-1.01						
	7.0	-0.90	-0.97						
	10.0	-0.99	-0.95						
	15.0	-1.06	-0.95						
	20.0	-1.05	-0.89						
	30.0	-1.04	-0.79						
	40.0	-0.99	-0.77						
	50.0	-0.92	-0.75						
	60.0	-0.86	-0.70						
	70.0	-0.72	-0.68						
	80.0	-0.47	-0.55						
	90.0	-0.31	-0.48						
	95.0	-0.21	-0.43						
0.44 b/2	0	.48	.37						
	1.5	-0.72	-0.85						
	4.0	-0.86	-0.89						
	7.0	-0.94	-0.88						
	10.0	-1.00	-0.88						
	15.0	-1.01	-0.80						
	20.0	-1.01	-0.74						
	30.0	-0.93	-0.68						
	40.0	-0.83	-0.65						
	50.0	-0.71	-0.61						
	60.0	-0.63	-0.58						
	70.0	-0.58	-0.54						
	80.0	-0.30	-0.52						
	90.0	-0.14	-0.47						
	95.0	-0.11	-0.45						



TABLE XVI.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING.
 M_∞ , 0.90; R, 2,000,000 - Concluded
 (b) α_u , 8° , 10° - Concluded

Spanwise stations	Percent chord	Upper surface						Lower surface					
		Angle of attack						Angle of attack					
		8°	10°	8°	10°	8°	10°	8°	10°	8°	10°	8°	10°
0.56 b/2	0	0.42	0.31										
	1.5	-.68	-.82										
	4.0	-.88	-1.04										
	7.0	-.94	-1.09										
	10.0	-.100	-1.13										
	15.0	-.111	-1.18										
	20.0	-.111	-1.15										
	30.0	-.111	-1.11										
	40.0	-.105	-.93										
	50.0	-.94	-.74										
	60.0	-.90	-.52										
	70.0	-.35	-.44										
	80.0	-.23	-.34										
	90.0	-.11	-.25										
	95.0	-.04	-.20										
0.68 b/2	0	---	---										
	1.5	-.58	-.74										
	4.0	-.89	-1.01										
	7.0	-.99	-1.06										
	10.0	-.99	-1.04										
	15.0	-.94	-1.02										
	20.0	-.94	-1.03										
	30.0	-.77	-.85										
	40.0	-.66	-.76										
	50.0	-.60	-.74										
	60.0	-.53	-.64										
	70.0	-.44	-.53										
	80.0	-.40	-.47										
	90.0	-.33	-.38										
	95.0	-.33	-.39										
0.80 b/2	0	.44	.32										
	1.5	-.70	-.84										
	4.0	-.86	-1.01										
	7.0	-.93	-1.08										
	10.0	-.99	-1.11										
	15.0	-.106	-1.06										
	20.0	-.107	-1.07										
	30.0	-.103	-1.00										
	40.0	-.95	-.91										
	50.0	-.75	-.79										
	60.0	-.64	-.70										
	70.0	-.53	-.59										
	80.0	-.41	-.43										
	90.0	-.29	-.45										
	95.0	-.19	-.41										
0.94 b/2	0	.52	.42										
	1.5	-.63	-.89										
	4.0	-.75	-.92										
	7.0	-.87	-1.01										
	10.0	-.93	-.99										
	15.0	-.89	-.91										
	20.0	-.88	-.94										
	30.0	-.75	-.78										
	40.0	-.63	-.72										
	50.0	-.54	-.62										
	60.0	-.46	-.58										
	70.0	-.38	-.49										
	80.0	-.30	-.43										
	90.0	-.23	-.35										
	95.0	-.19	-.31										

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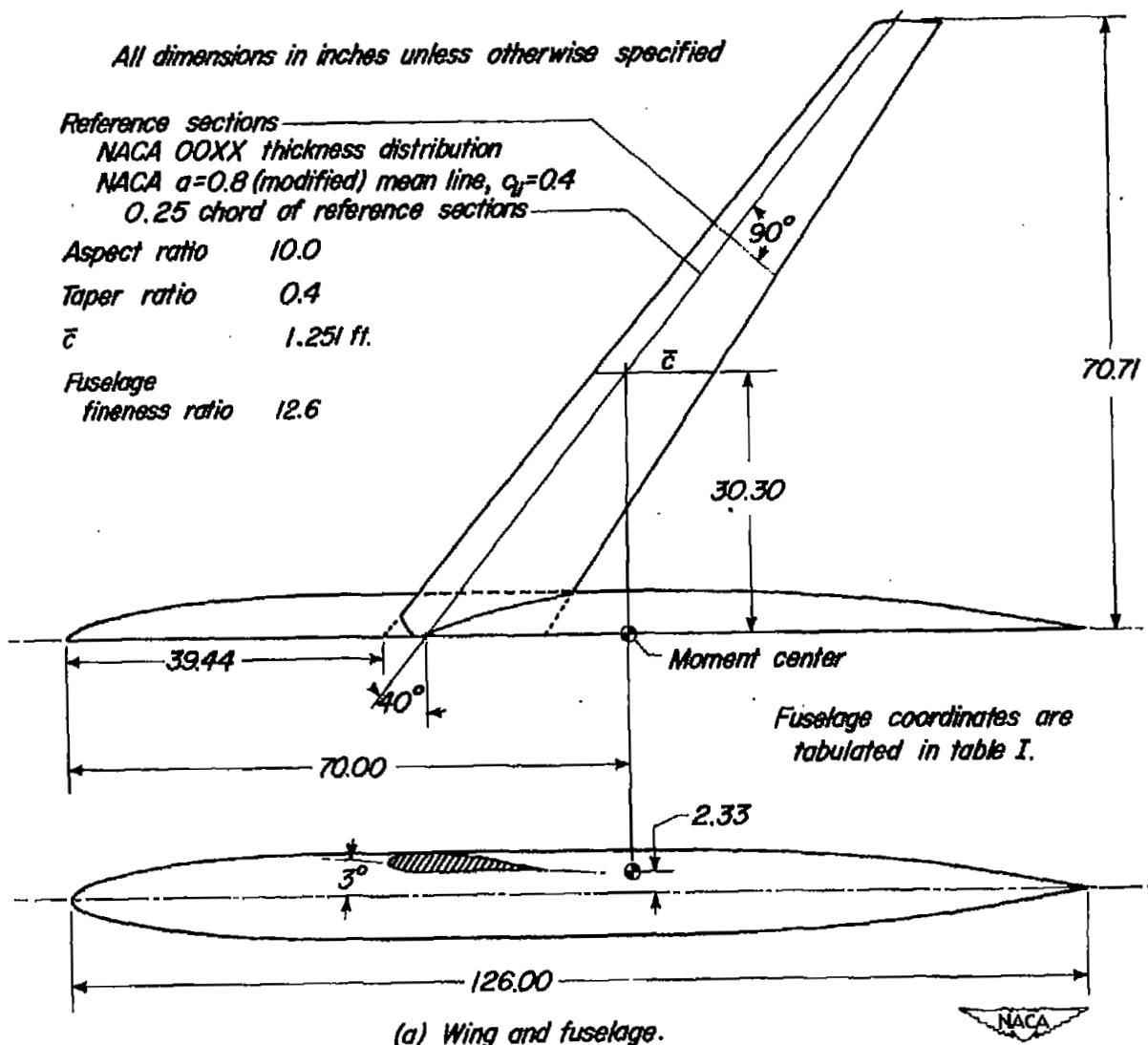
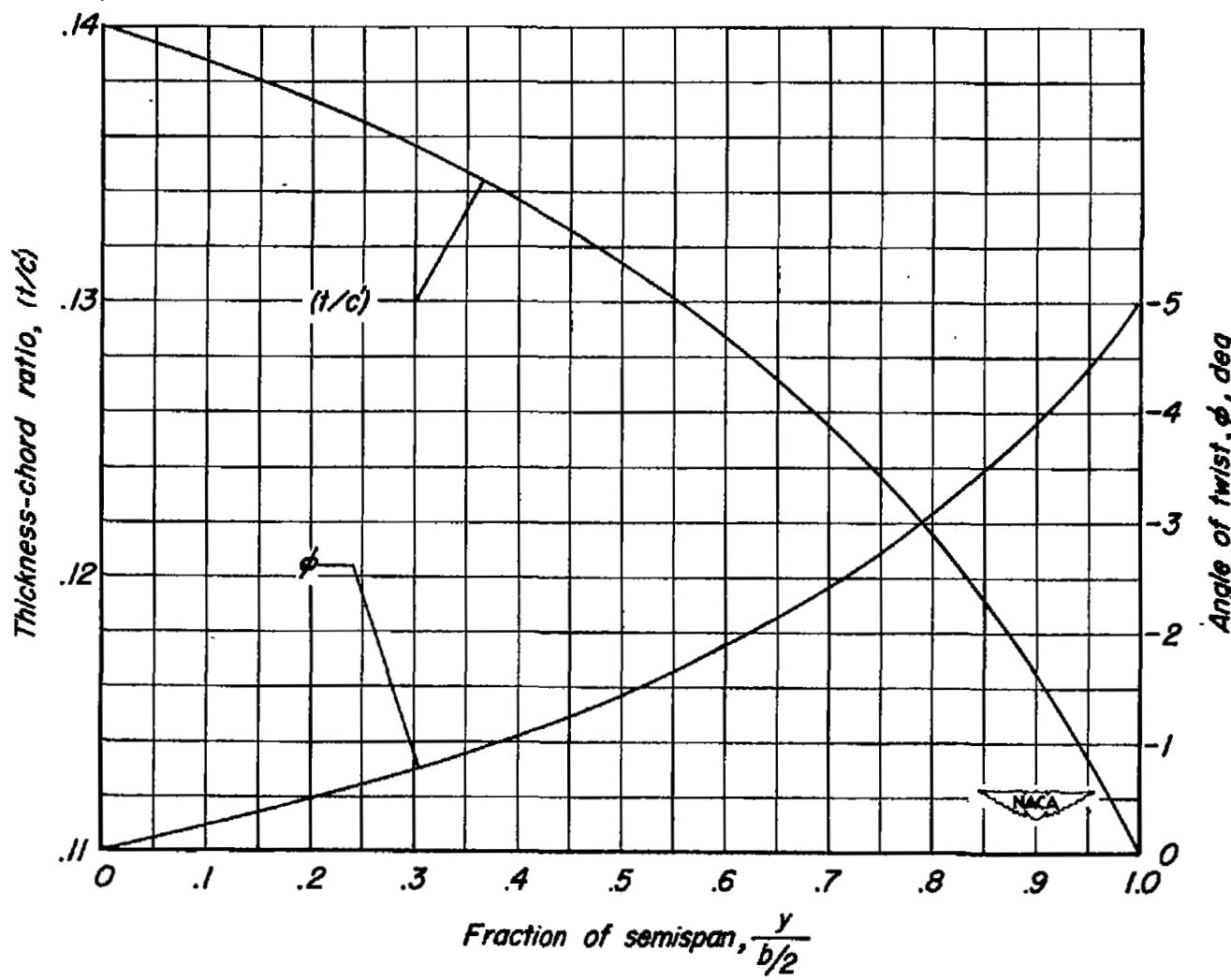
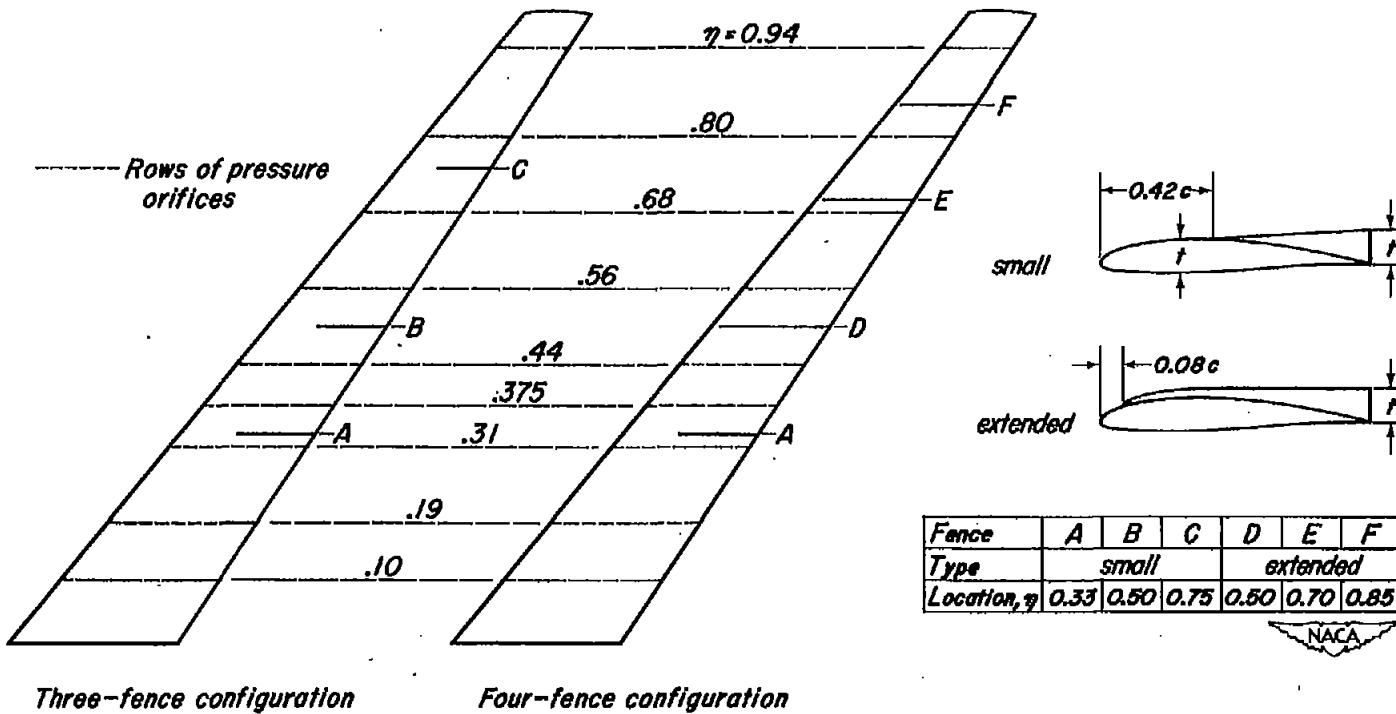


Figure 1 - Geometry of the model.



(b) Distribution of wing twist and thickness-chord ratio.

Figure 1. — Continued.



(c) Location of the pressure-orifice stations and details of the two fence configurations.

Figure 1.—Concluded.



(a) Wing-fuselage model in the wind tunnel.



(b) Details of the fences.

Figure 2.- Photographs of the model.

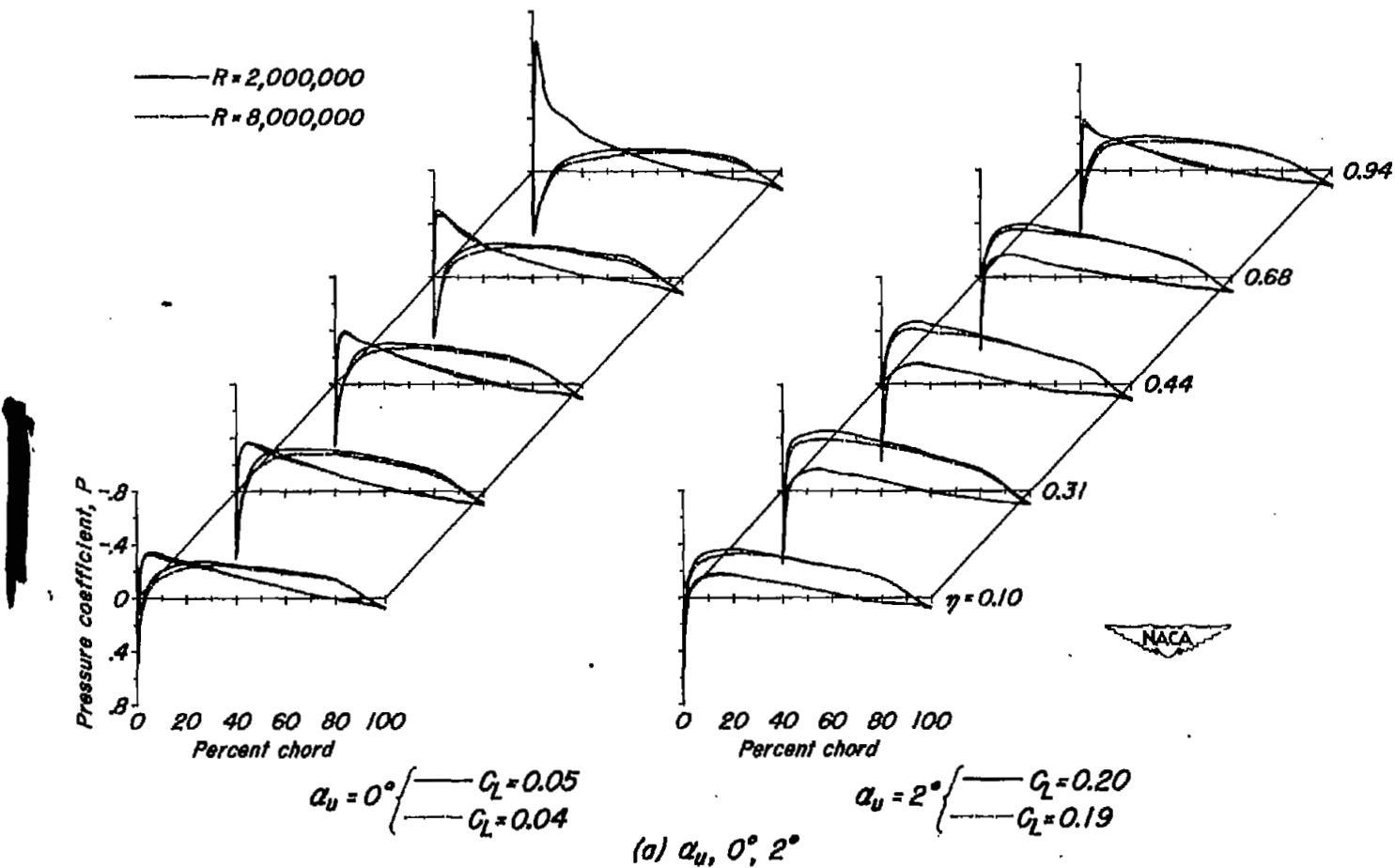


Figure 3.—The chordwise distribution of pressure coefficient at five semispan stations of the wing for the wing-fuselage combination at Reynolds numbers of 2,000,000 and 8,000,000. $M, 0.25$.

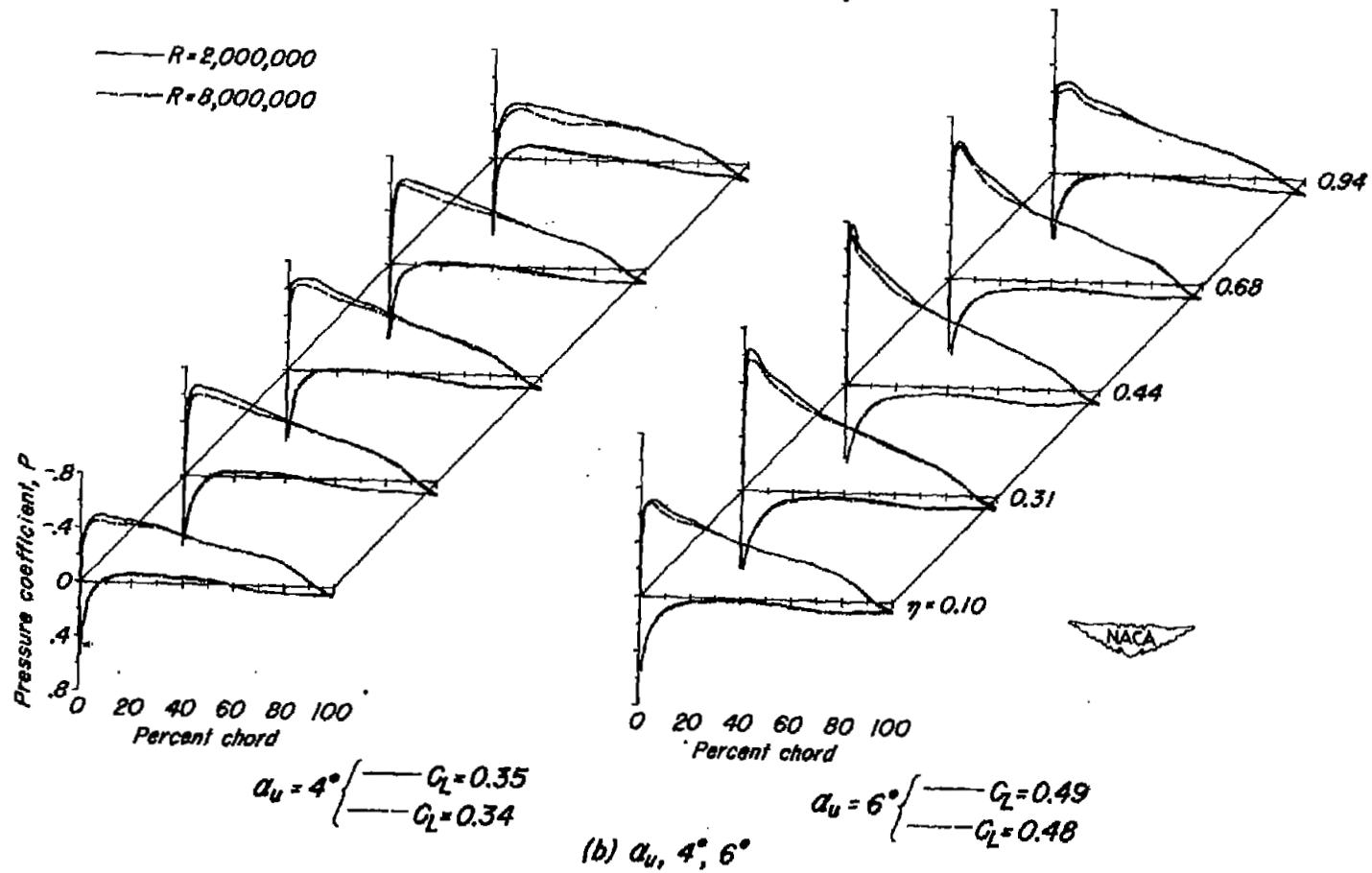


Figure 3.-Continued.

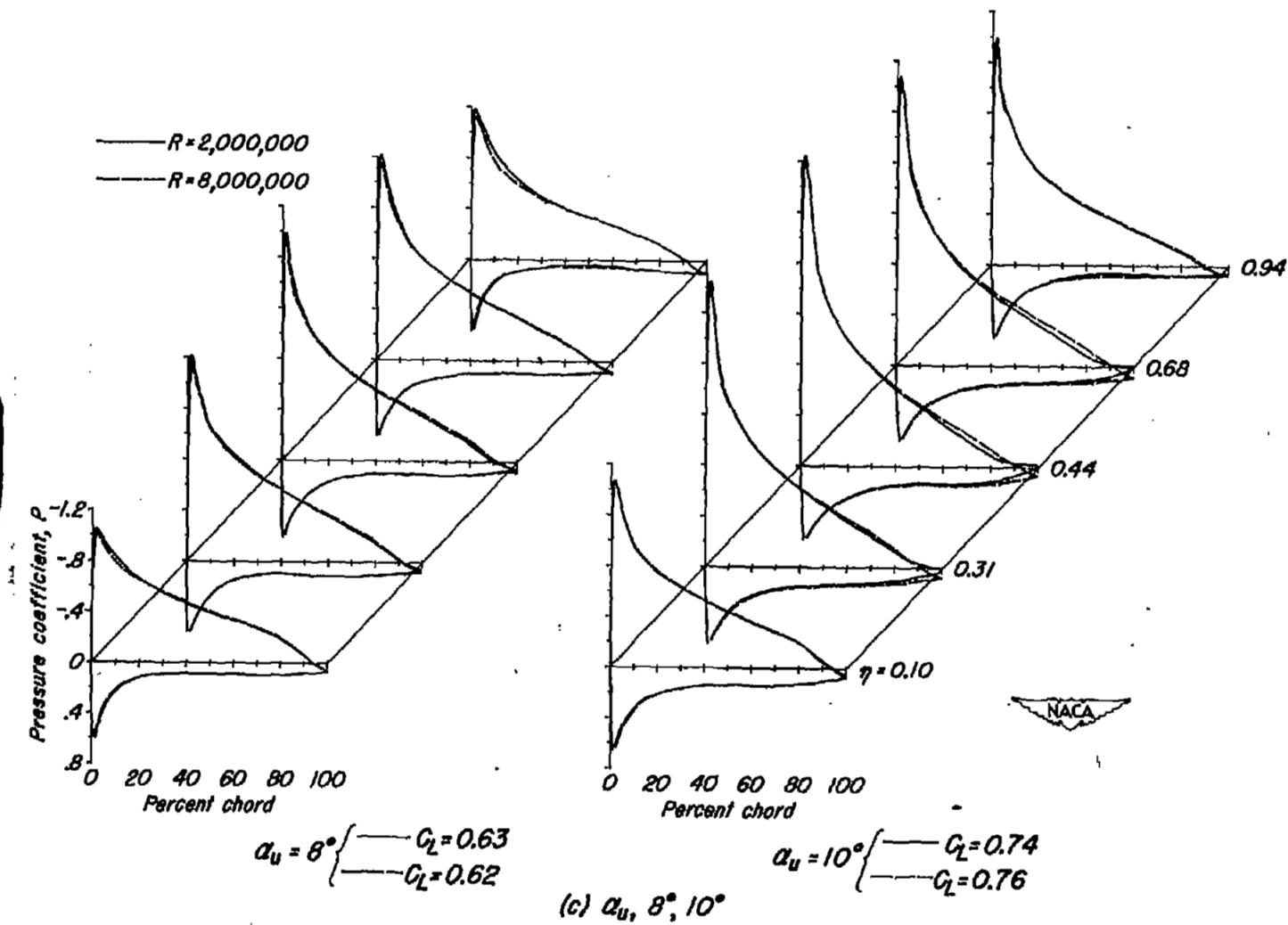


Figure 3.-Continued.

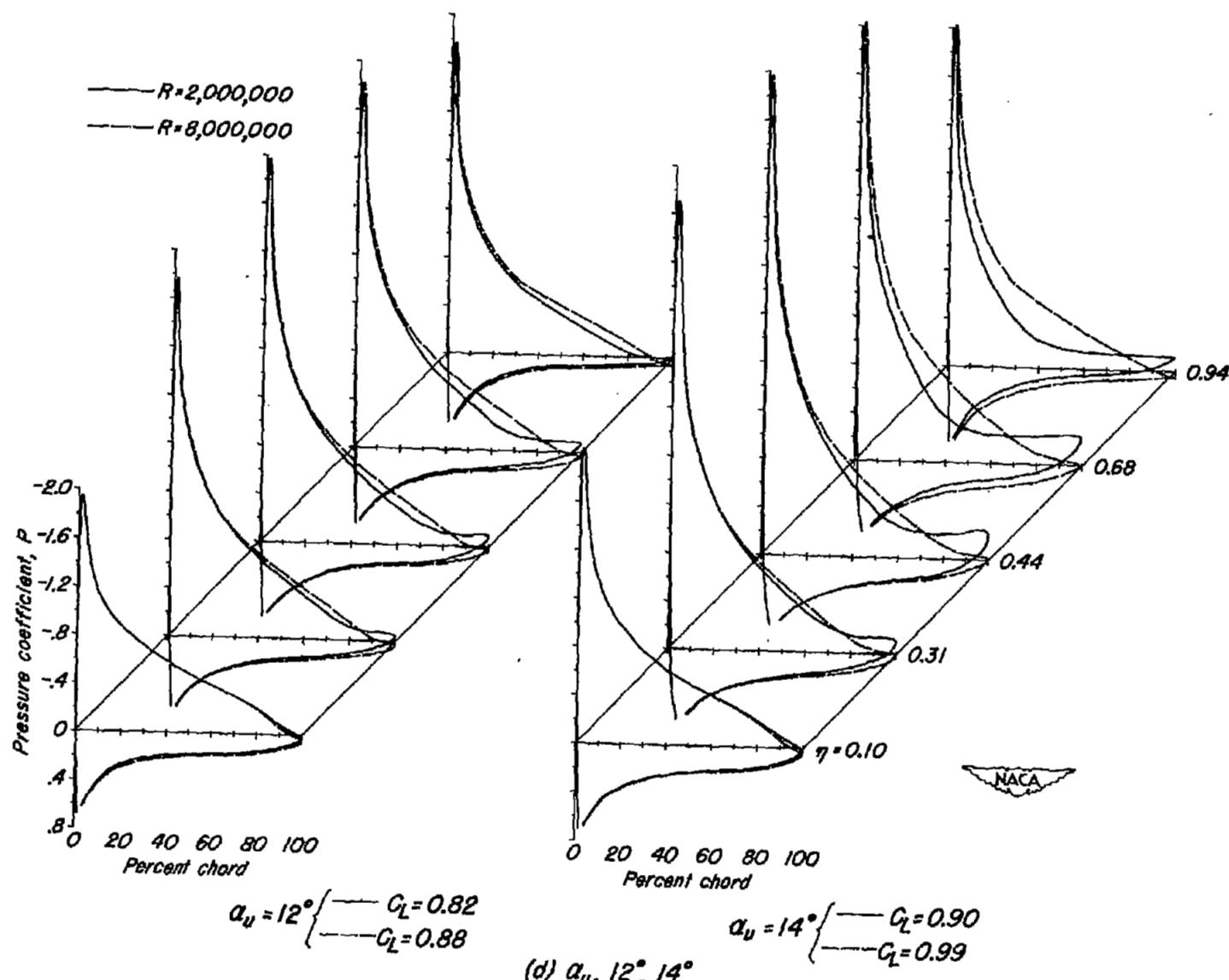


Figure 3.-Continued.

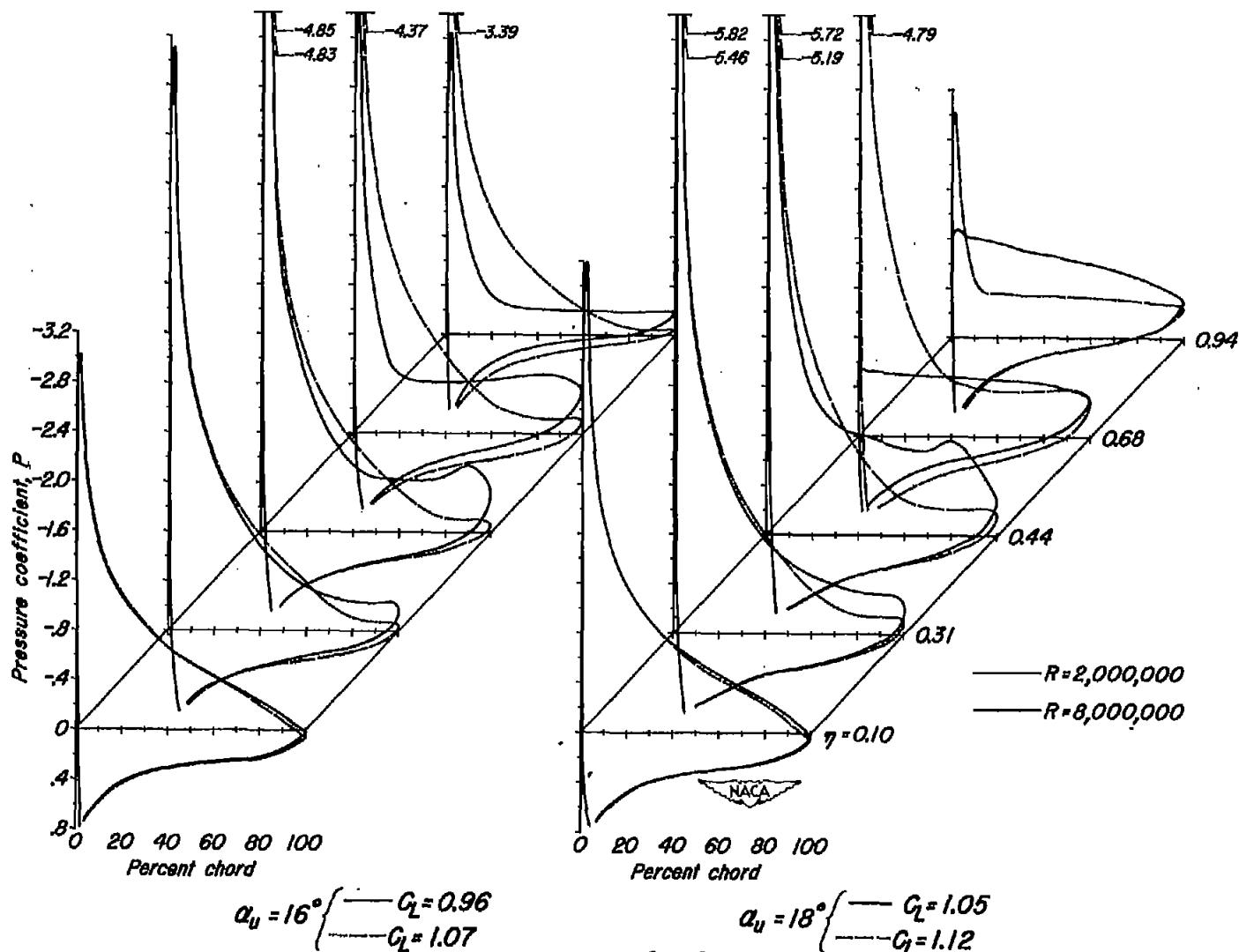


Figure 3.-Concluded.

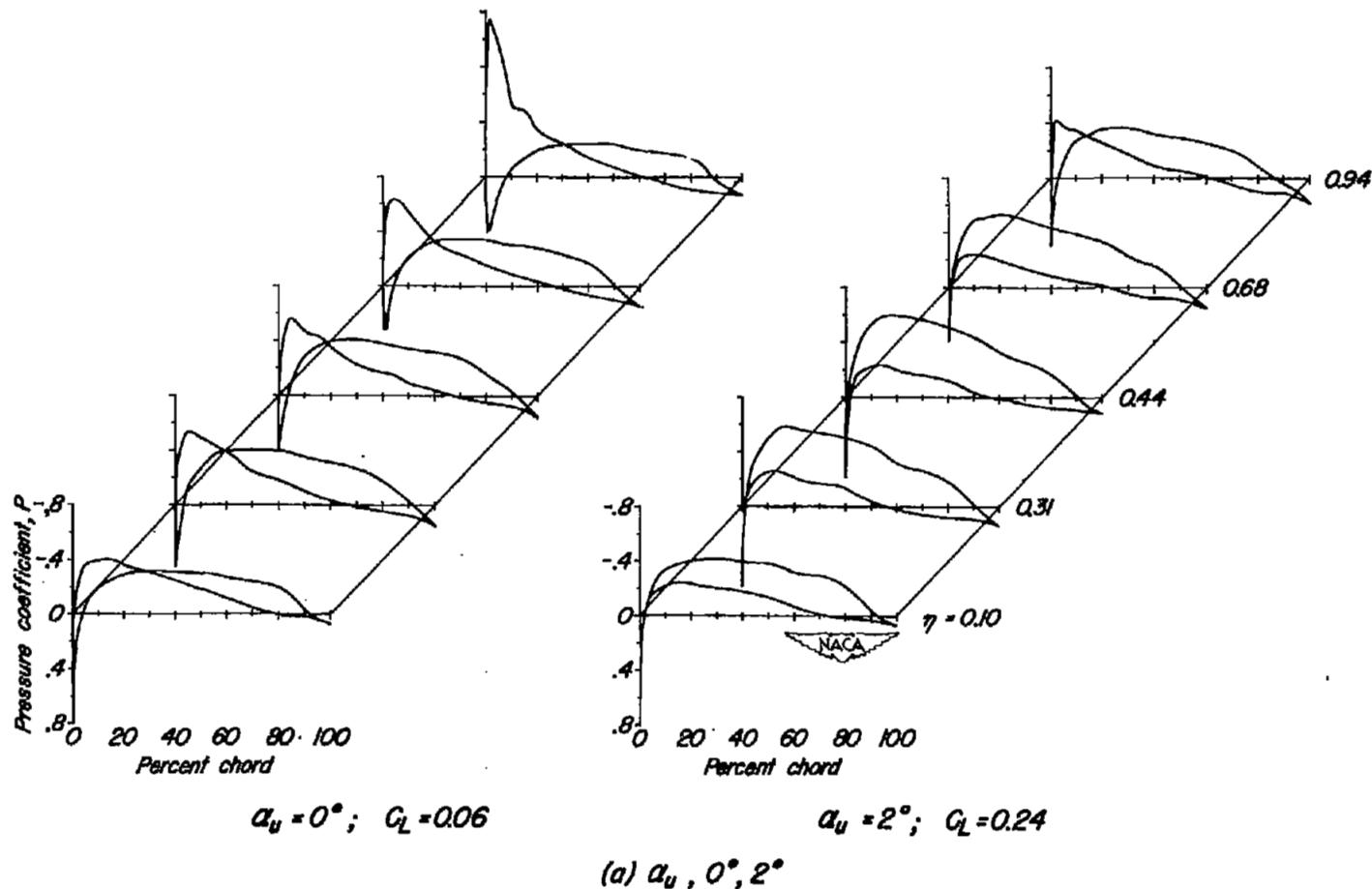


Figure 4.-The chordwise distribution of pressure coefficient at five semispan stations of the wing for the wing-fuselage combination. $M, 0.80; R, 2,000,000$.

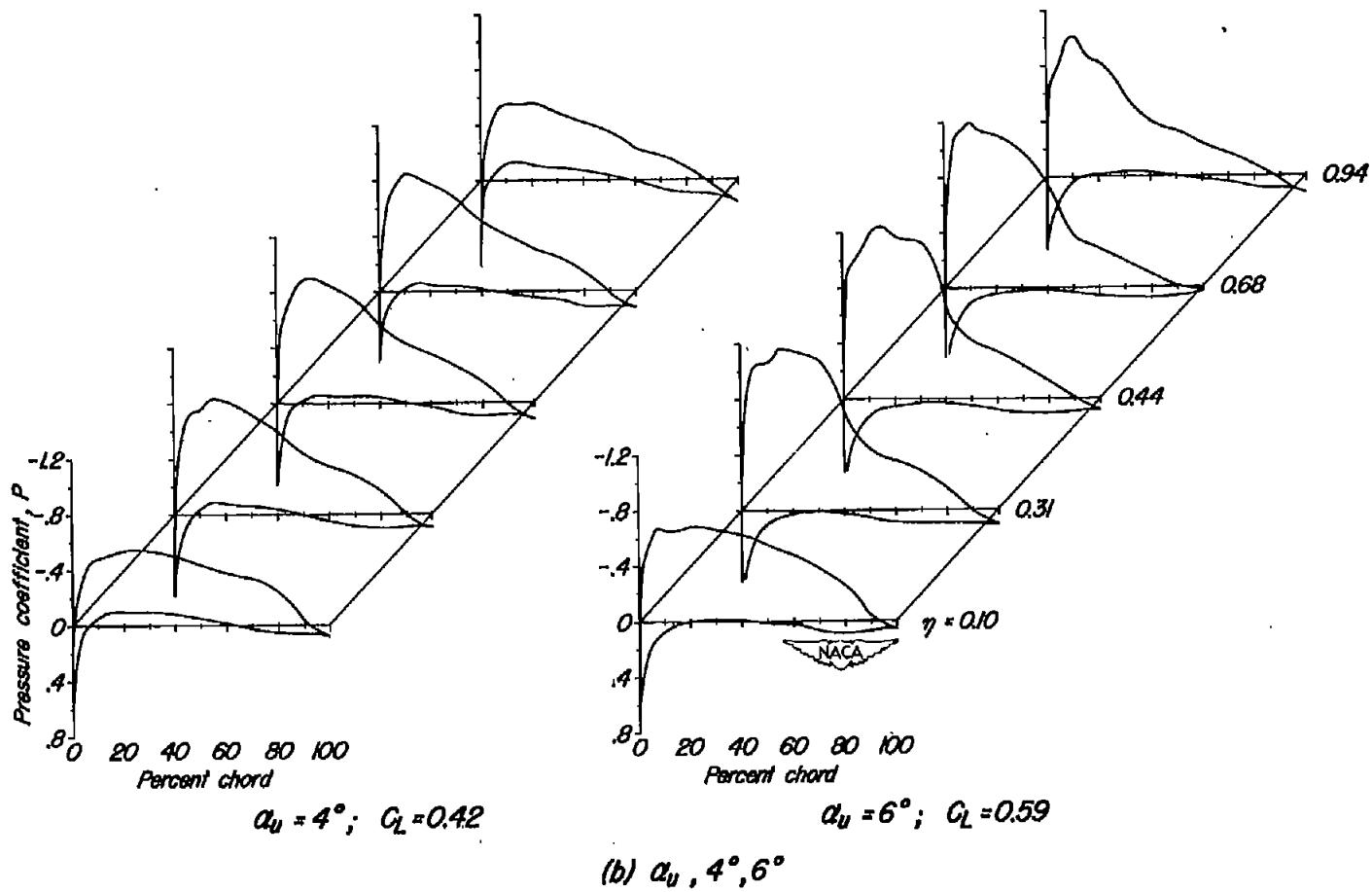
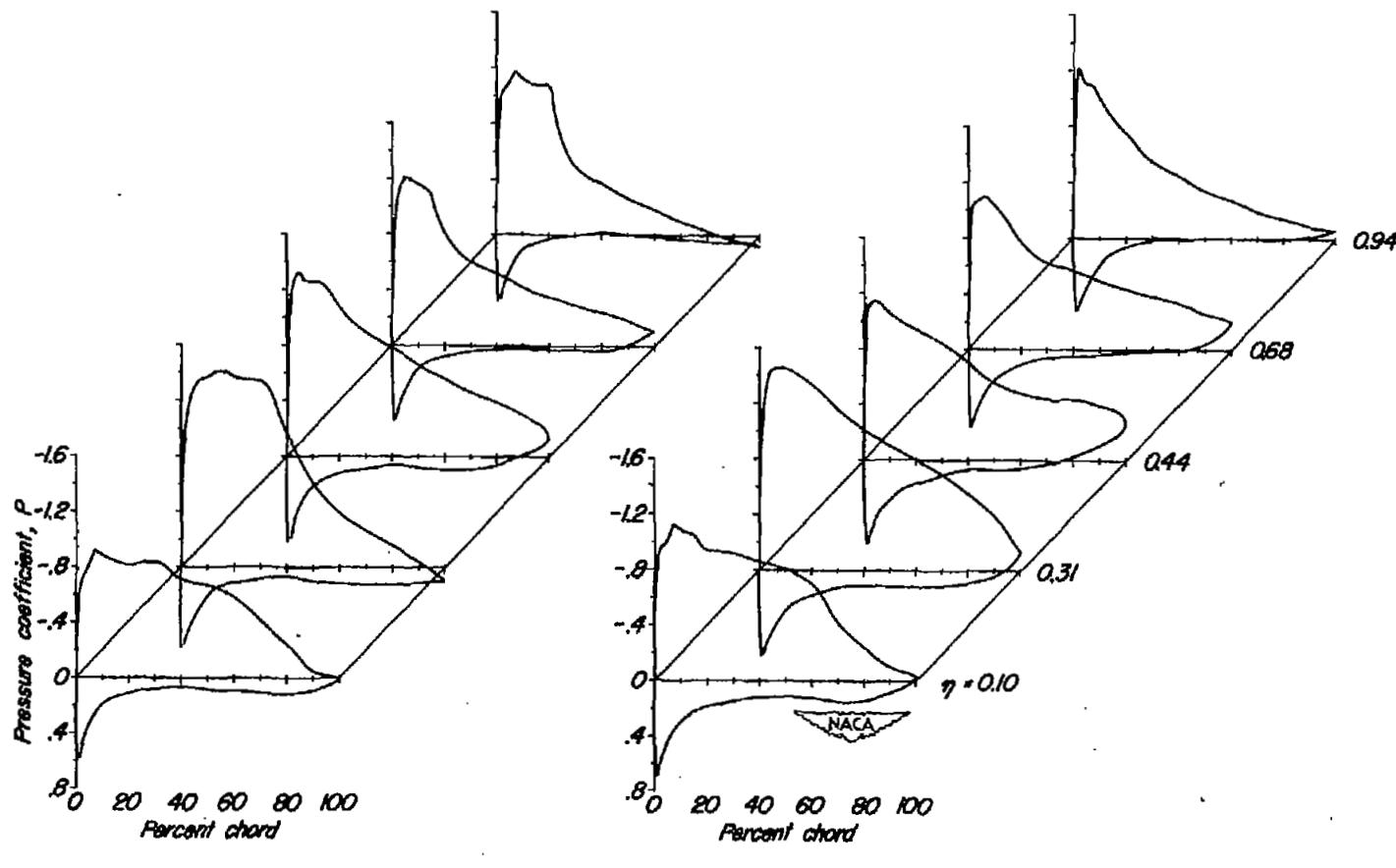


Figure 4.-Continued.



$$\alpha_u = 8^\circ; C_L = 0.69$$

$$\alpha_u = 10^\circ; C_L = 0.77$$

(c) $\alpha_u, 8^\circ, 10^\circ$

Figure 4.—Continued.

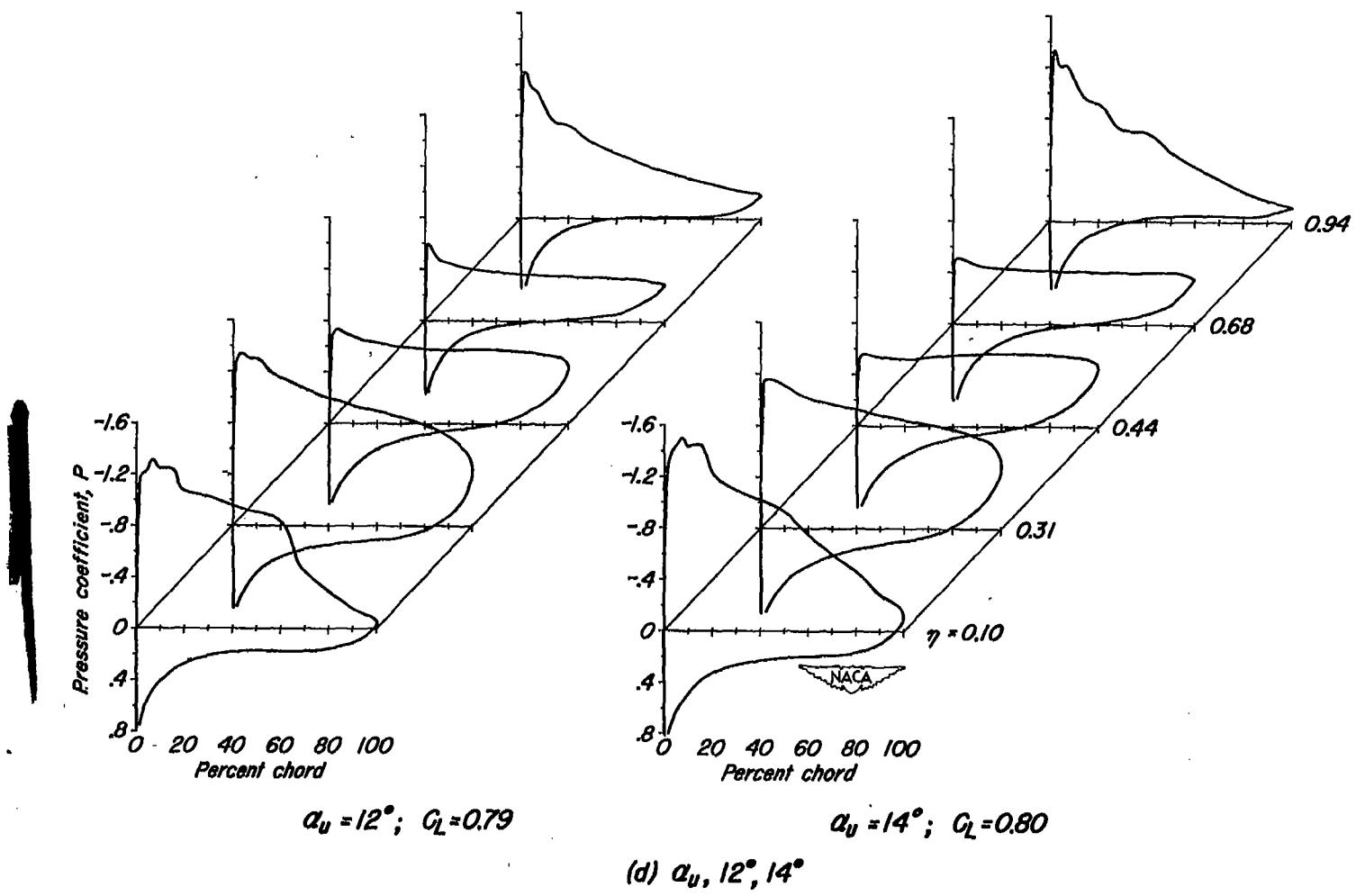


Figure 4.-Concluded.

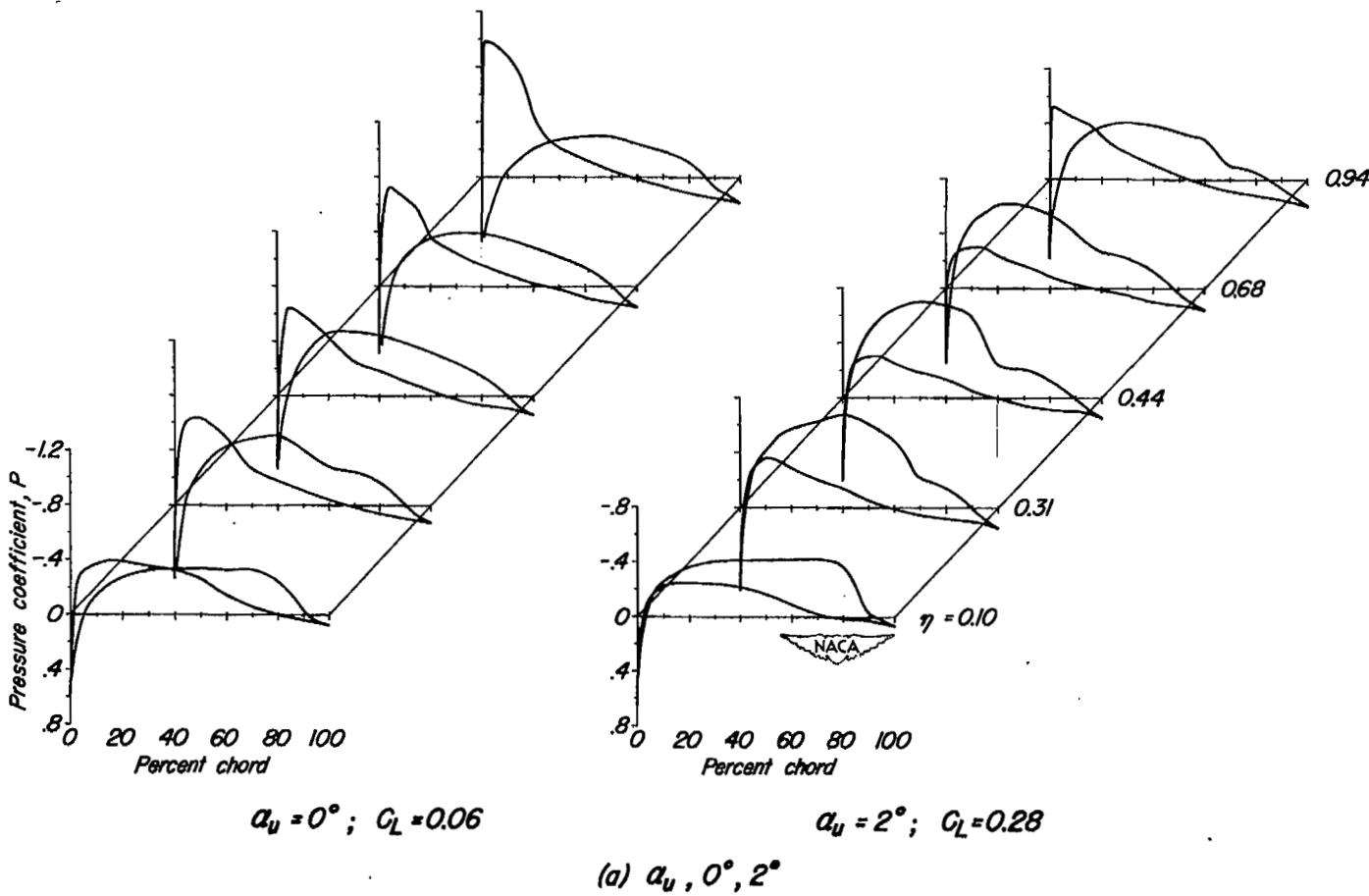


Figure 5.—The chordwise distribution of pressure coefficient at five semispan stations of the wing for the wing-fuselage combination. $M, 0.90$; $R, 2,000,000$.

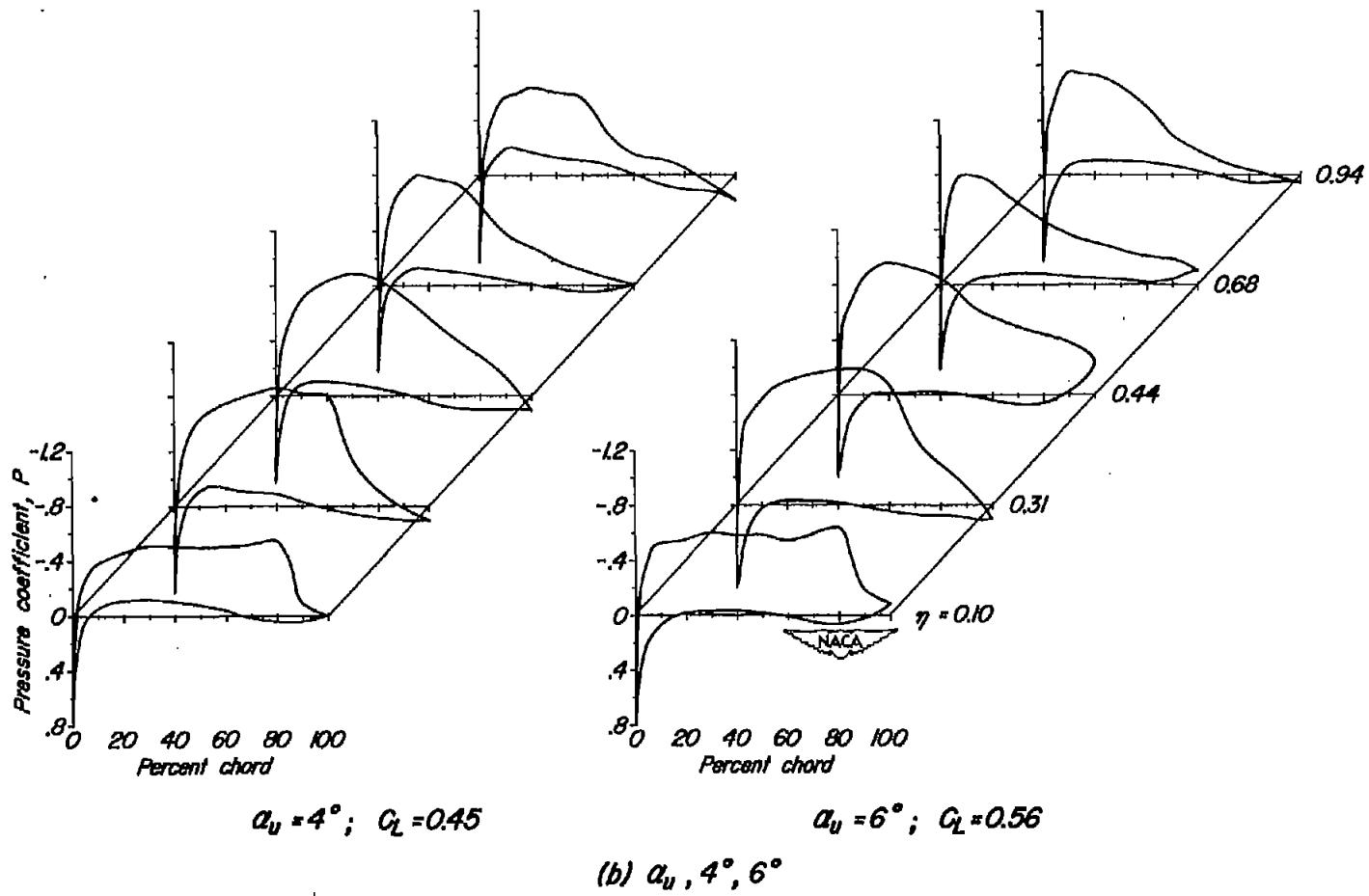
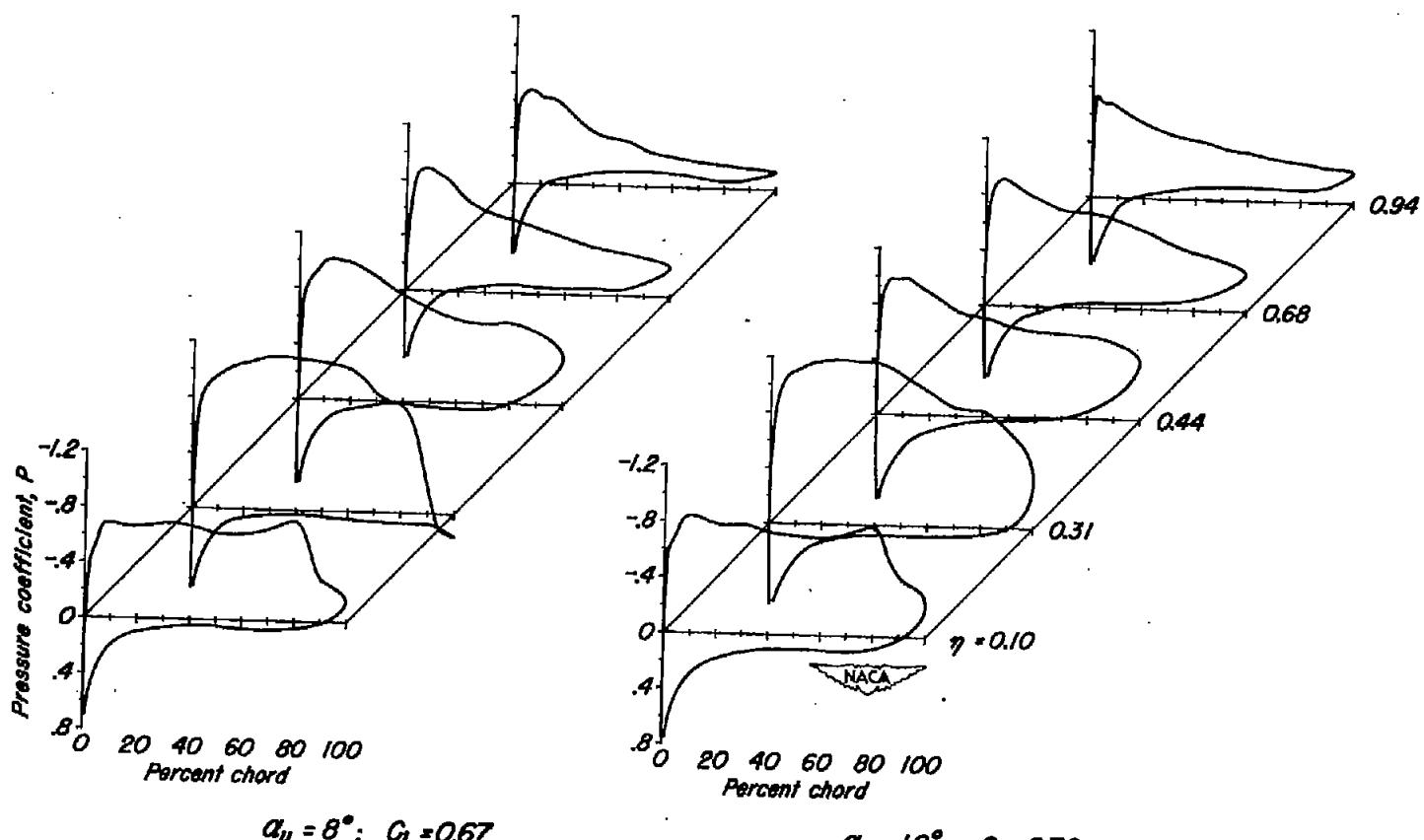


Figure 5.—Continued.



(c) $\alpha_u, 8^\circ, 10^\circ$

Figure 5.-Concluded.

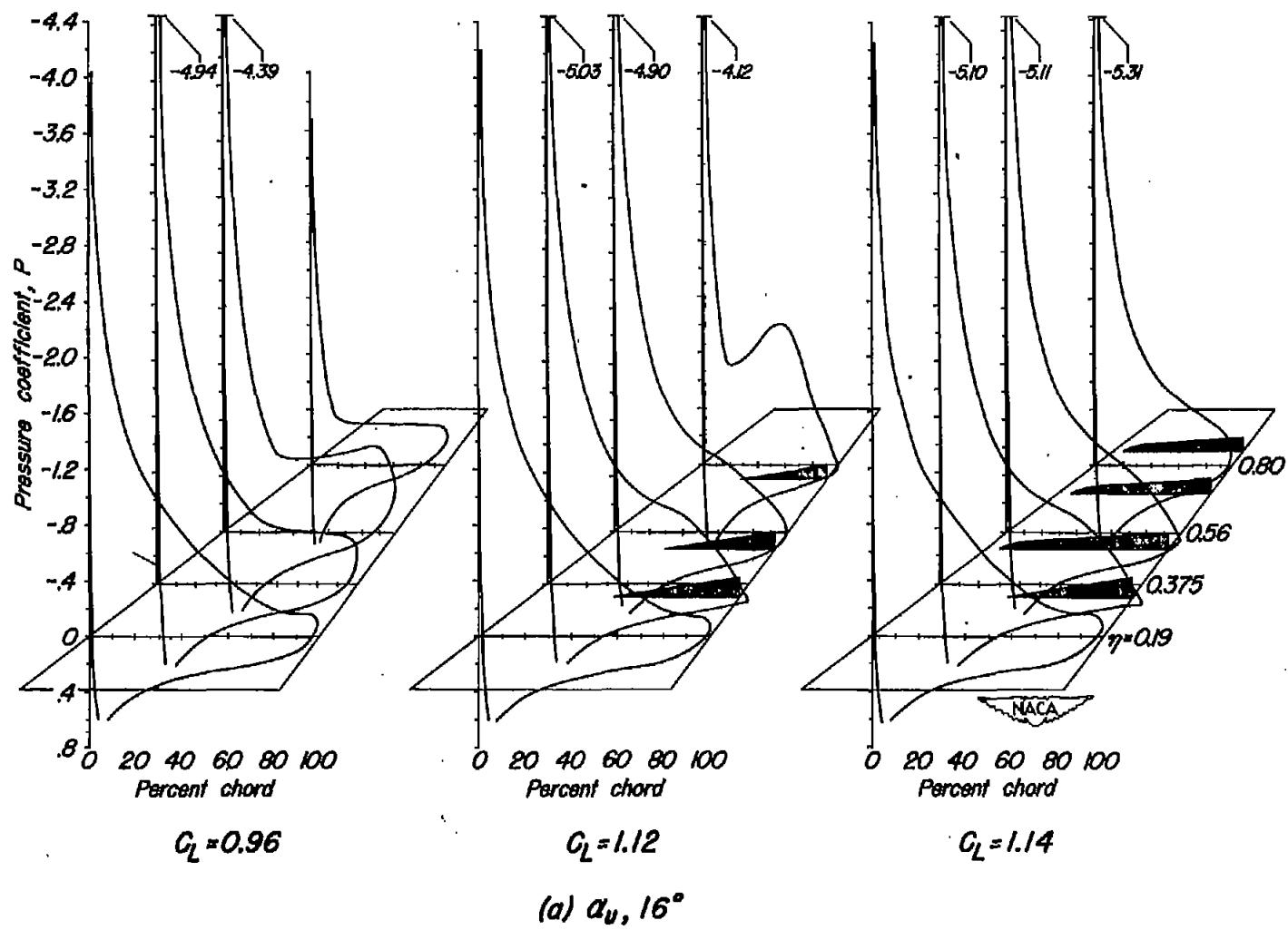


Figure 6.- The chordwise distribution of pressure coefficient at four semispan stations of the wing for the wing-fuselage combination without fences, with three fences, and with four fences. $M, 0.25; R, 2,000,000.$

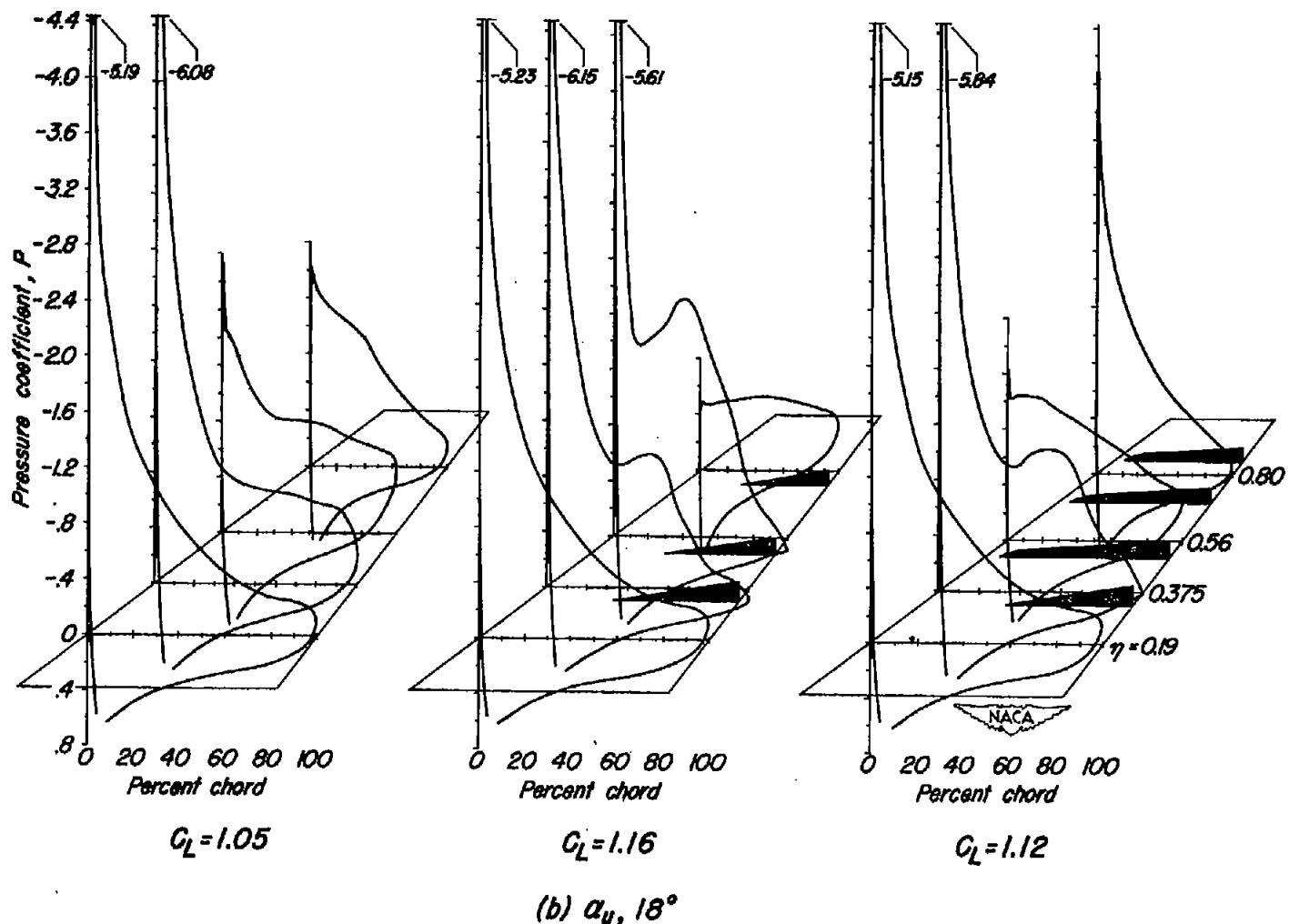


Figure 6.-Concluded.

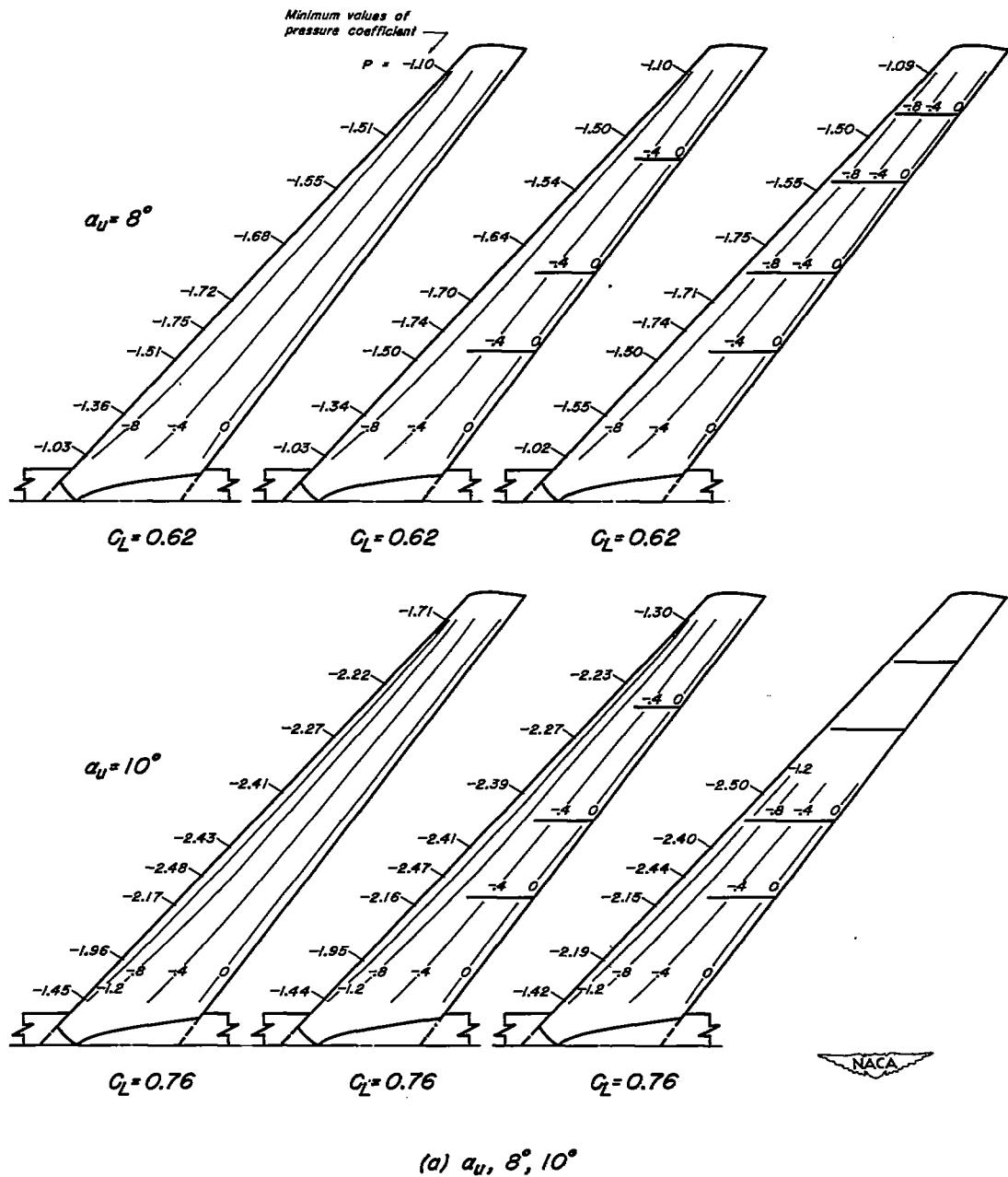


Figure 7.—The lines of constant pressure coefficient and the approximate regions of separated flow on the wing-fuselage combination without fences, with three fences, and with four fences. $M, 0.25; R, 8,000,000$.

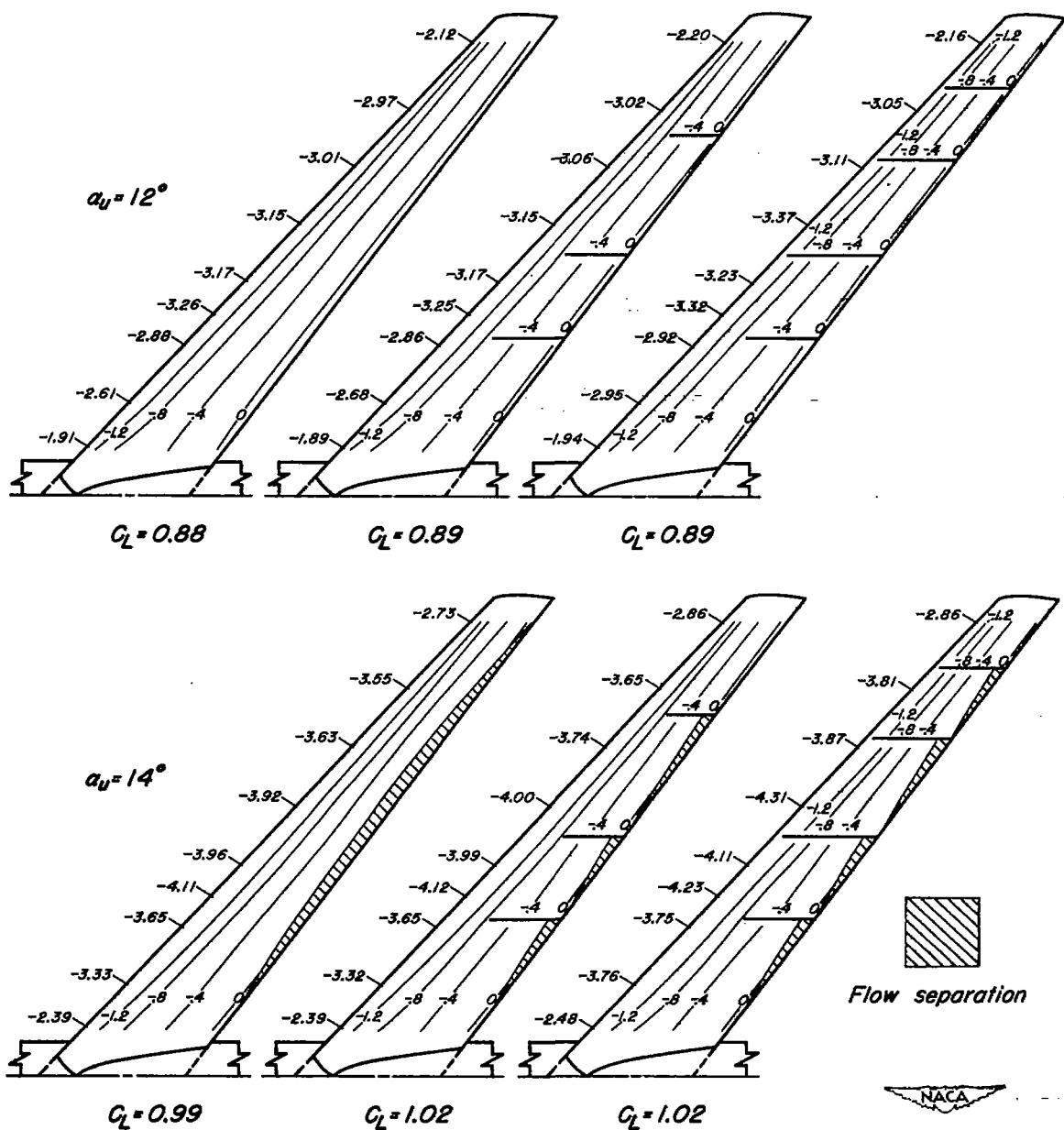
(b) $\alpha_u, 12^\circ, 14^\circ$

Figure 7.—Continued.

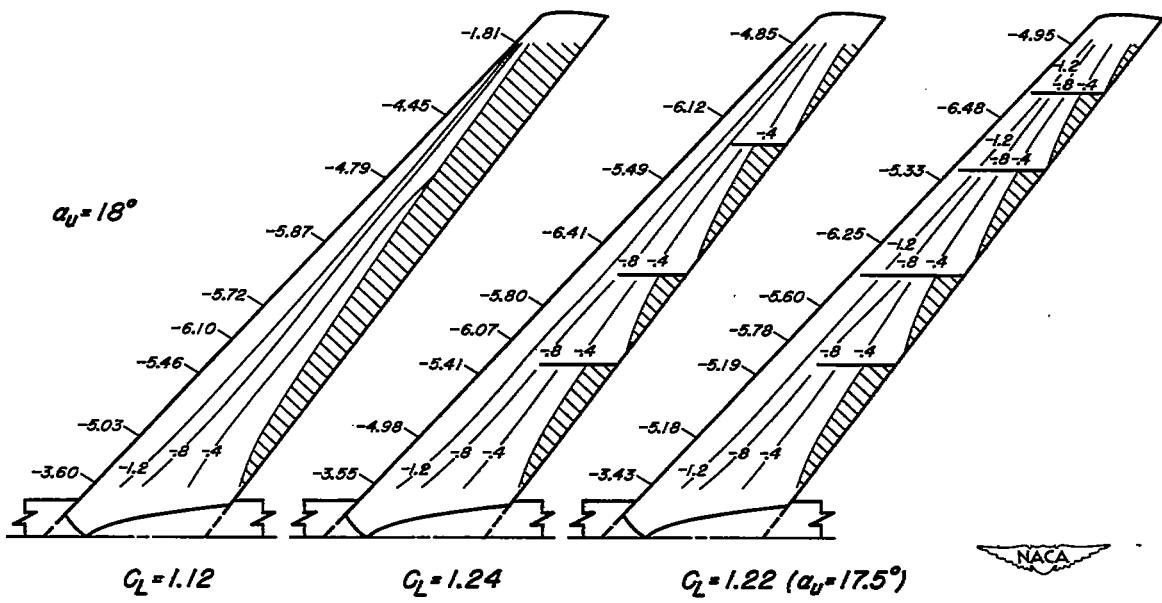
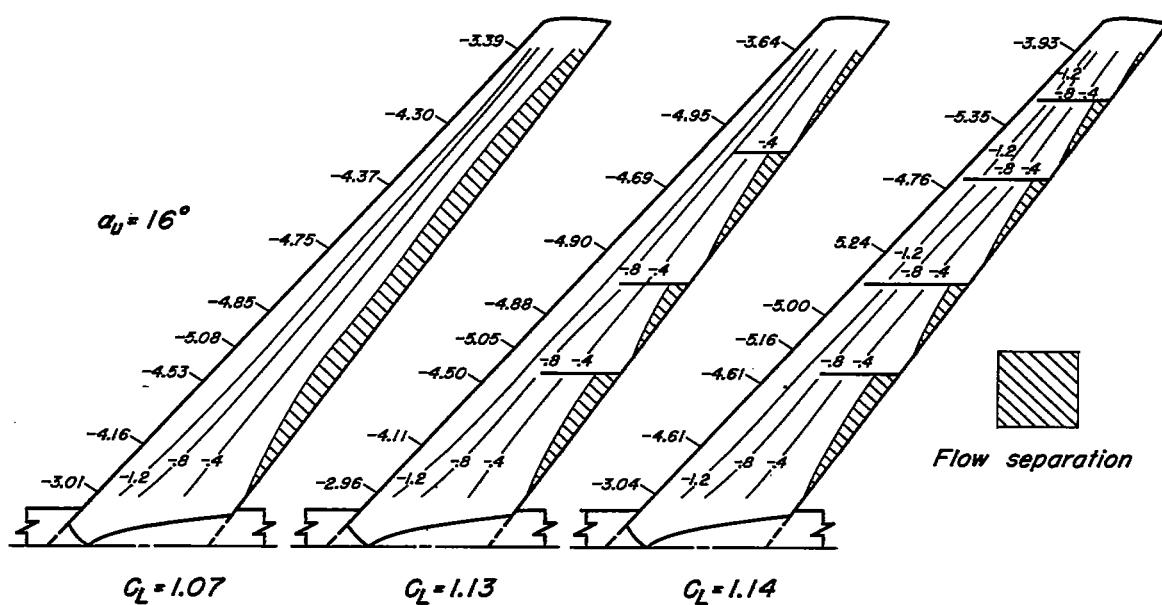
(c) $\alpha_u, 16^\circ, 18^\circ$

Figure 7.—Concluded.

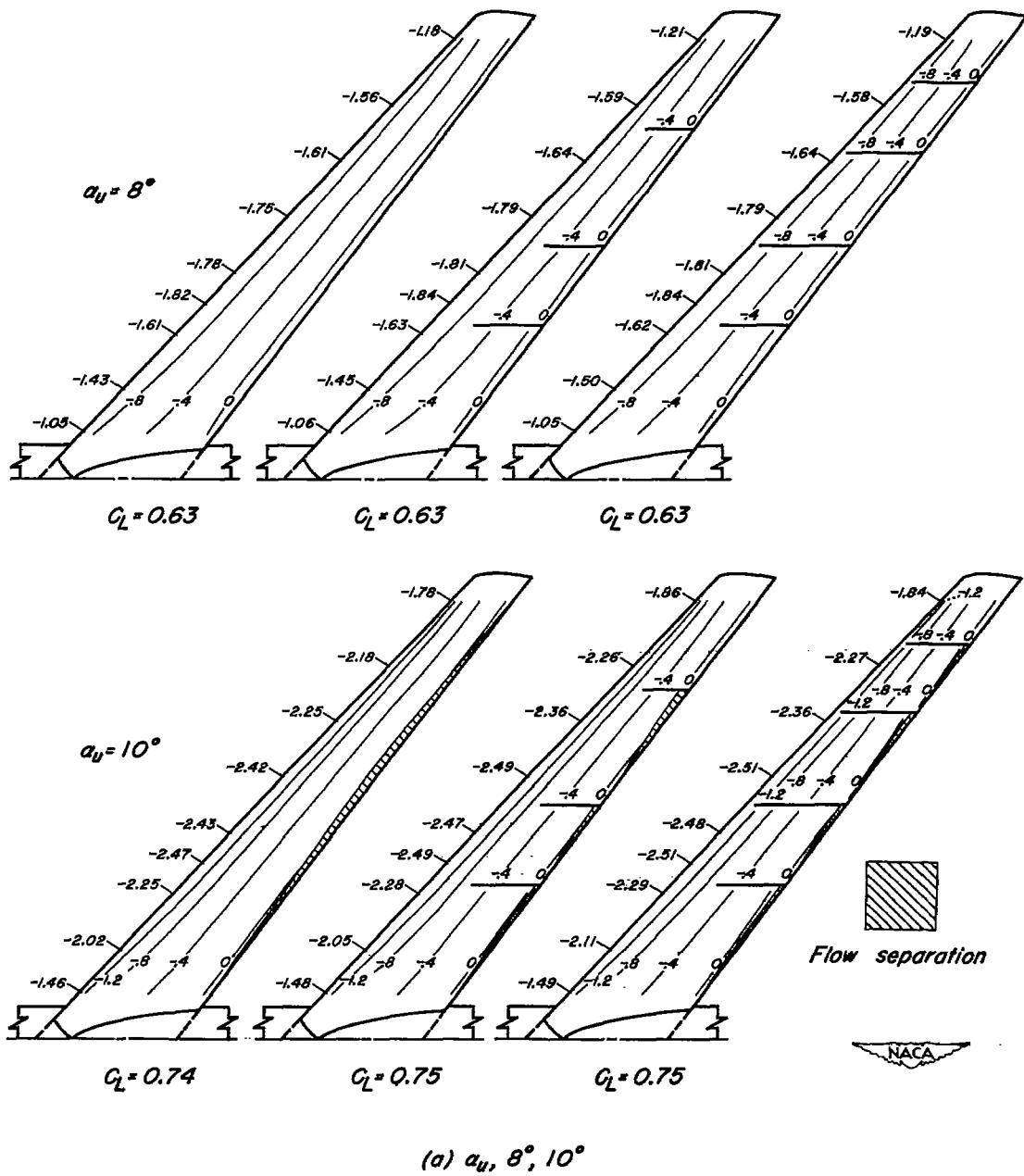


Figure 8.—The lines of constant pressure coefficient and the approximate regions of separated flow on the wing-fuselage combination without fences, with three fences, and with four fences. $M, 0.25; R, 2,000,000$.

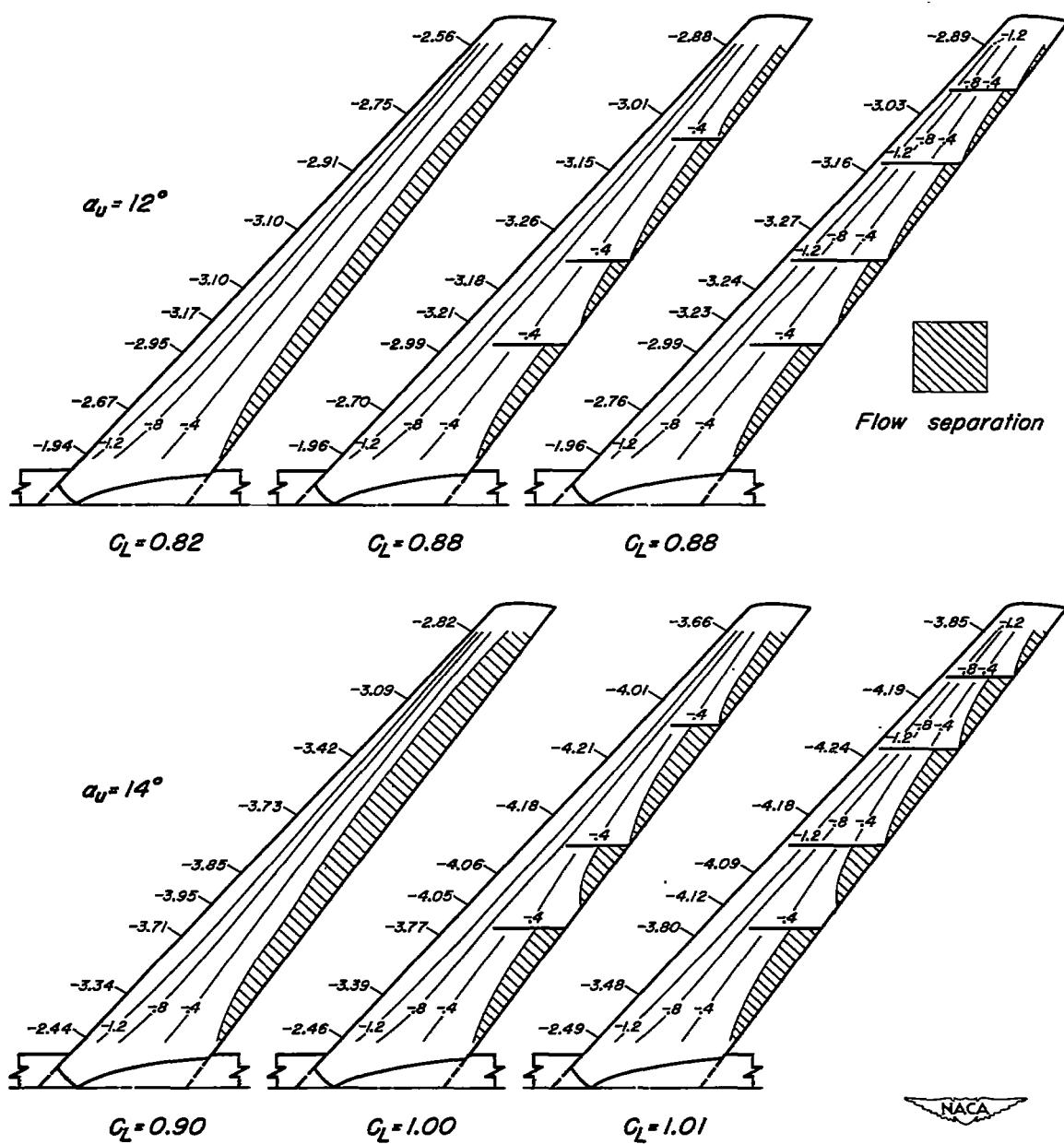
(b) $\alpha_u, 12^\circ, 14^\circ$

Figure 8.—Continued.

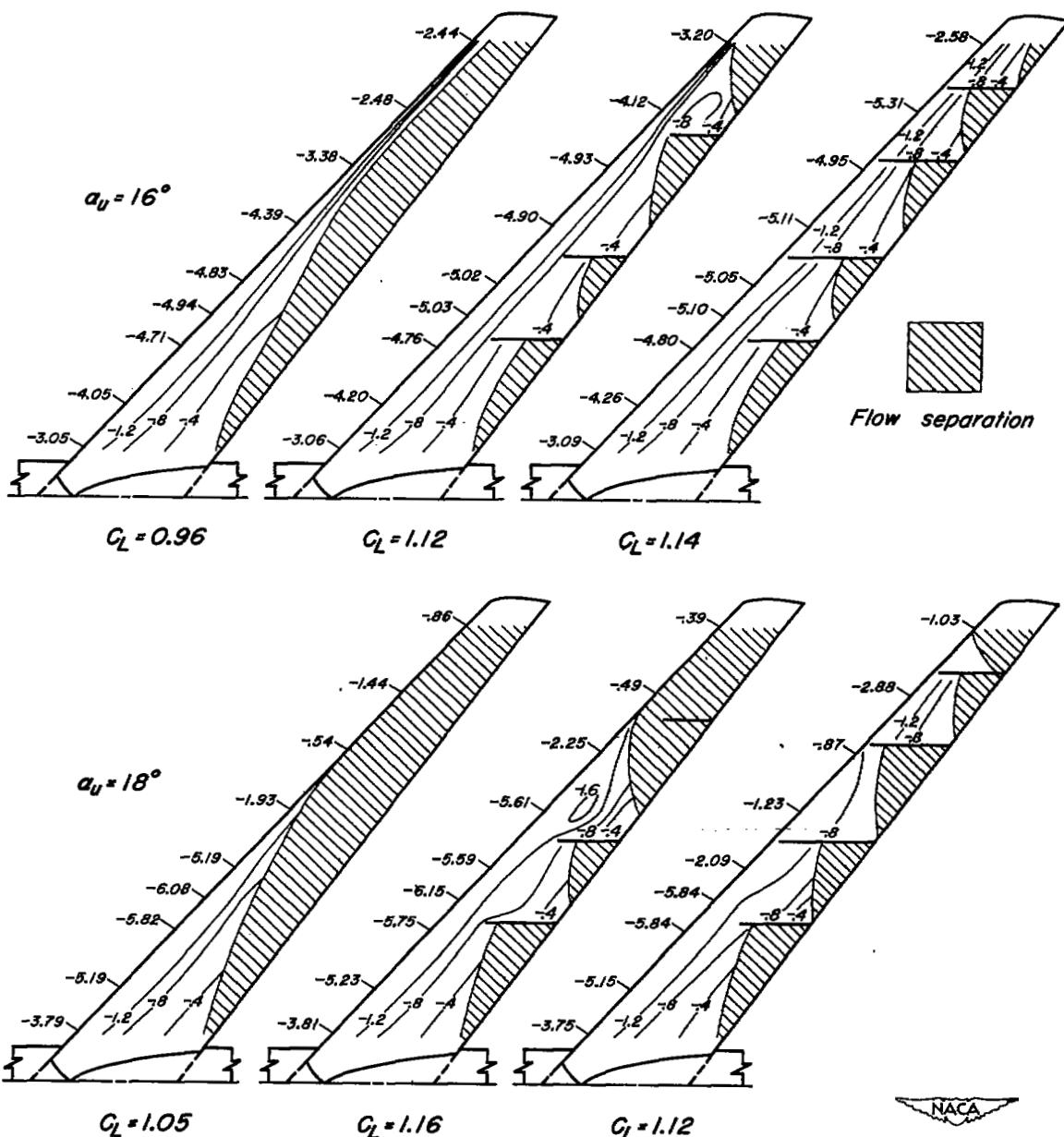
(c) $\alpha_U, 16^\circ, 18^\circ$

Figure 8.-Concluded.

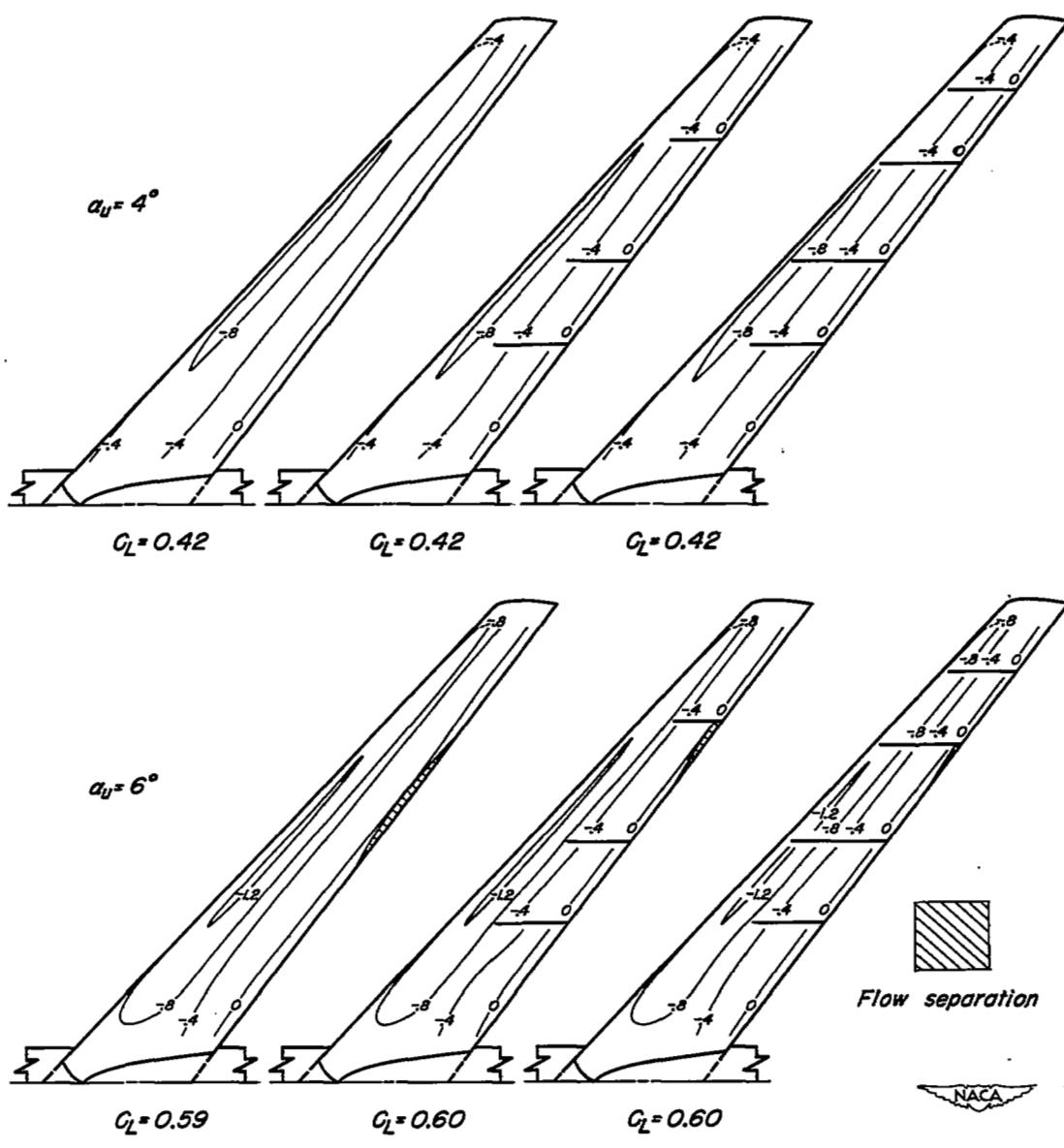
(a) $\alpha_U, 4^\circ, 6^\circ$

Figure 9.—The lines of constant pressure coefficient and the approximate regions of separated flow on the wing-fuselage combination without fences, with three fences, and with four fences. $M, 0.80; R, 2,000,000$.

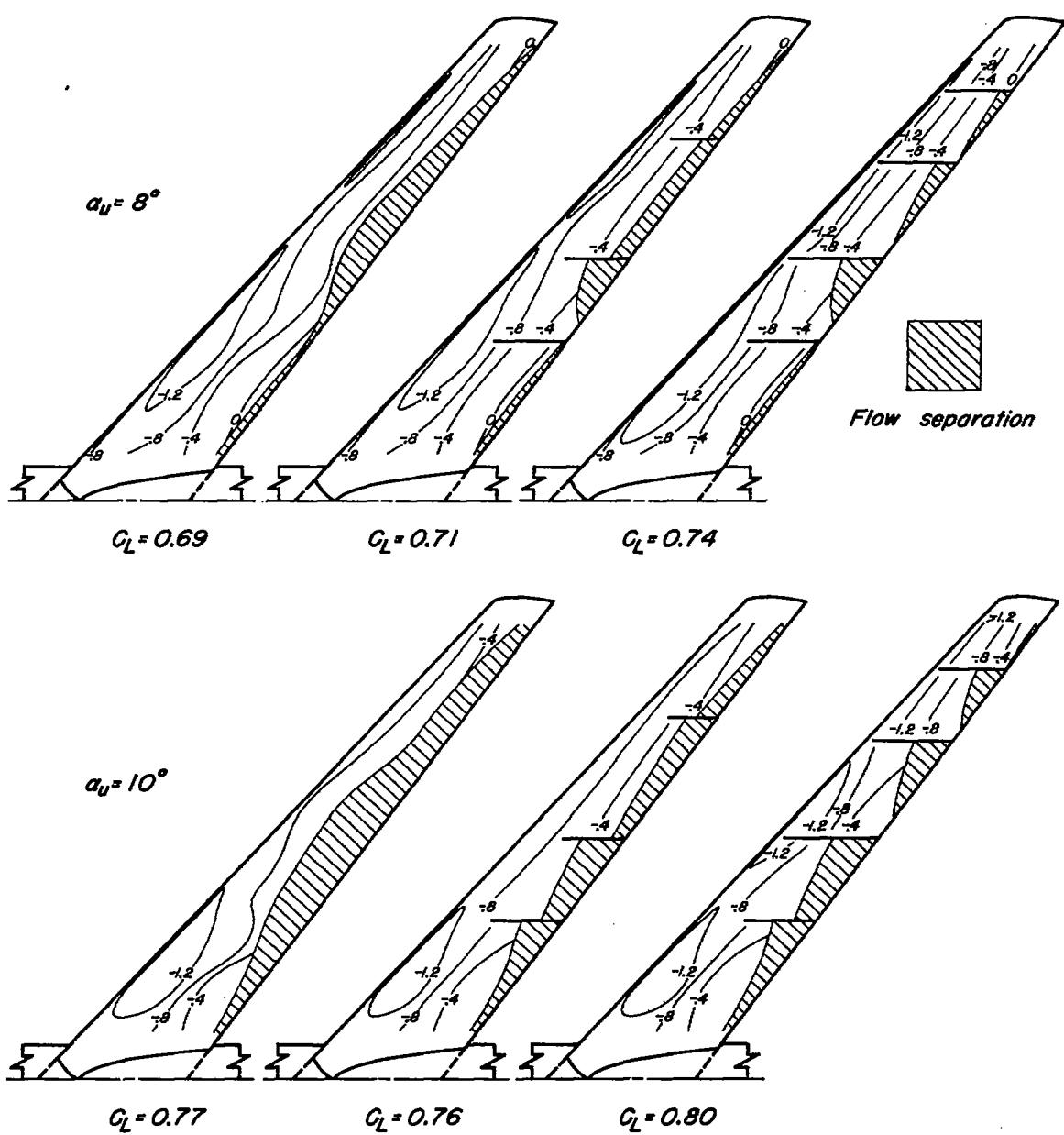
(b) $\alpha_u, 8^\circ, 10^\circ$

Figure 9.—Concluded.

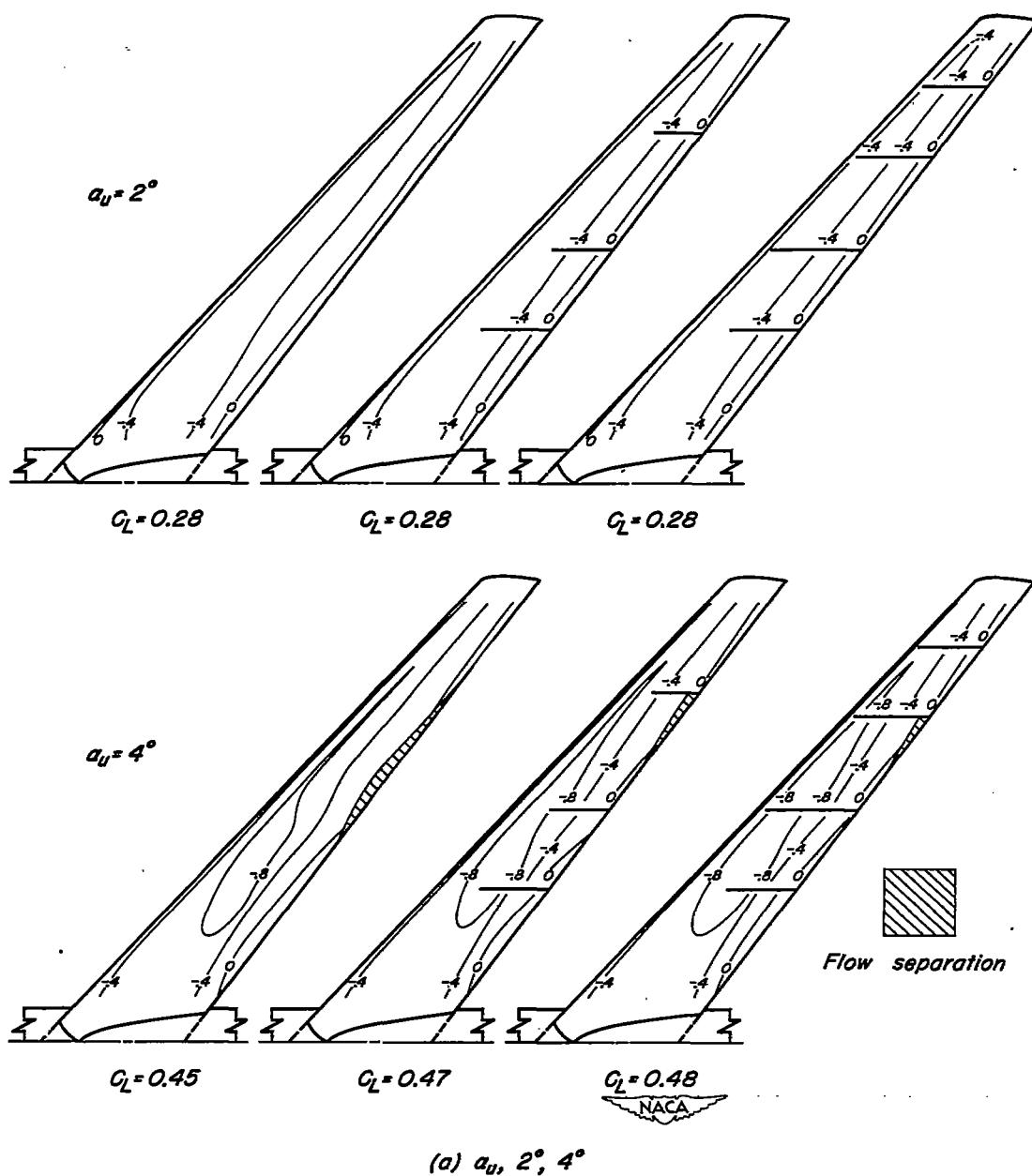
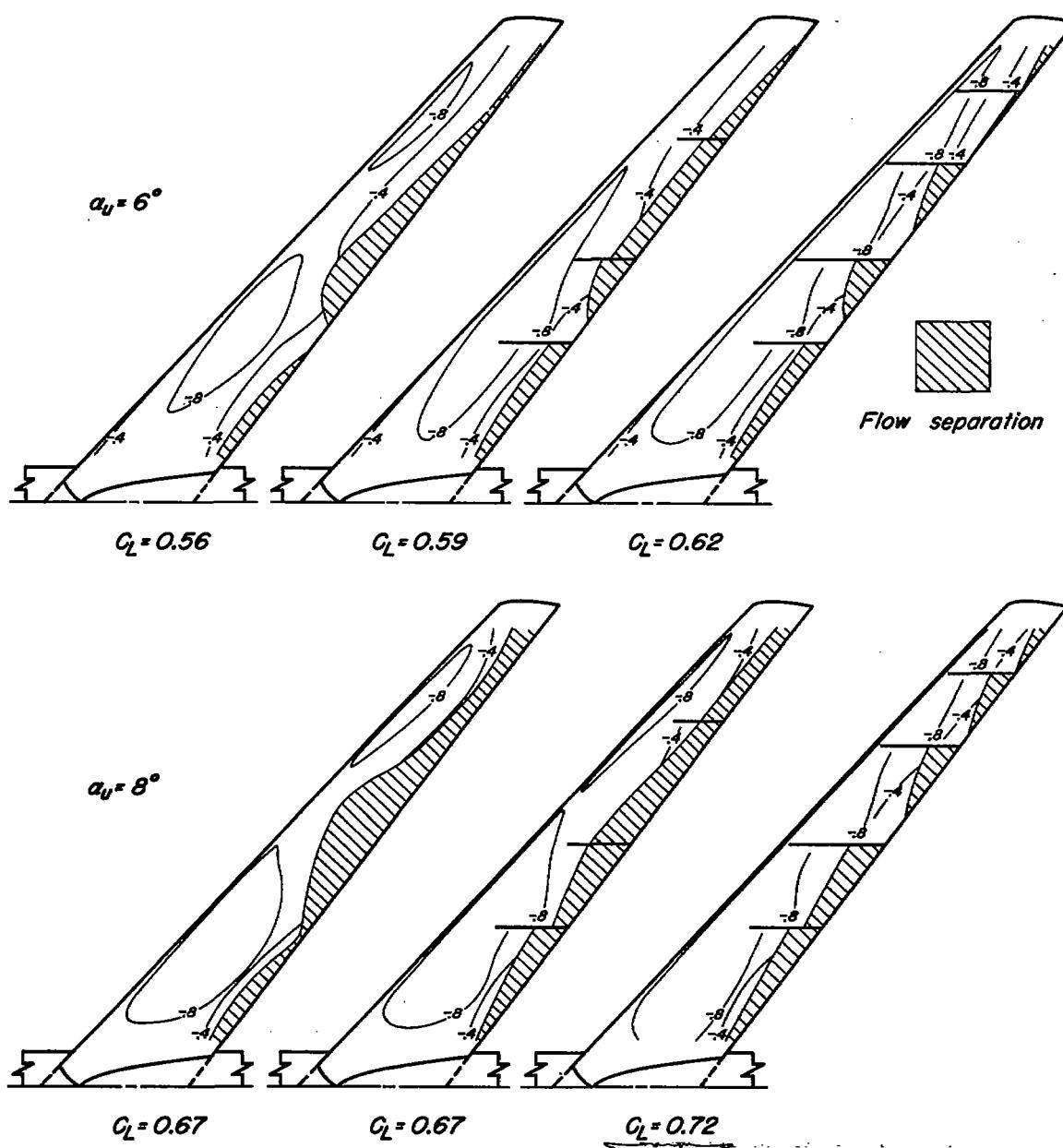
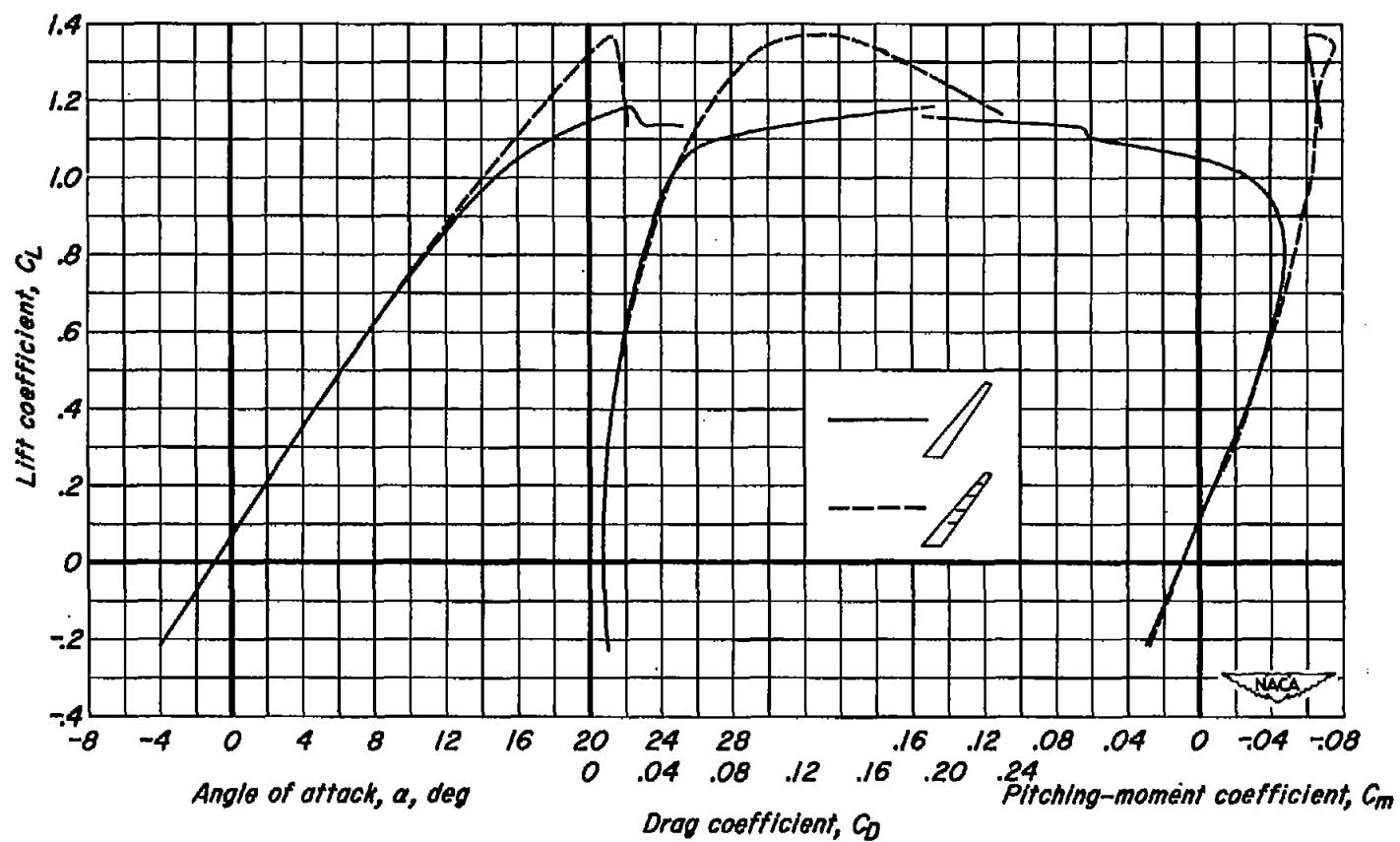


Figure 10.—The lines of constant pressure coefficient and the approximate regions of separated flow on the wing-fuselage combination without fences, with three fences, and with four fences $M, 0.90; R, 2,000,000$.

(b) $\alpha_u, 6^\circ, 8^\circ$

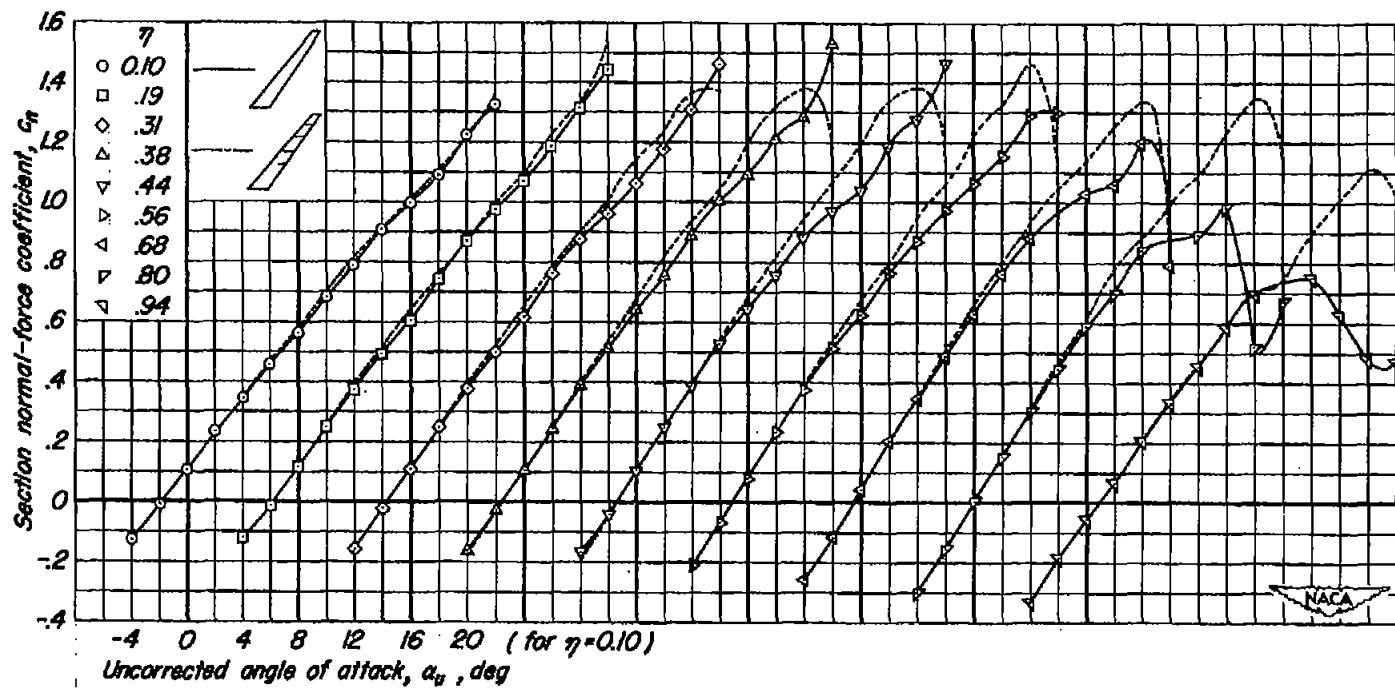
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Figure 10.-Concluded.



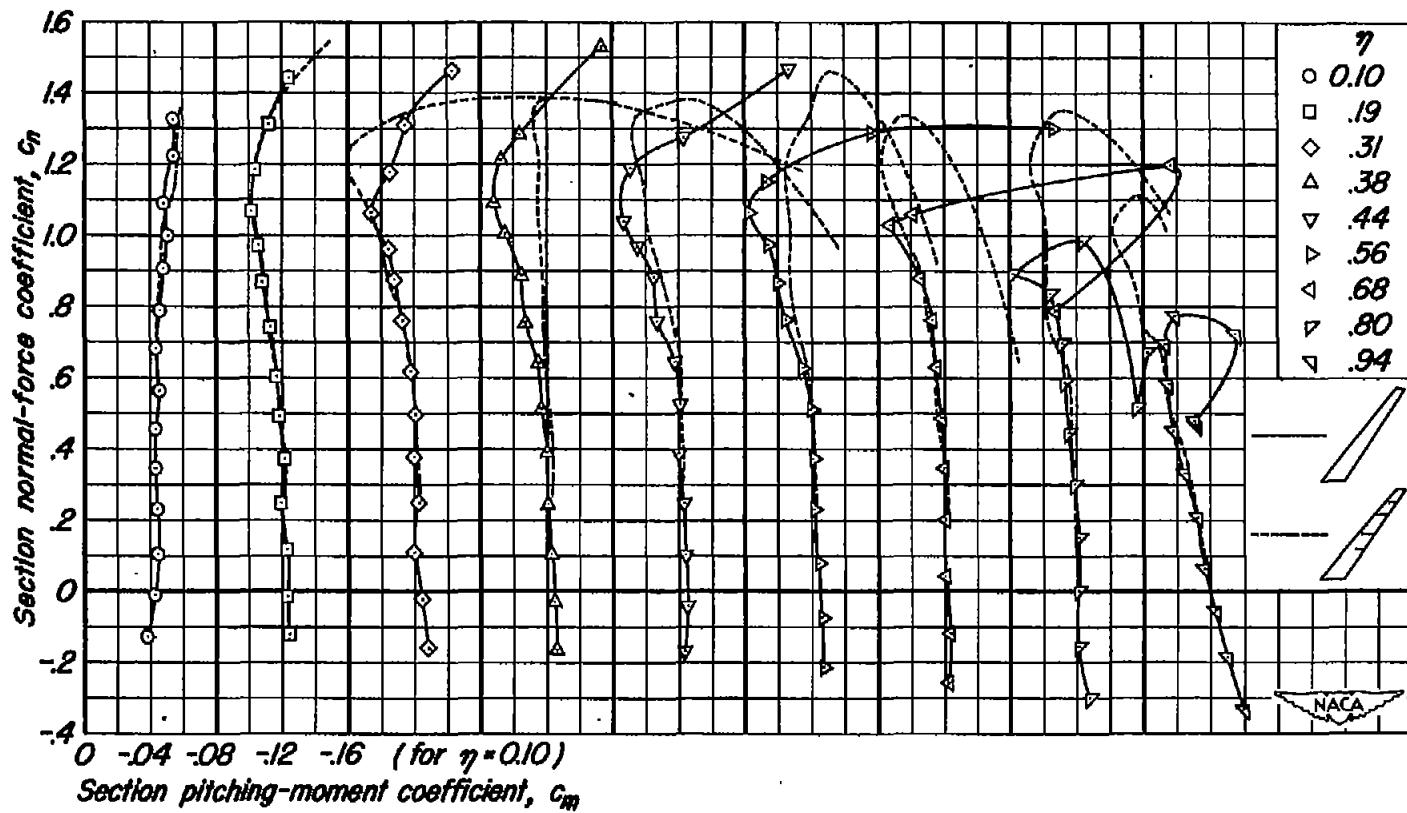
(a) Lift, drag, and pitching-moment characteristics.

Figure 11.—The lift, drag, and pitching-moment characteristics of the wing without fences and with four fences and the corresponding section normal-force and section pitching-moment characteristics at nine semispan stations of the wing. $M, 0.165$; $R, 8,000,000$.



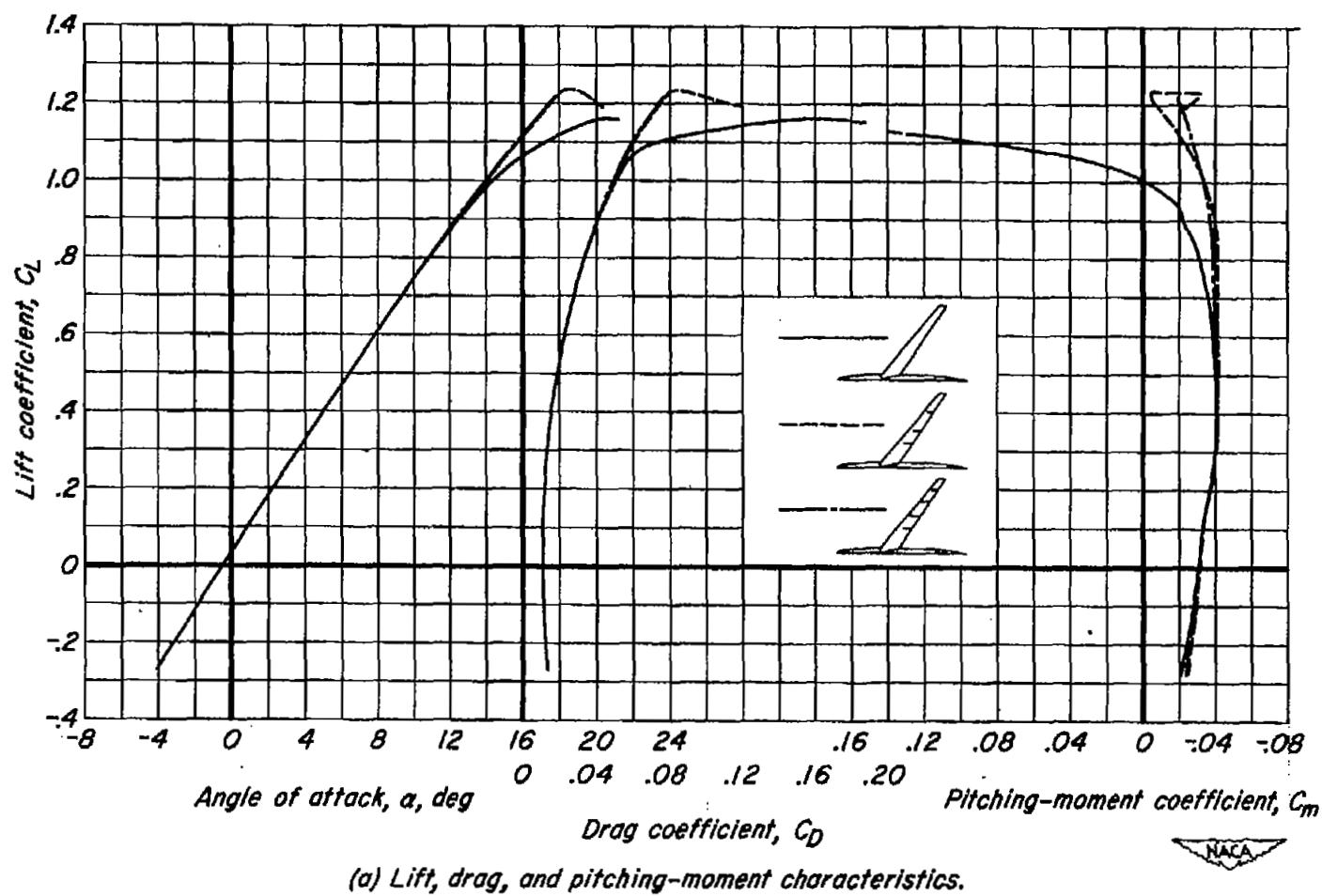
(b) Section normal-force characteristics.

Figure 11.-Continued.



(c) Section pitching-moment characteristics.

Figure 11.-Concluded.



(a) Lift, drag, and pitching-moment characteristics.

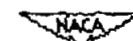
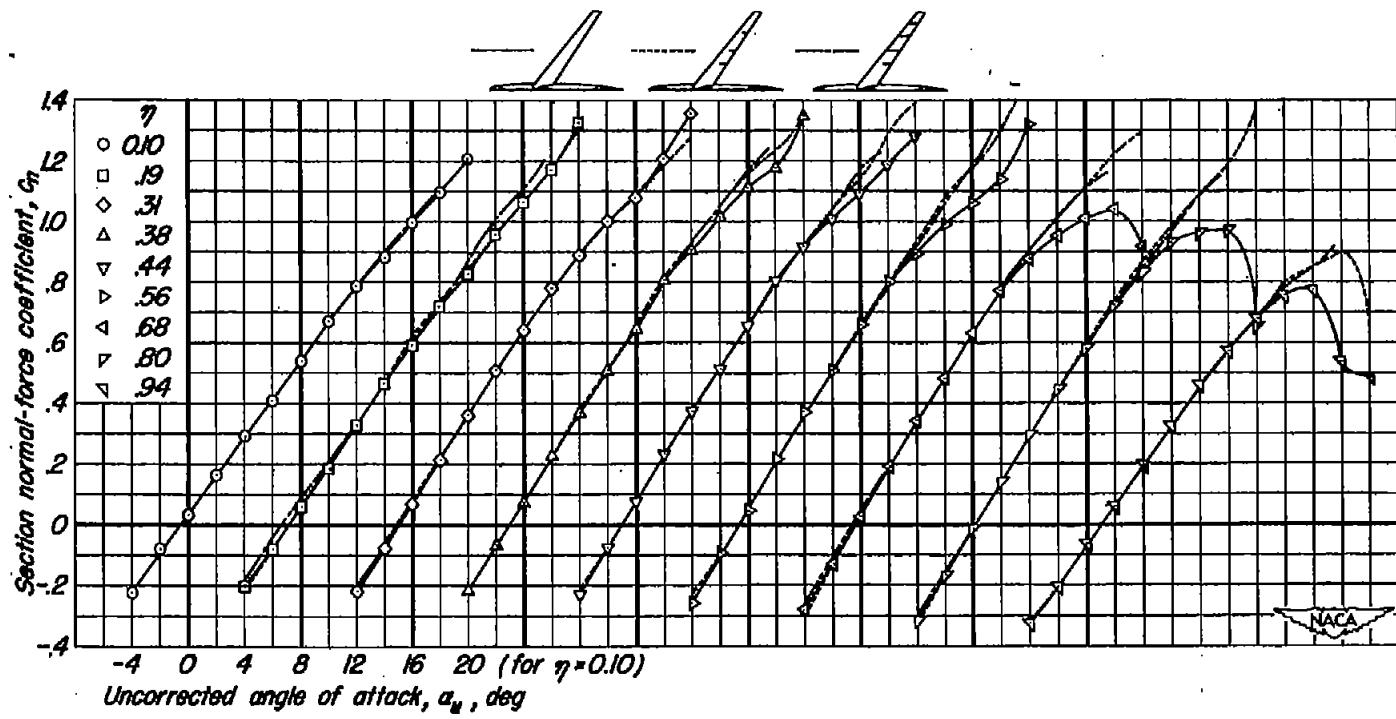
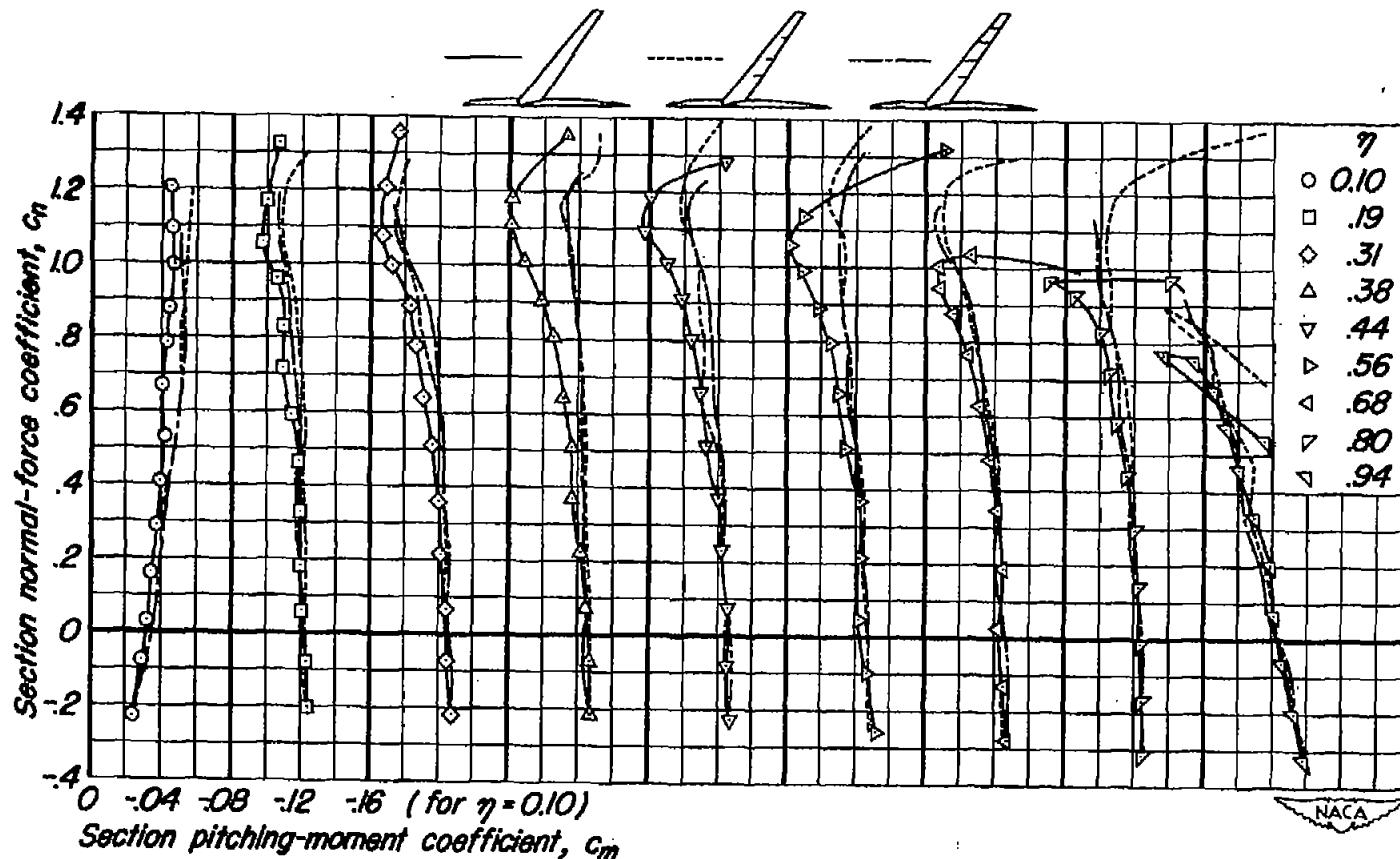


Figure 12.—The lift, drag, and pitching-moment characteristics of the wing-fuselage combination without fences, with three fences, and with four fences and the corresponding section normal-force and section pitching-moment characteristics at nine semispan stations of the wing. $M, 0.25$; $R, 8,000,000$.



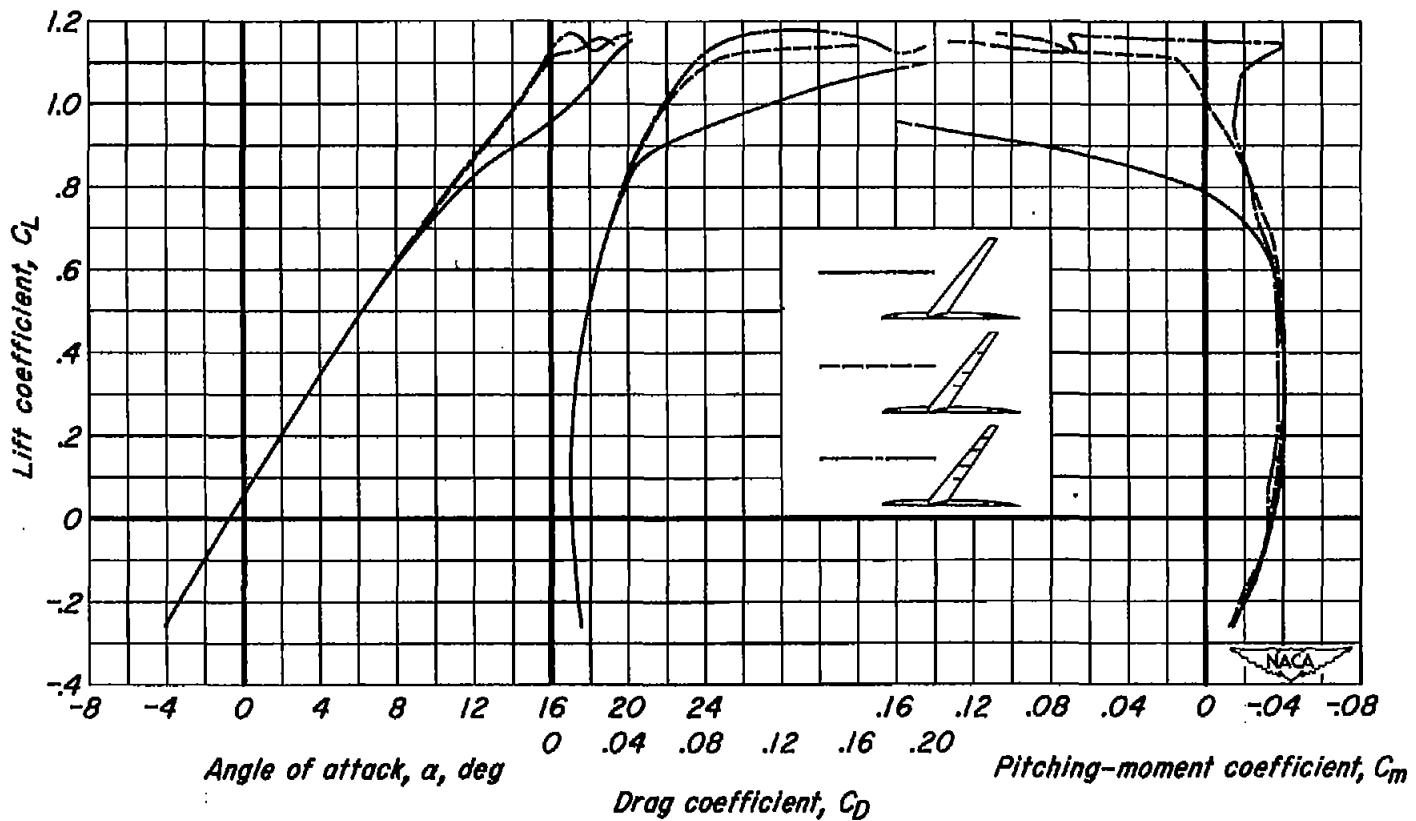
(b) Section normal-force characteristics.

Figure 12.-Continued.



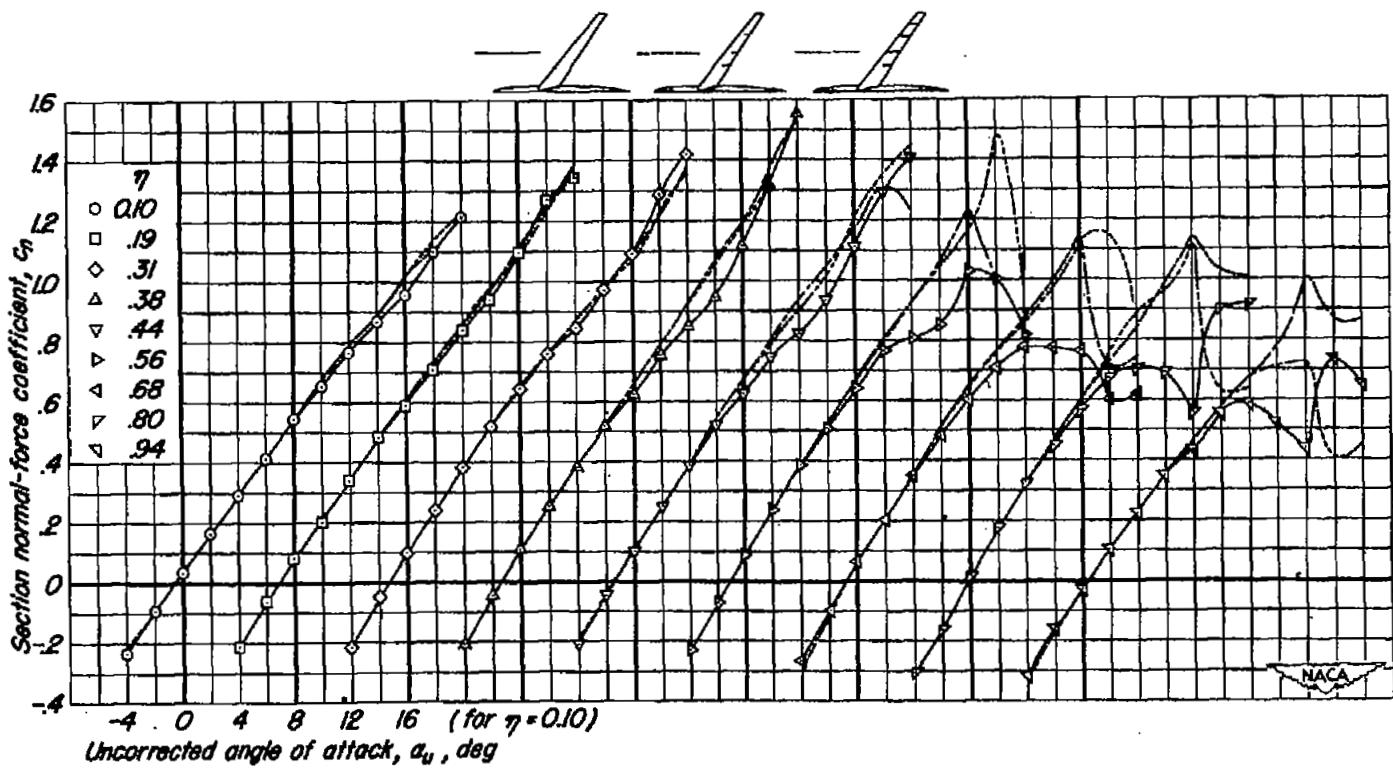
(c) Section pitching-moment characteristics.

Figure 12.-Concluded.



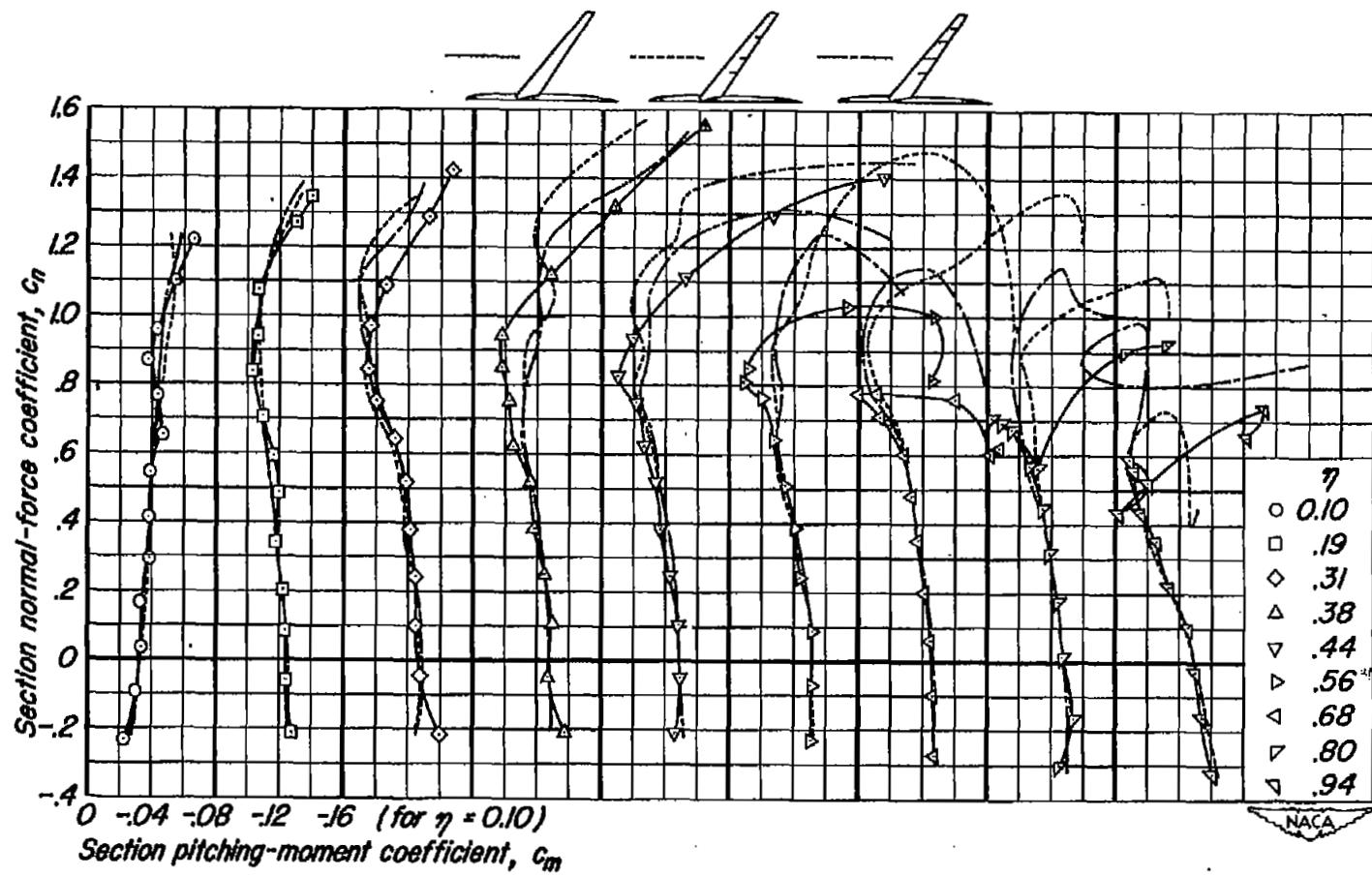
(a) Lift, drag, and pitching-moment characteristics.

Figure 13.—The lift, drag, and pitching-moment characteristics of the wing-fuselage combination without fences, with three fences, and with four fences and the corresponding section normal-force and section pitching-moment characteristics at nine semispan stations of the wing. $M, 0.25$; $R, 2,000,000$.



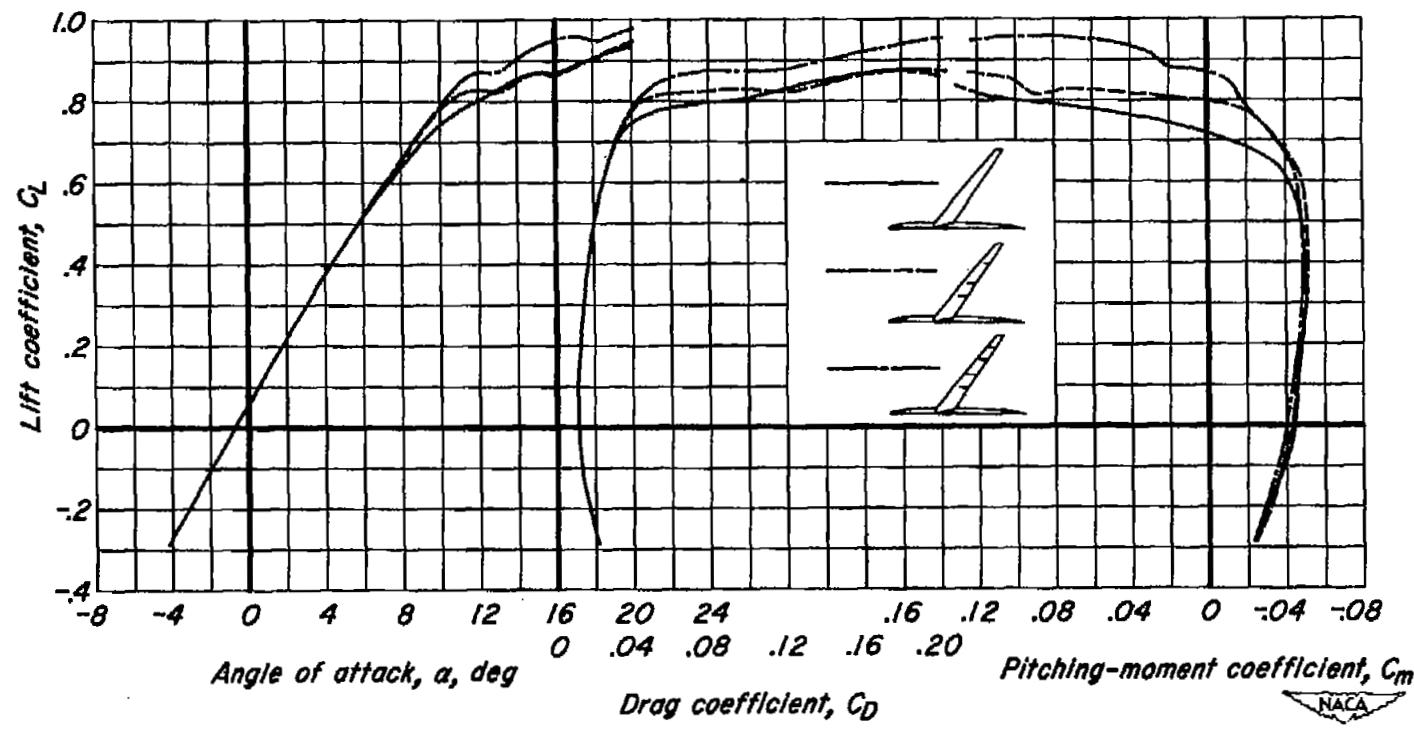
(b) Section normal-force characteristics.

Figure 13.-Continued.



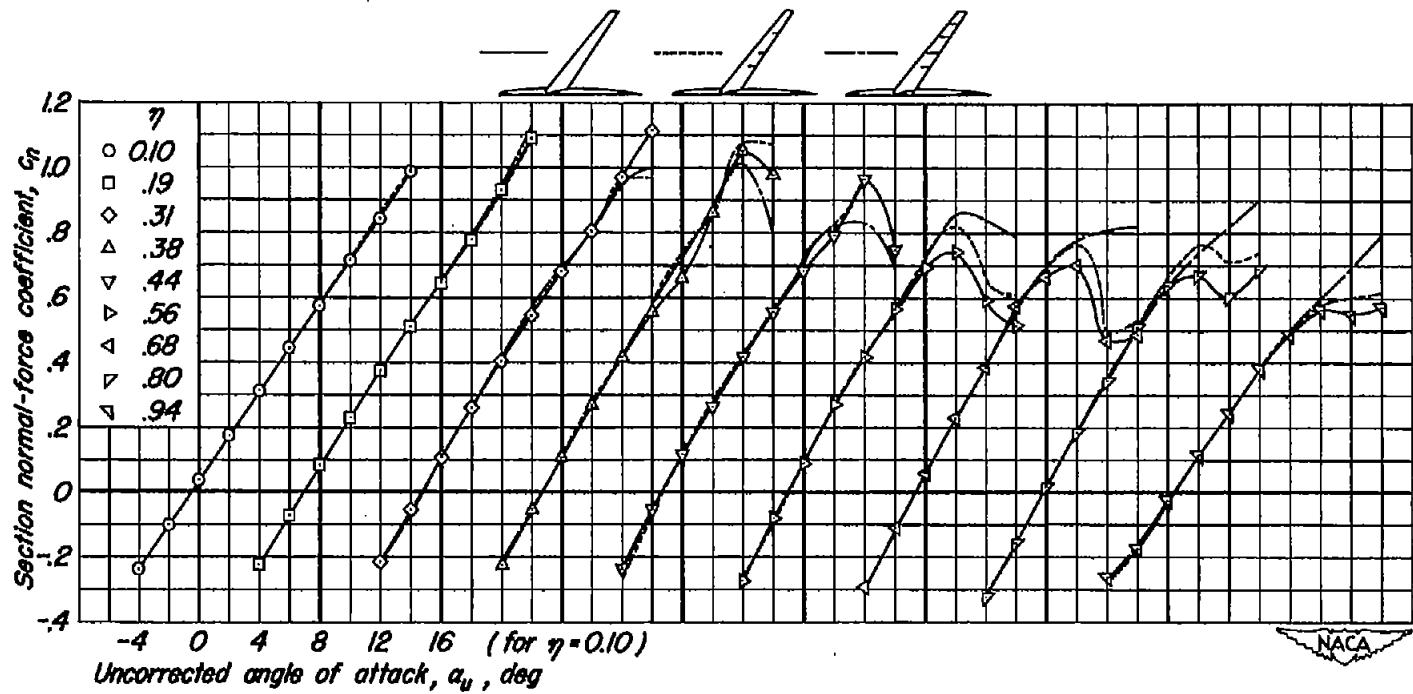
(c) Section pitching-moment characteristics.

Figure 13.—Concluded.



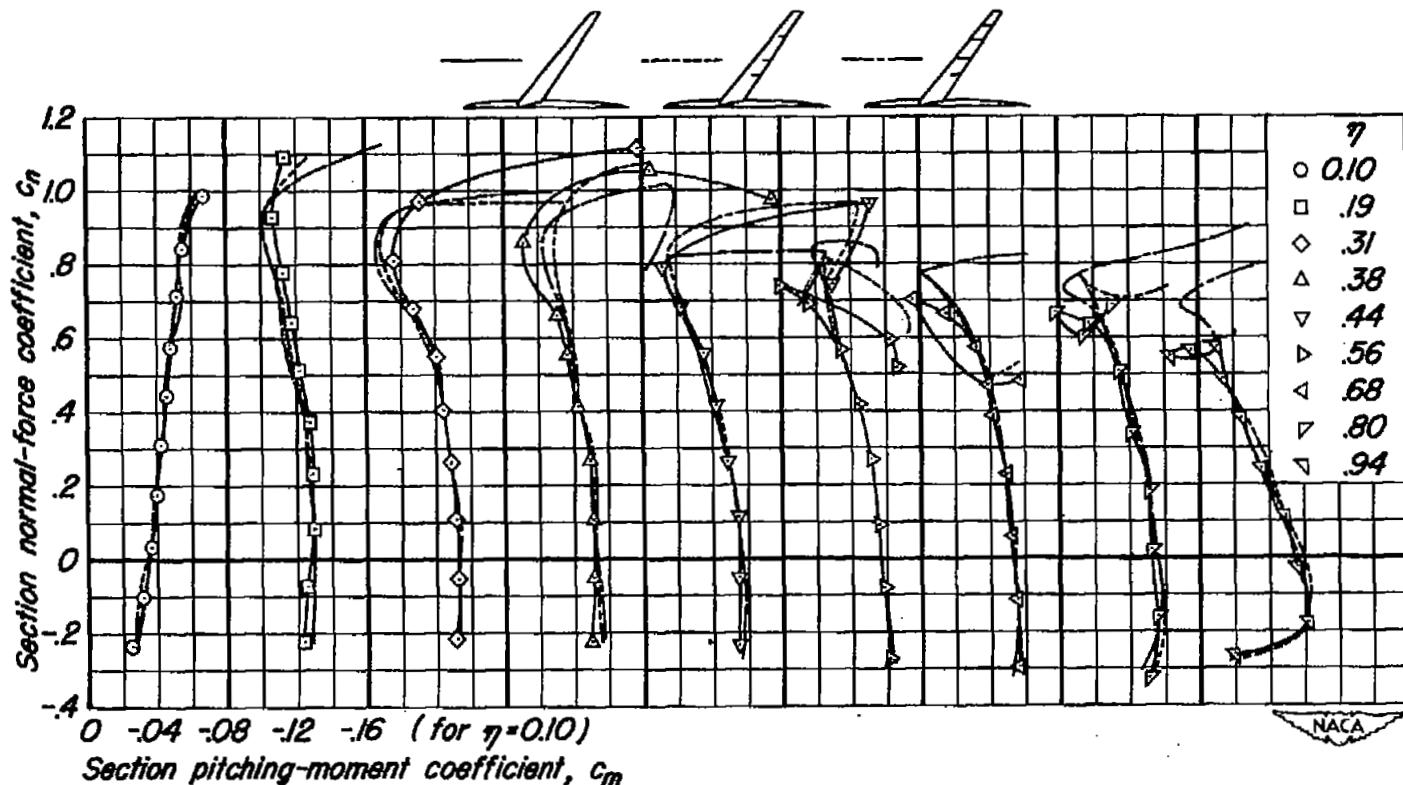
(a) Lift, drag, and pitching-moment characteristics.

Figure 14.—The lift, drag, and pitching-moment characteristics of the wing-fuselage combination without fences, with three fences, and with four fences and the corresponding section normal-force and section pitching-moment characteristics at nine semispan stations of the wing. $M, 0.60$; $R, 2,000,000$.



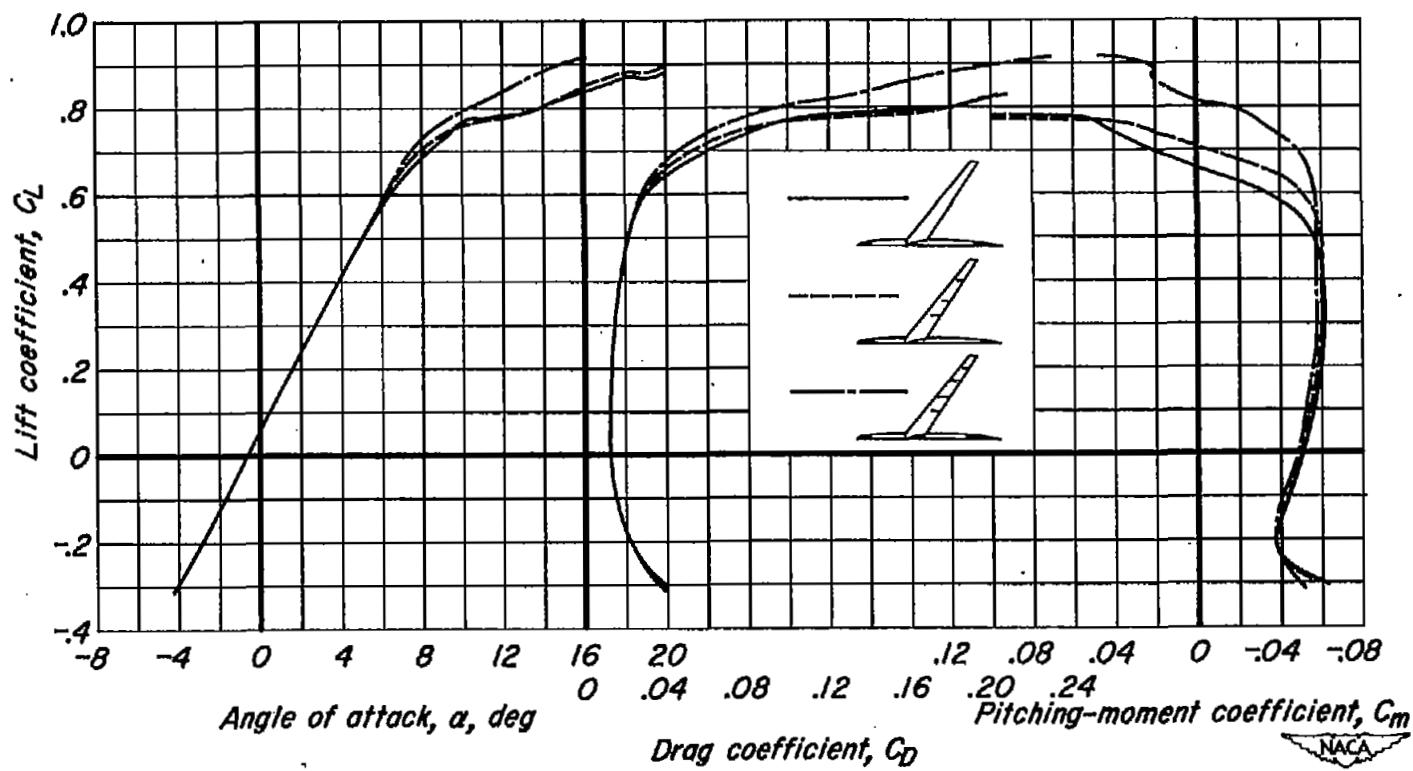
(b) Section normal-force characteristics.

Figure 14.-Continued.



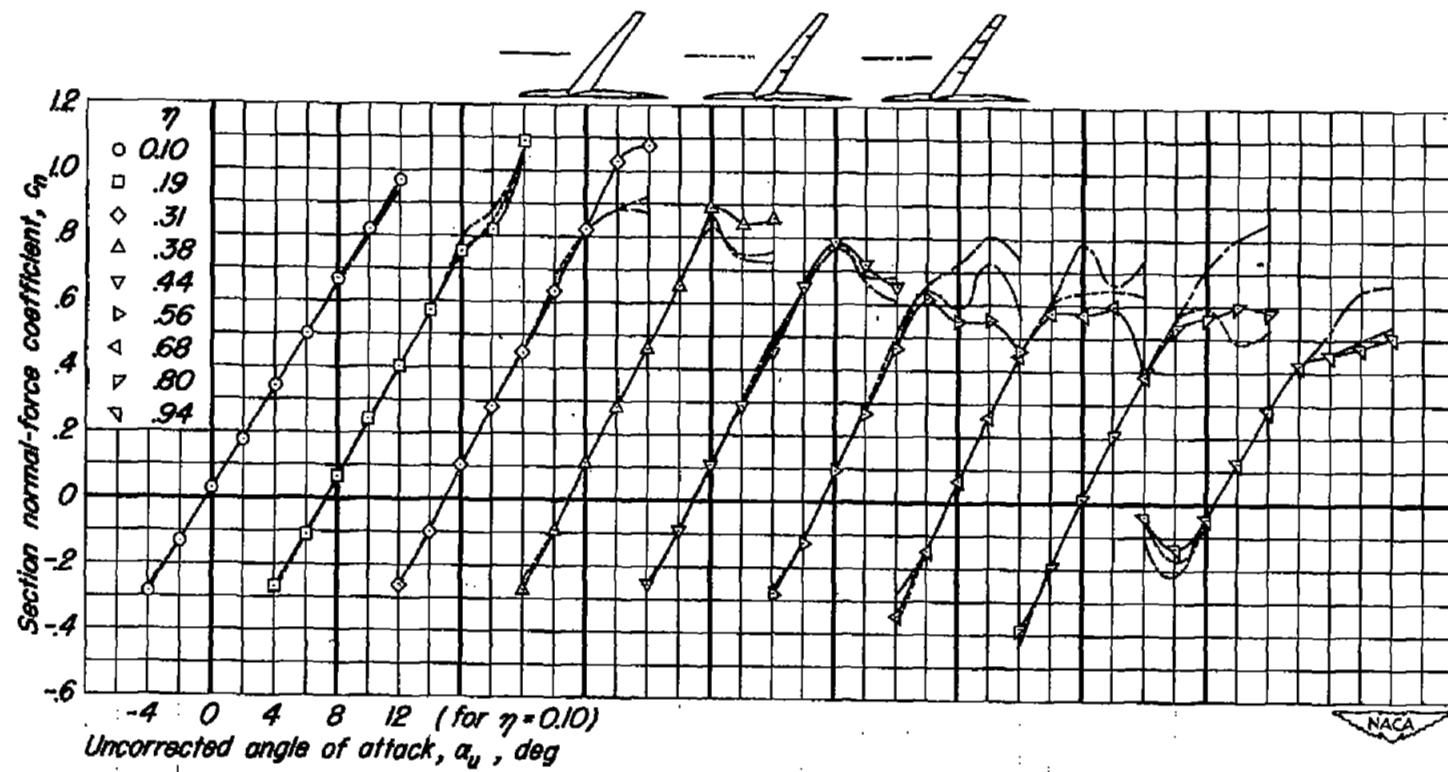
(c) Section pitching-moment characteristics.

Figure 14.-Concluded.



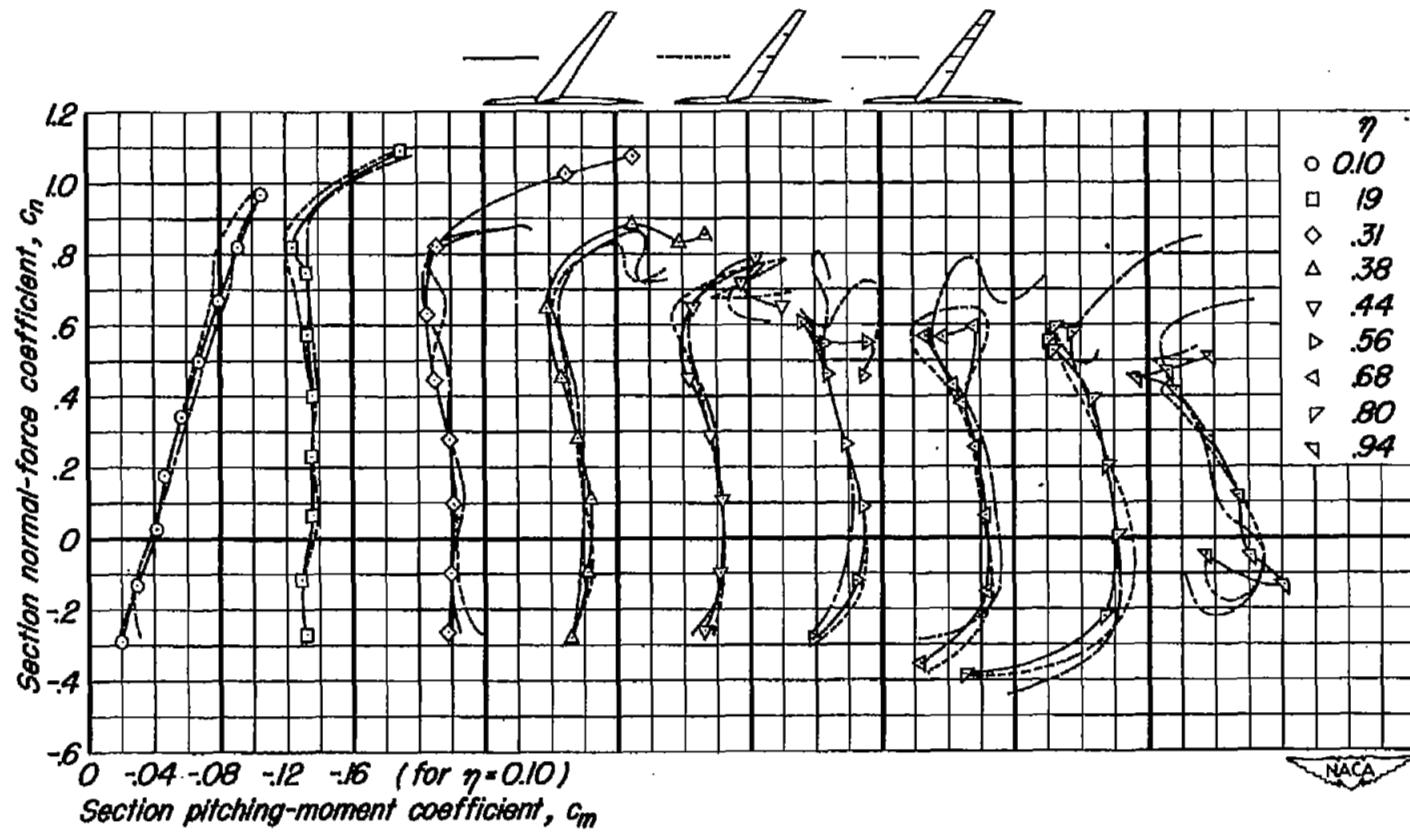
(a) Lift, drag, and pitching-moment characteristics.

Figure 15.—The lift, drag, and pitching-moment characteristics of the wing-fuselage combination without fences, with three fences, and with four fences and the corresponding section normal-force and section pitching-moment characteristics at nine semispan stations of the wing.
 $M = 0.80$; $R = 2,000,000$.



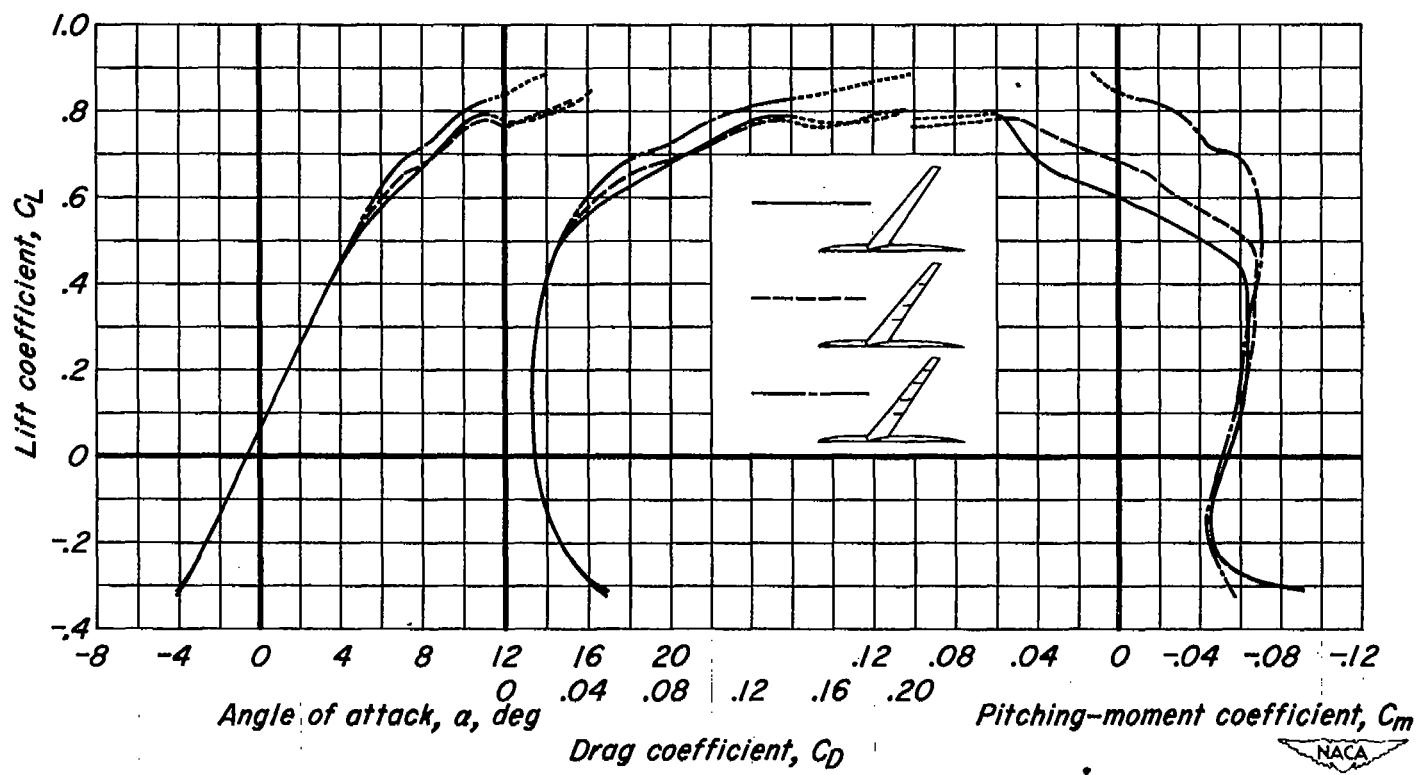
(b) Section normal-force characteristics.

Figure 15.-Continued.



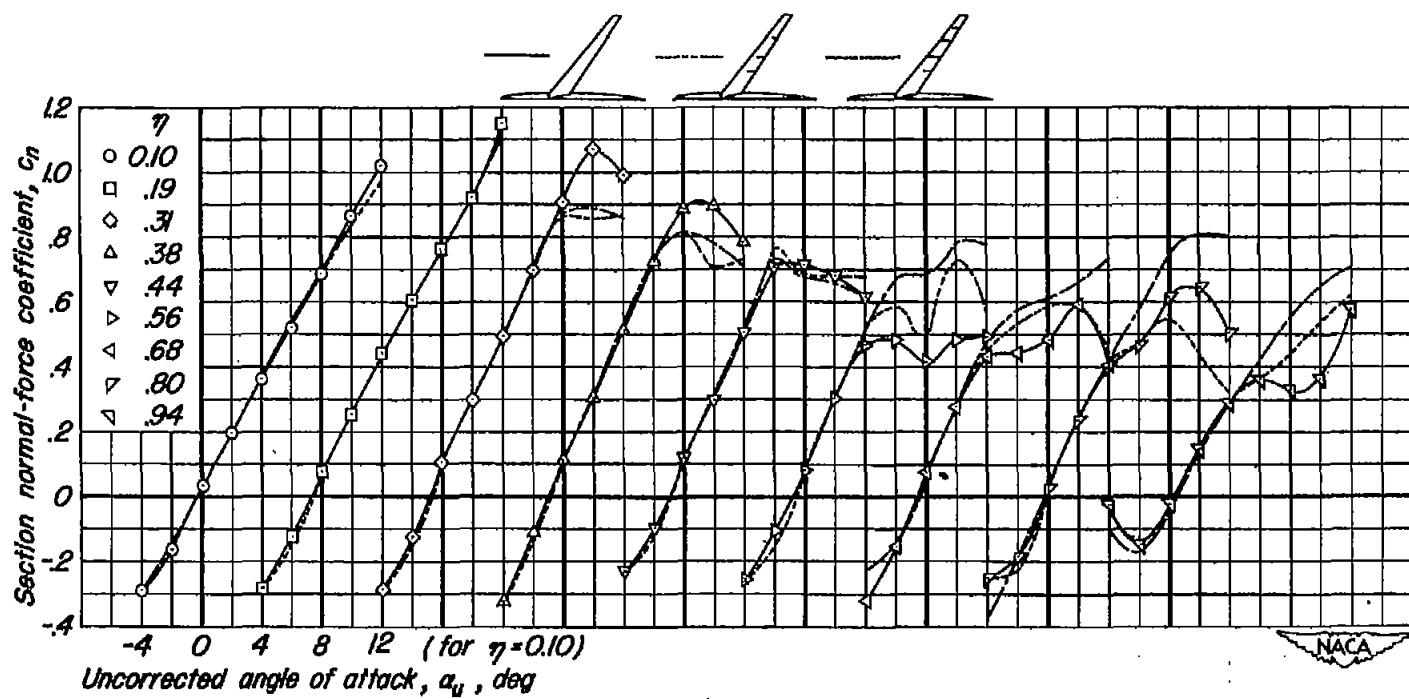
(c) Section pitching-moment characteristics.

Figure 15.—Concluded.



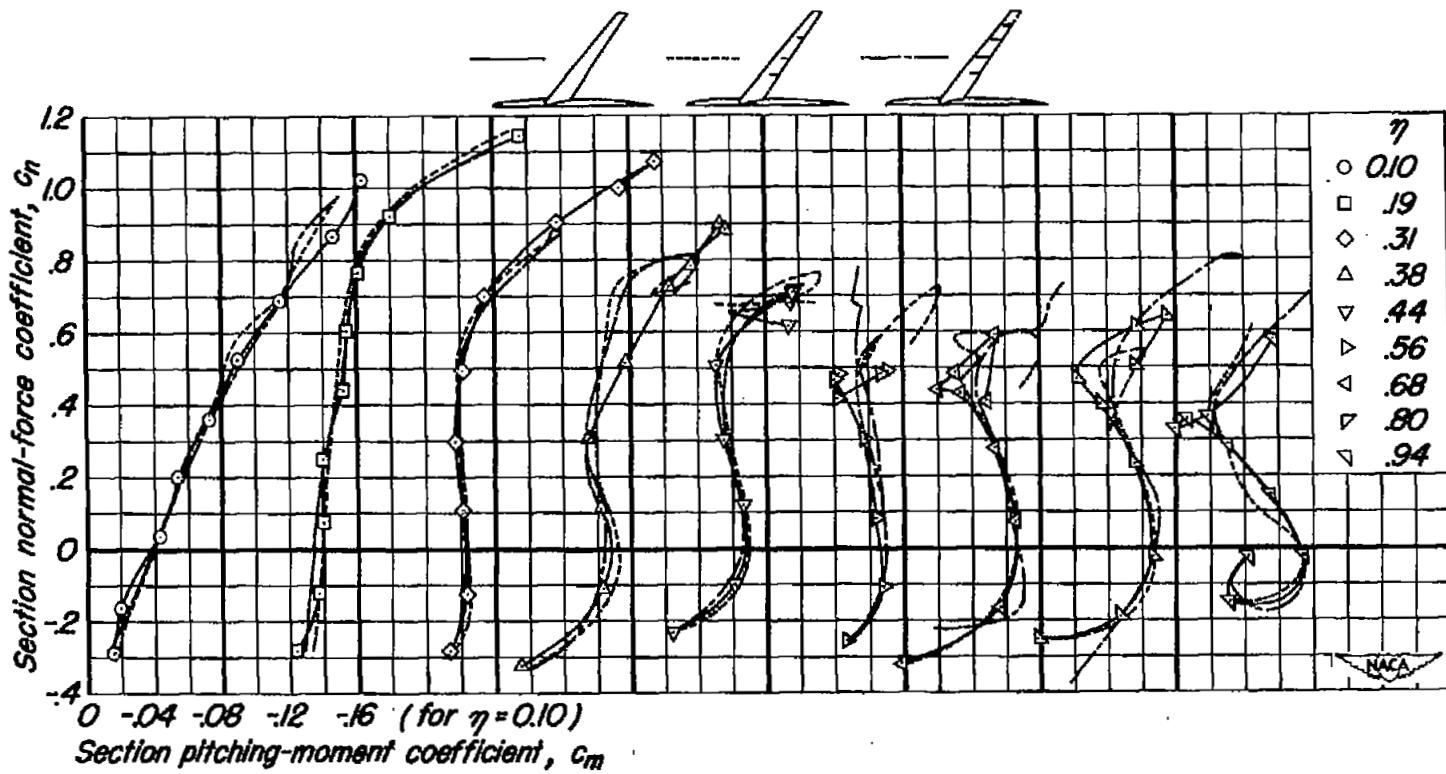
(a) Lift, drag, and pitching-moment characteristics.

Figure 16.—The lift, drag, and pitching-moment characteristics of the wing-fuselage combination without fences, with three fences, and with four fences and the corresponding section normal-force and section pitching-moment characteristics at nine semispan stations of the wing.
 M , 0.86; R , 2,000,000.



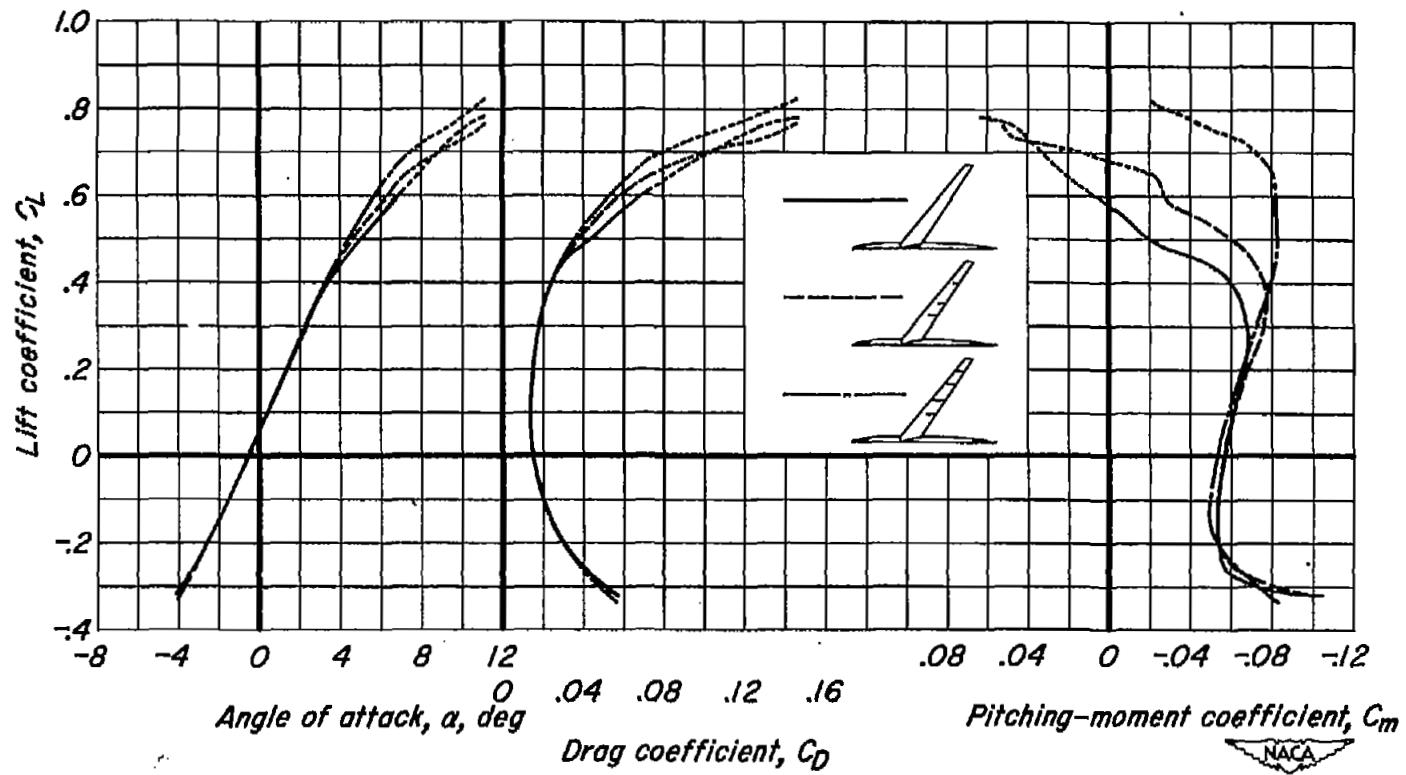
(b) Section normal-force characteristics.

Figure 16.—Continued.



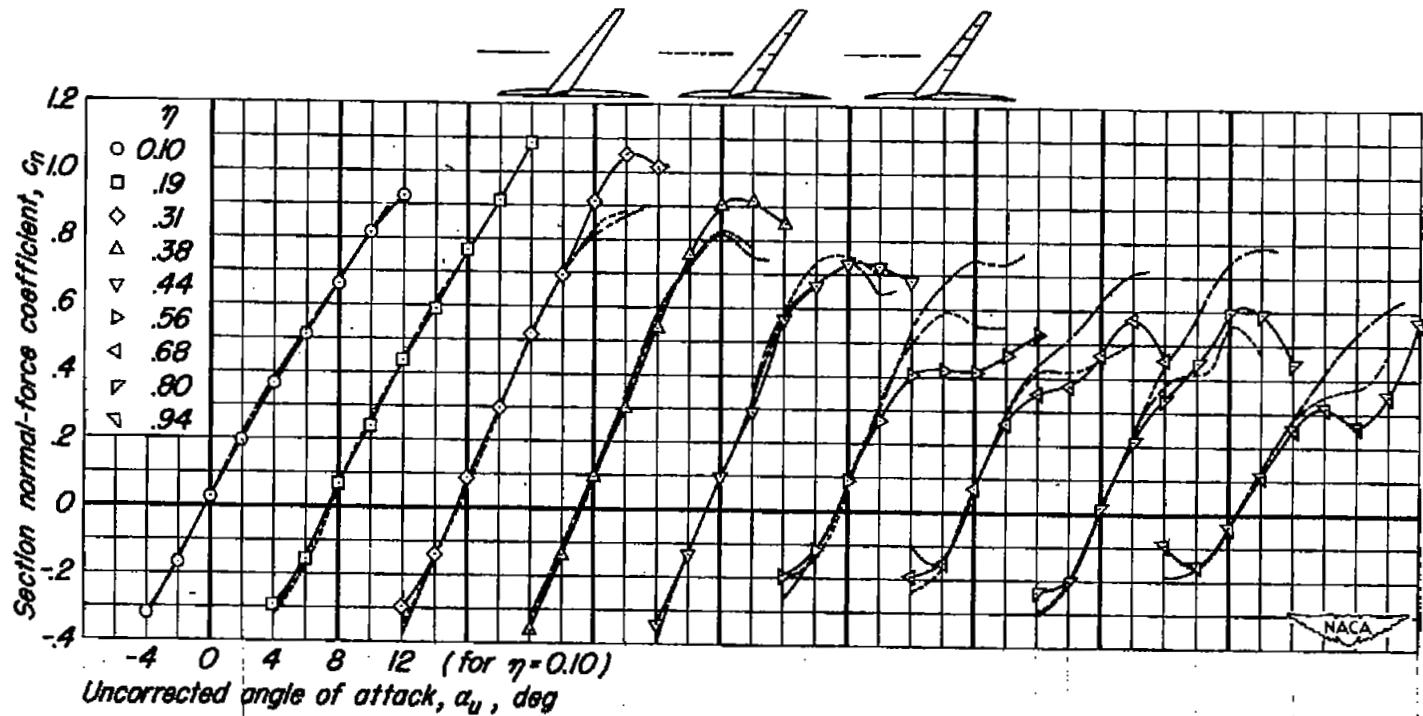
(c) Section pitching-moment characteristics.

Figure 16.-Concluded.



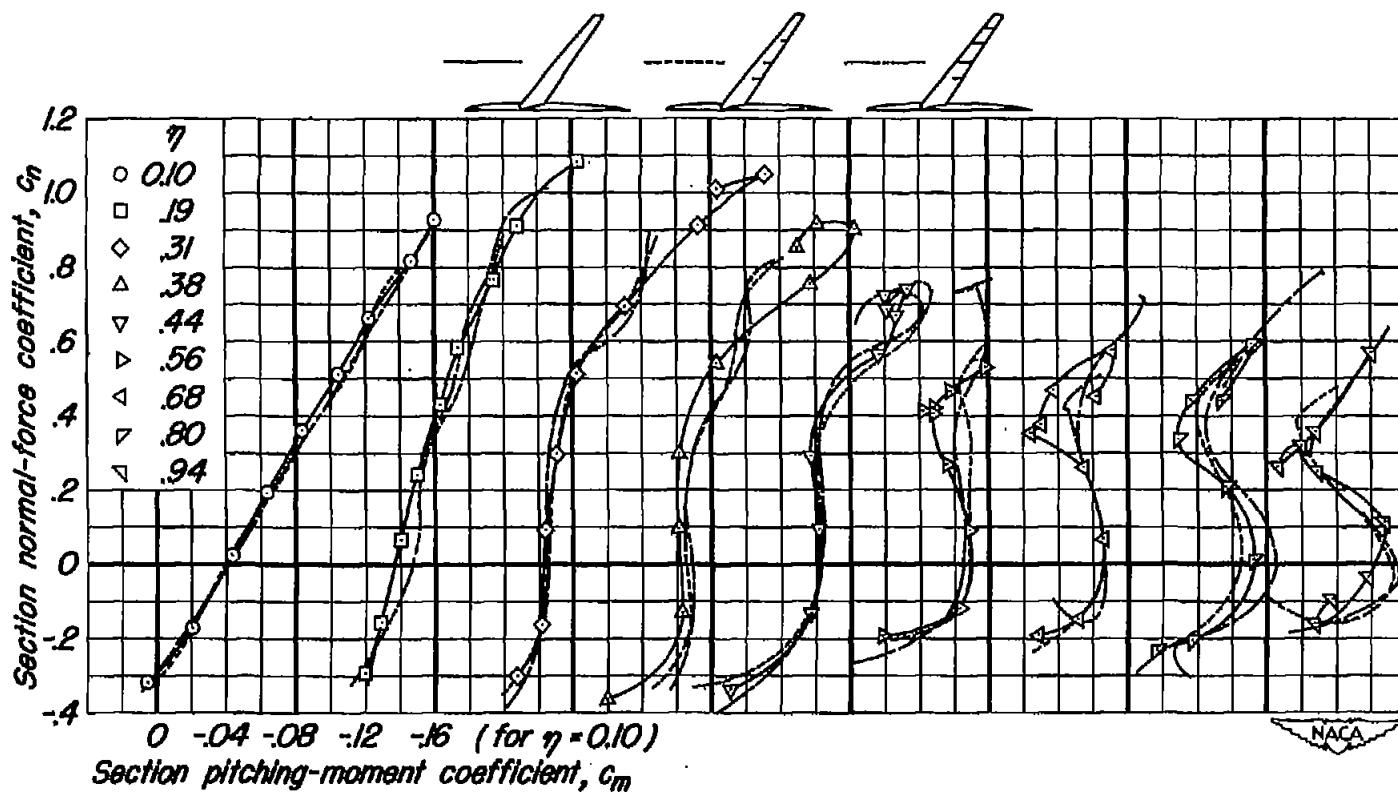
(a) Lift, drag, and pitching-moment characteristics.

Figure 17.-The lift, drag, and pitching-moment characteristics of the wing-fuselage combination without fences, with three fences, and with four fences and the corresponding section normal-force and section pitching-moment characteristics at nine semispan stations of the wing.
 $M, 0.90; R, 2,000,000$.



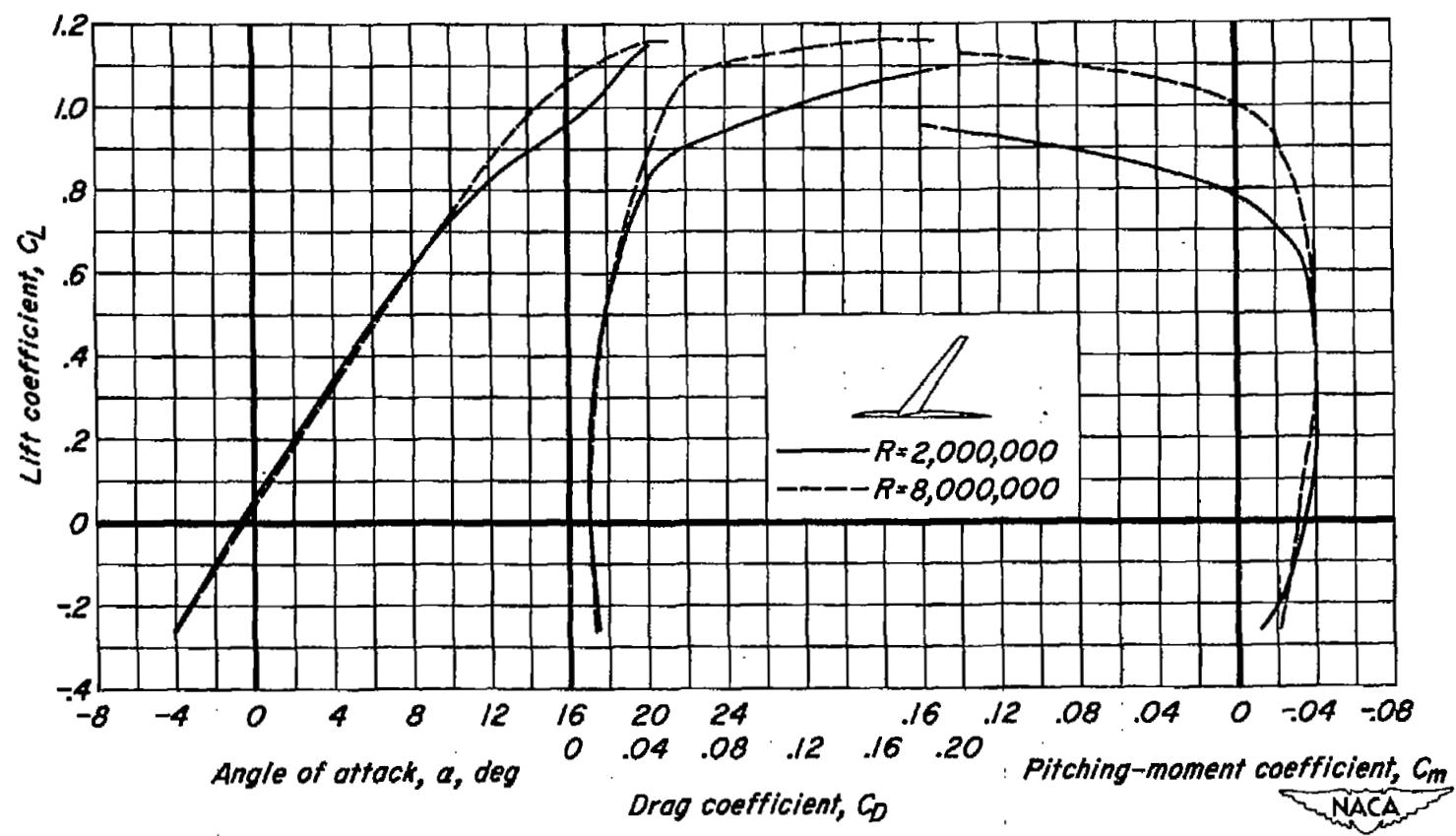
(b) Section normal-force characteristics.

Figure 17.—Continued.



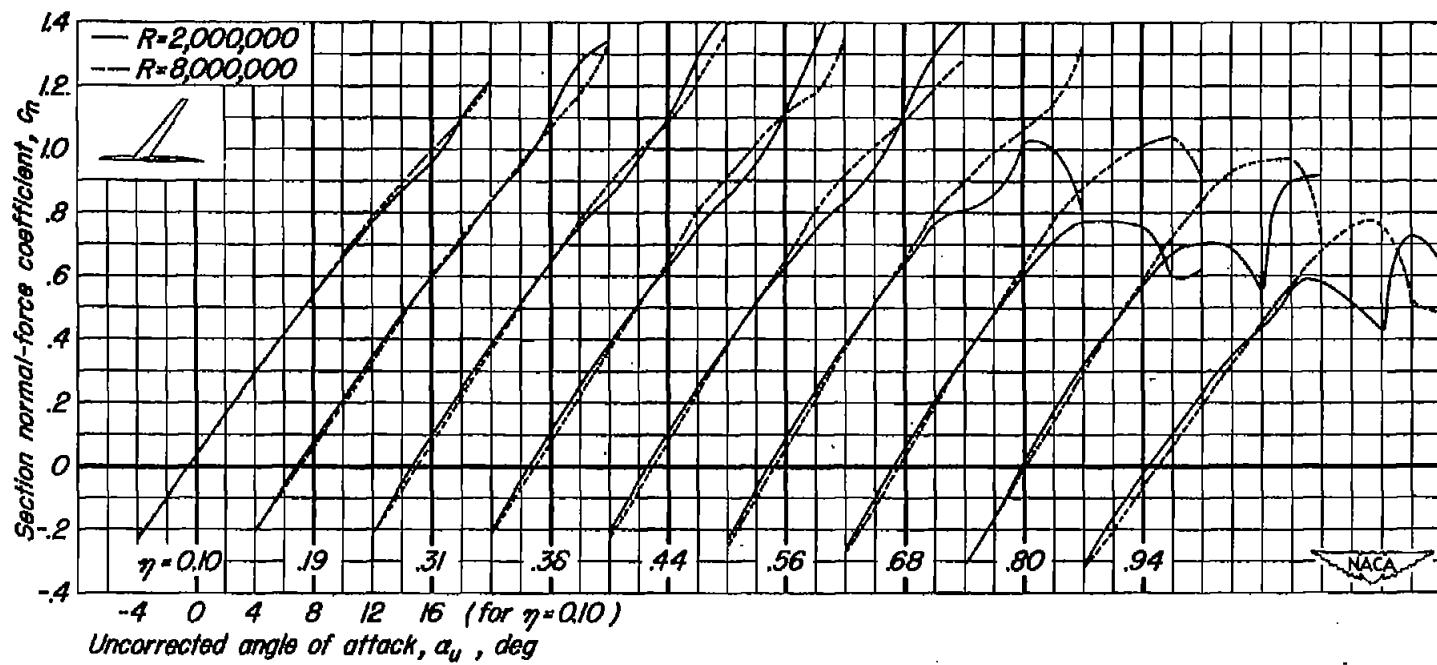
(c) Section pitching-moment characteristics.

Figure 17.—Concluded.



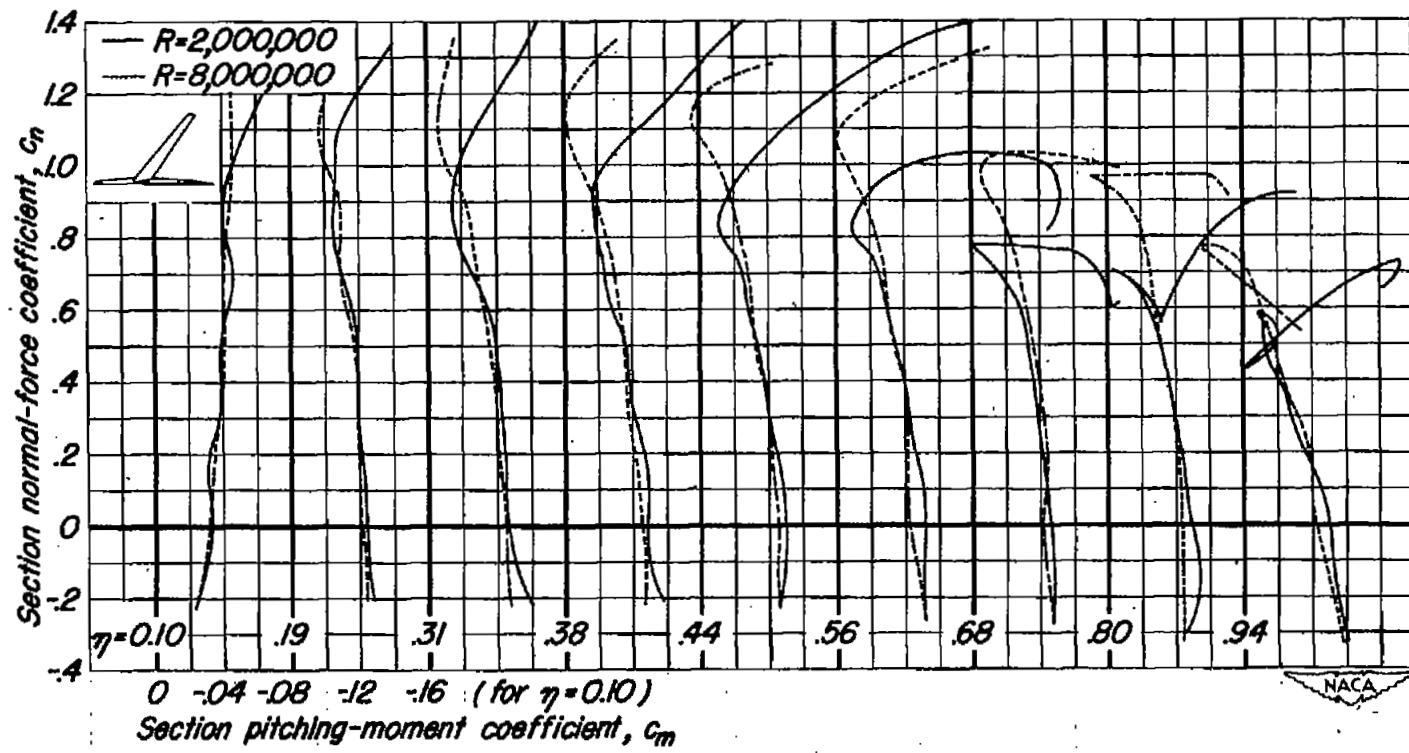
(a) Lift, drag, and pitching-moment characteristics.

Figure 18.—The lift, drag, and pitching-moment characteristics of the wing-fuselage combination and the corresponding section normal-force and section pitching-moment characteristics at nine semispan stations of the wing at Reynolds numbers of 2,000,000 and 8,000,000. $M = 0.25$.



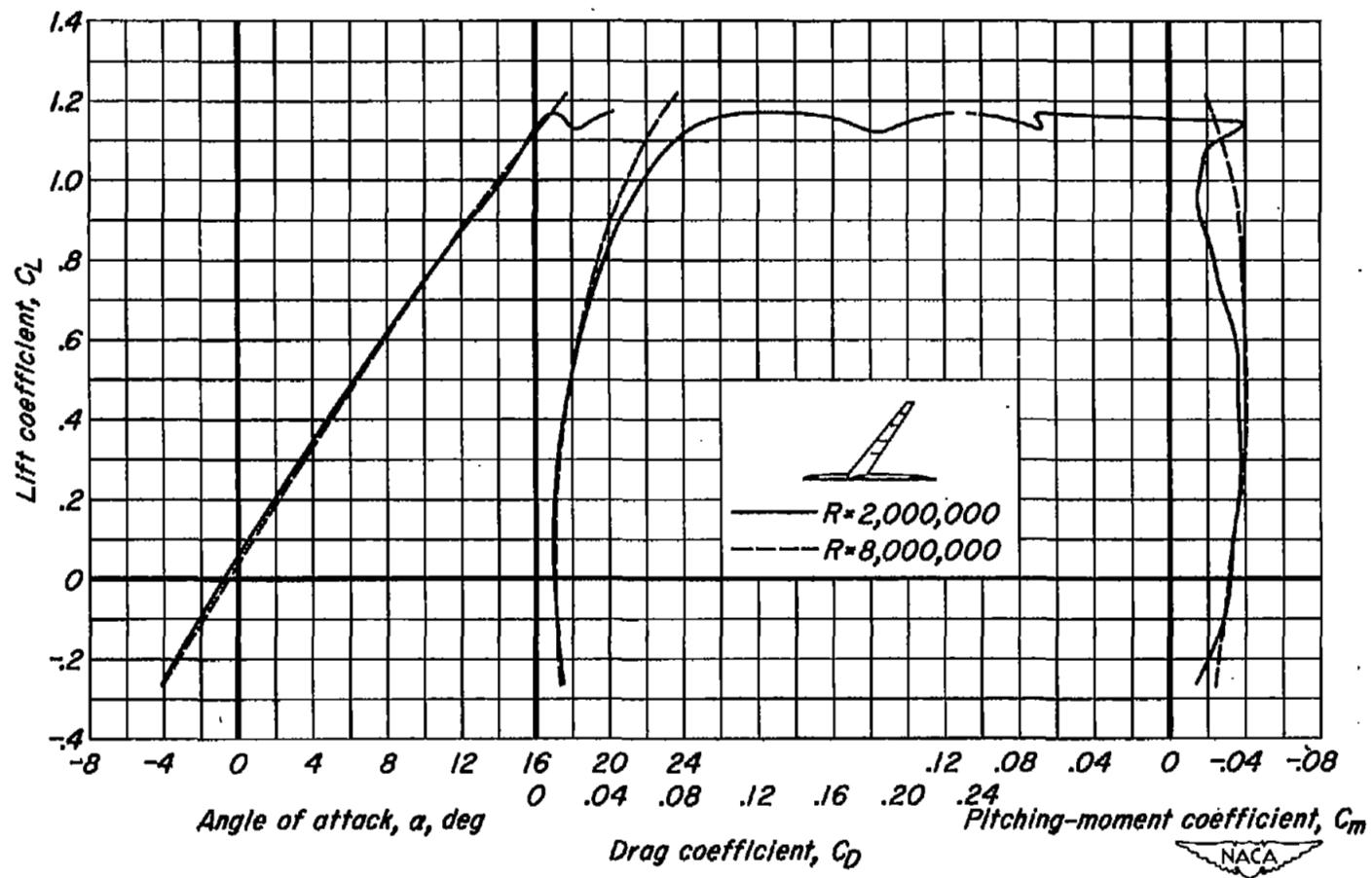
(b) Section normal-force characteristics.

Figure 18.-Continued.



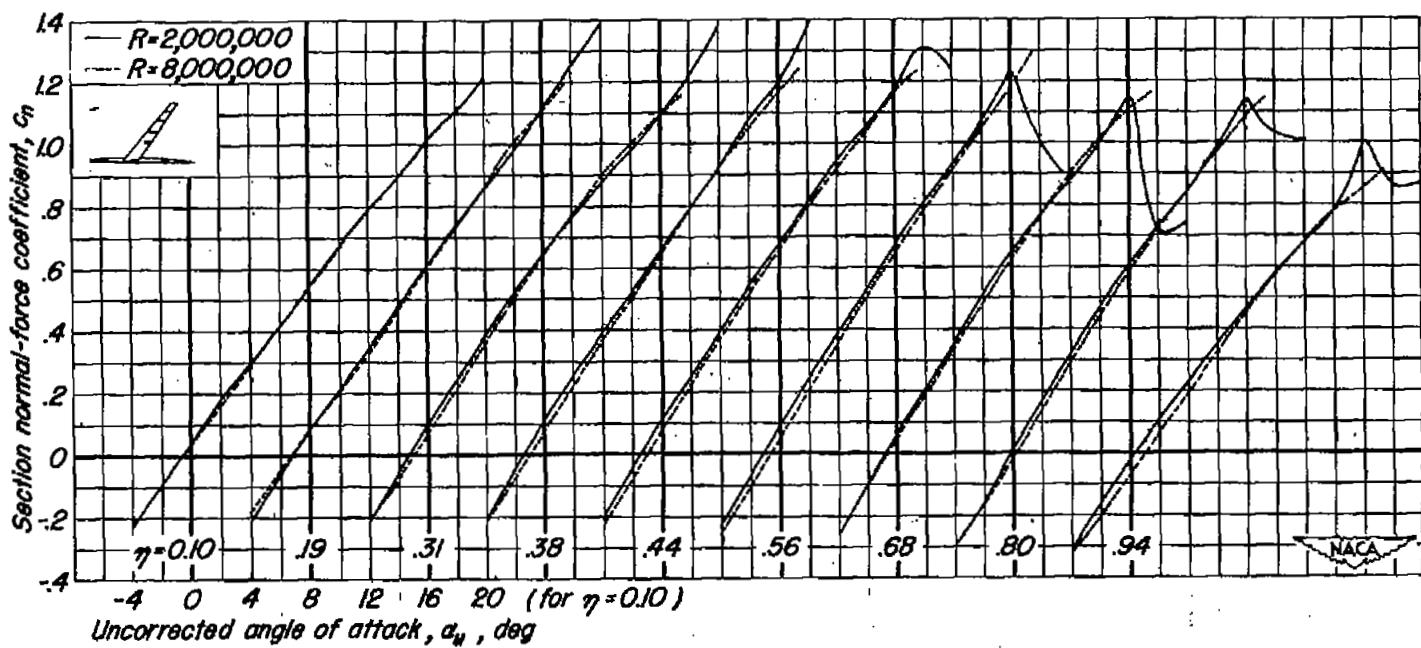
(c) Section pitching-moment characteristics.

Figure 18.-Concluded.



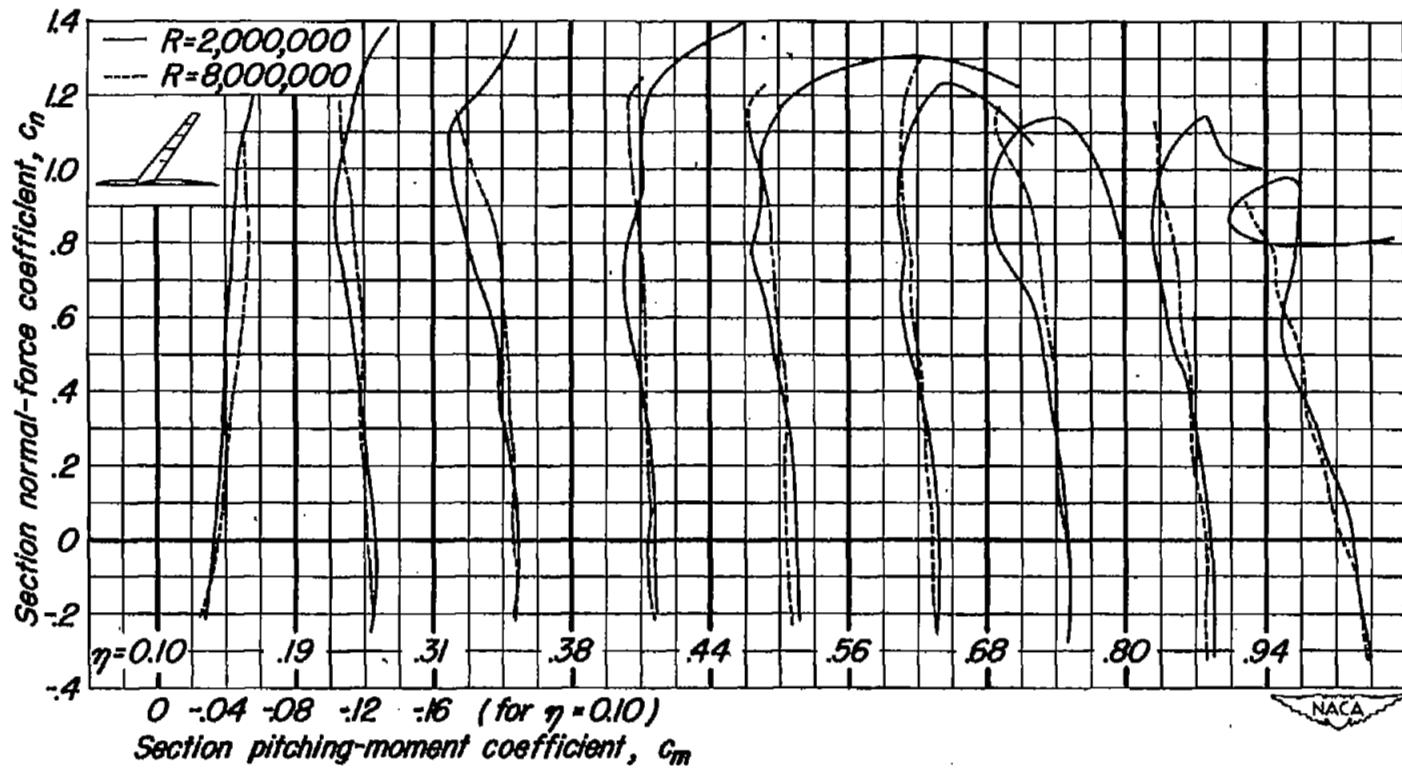
(a) Lift, drag, and pitching-moment characteristics.

Figure 19.-The lift, drag, and pitching-moment characteristics of the wing-fuselage combination with four fences and the corresponding section normal-force and section pitching-moment characteristics at nine semispan stations of the wing at Reynolds numbers of 2,000,000 and 8,000,000. M, 0.25.



(b) Section normal-force characteristics.

Figure 19.-Continued.



(c) Section pitching-moment characteristics.

Figure 19.—Concluded.

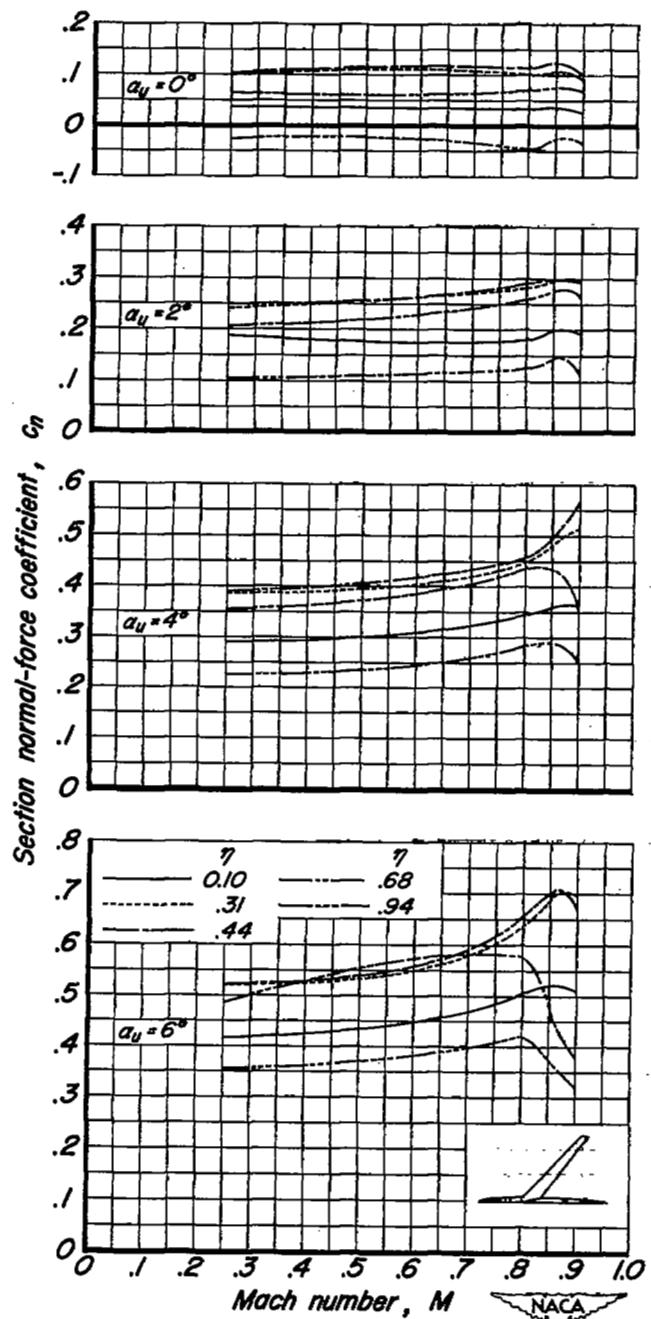


Figure 20.-The variation with Mach number of the section normal-force coefficients of the wing-fuselage combination for several angles of attack. R, 2,000,000.

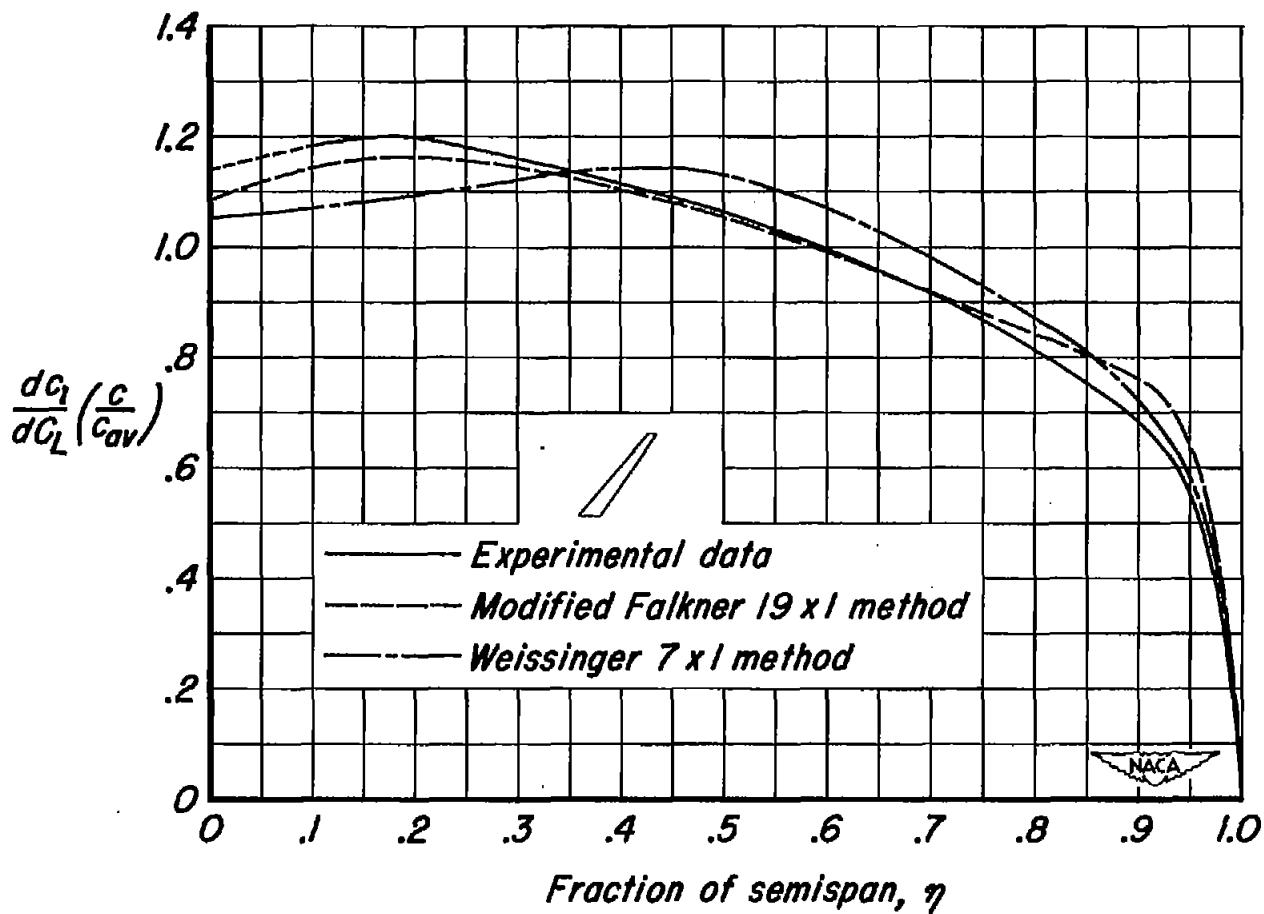


Figure 21.- A comparison of the experimental and theoretical spanwise distributions of additional loading for the wing alone. $M, 0.165$; $R, 8,000,000$.

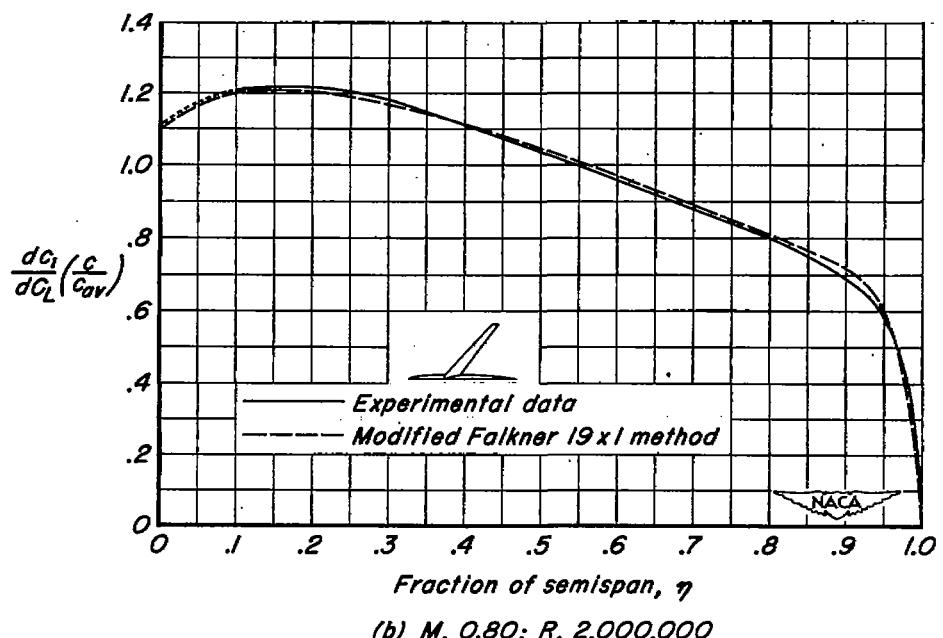
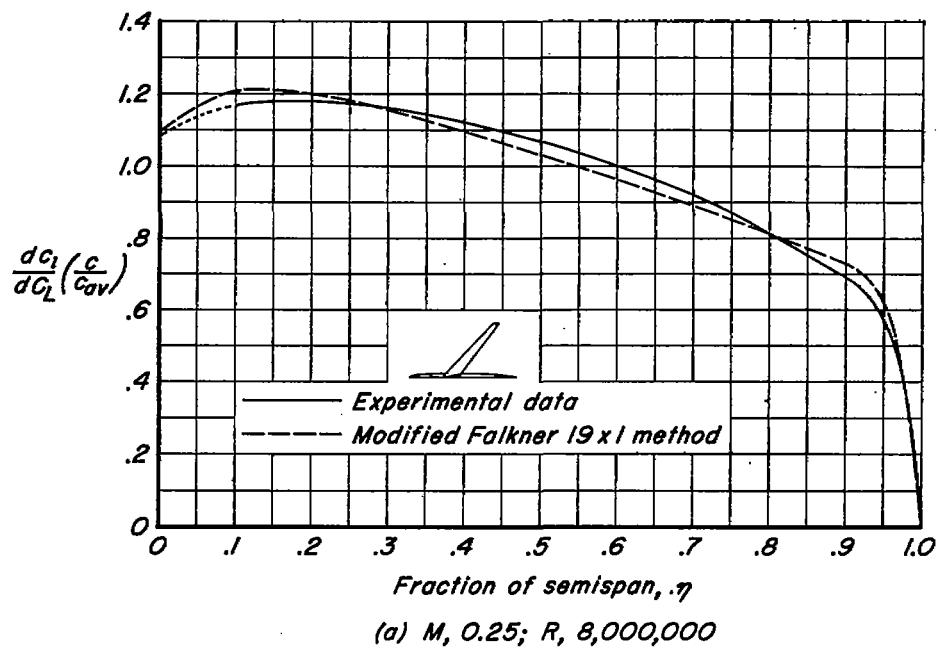


Figure 22.—A comparison of the experimental and theoretical spanwise distributions of additional loading for the wing-fuselage combination at Mach numbers of 0.25 and 0.80.

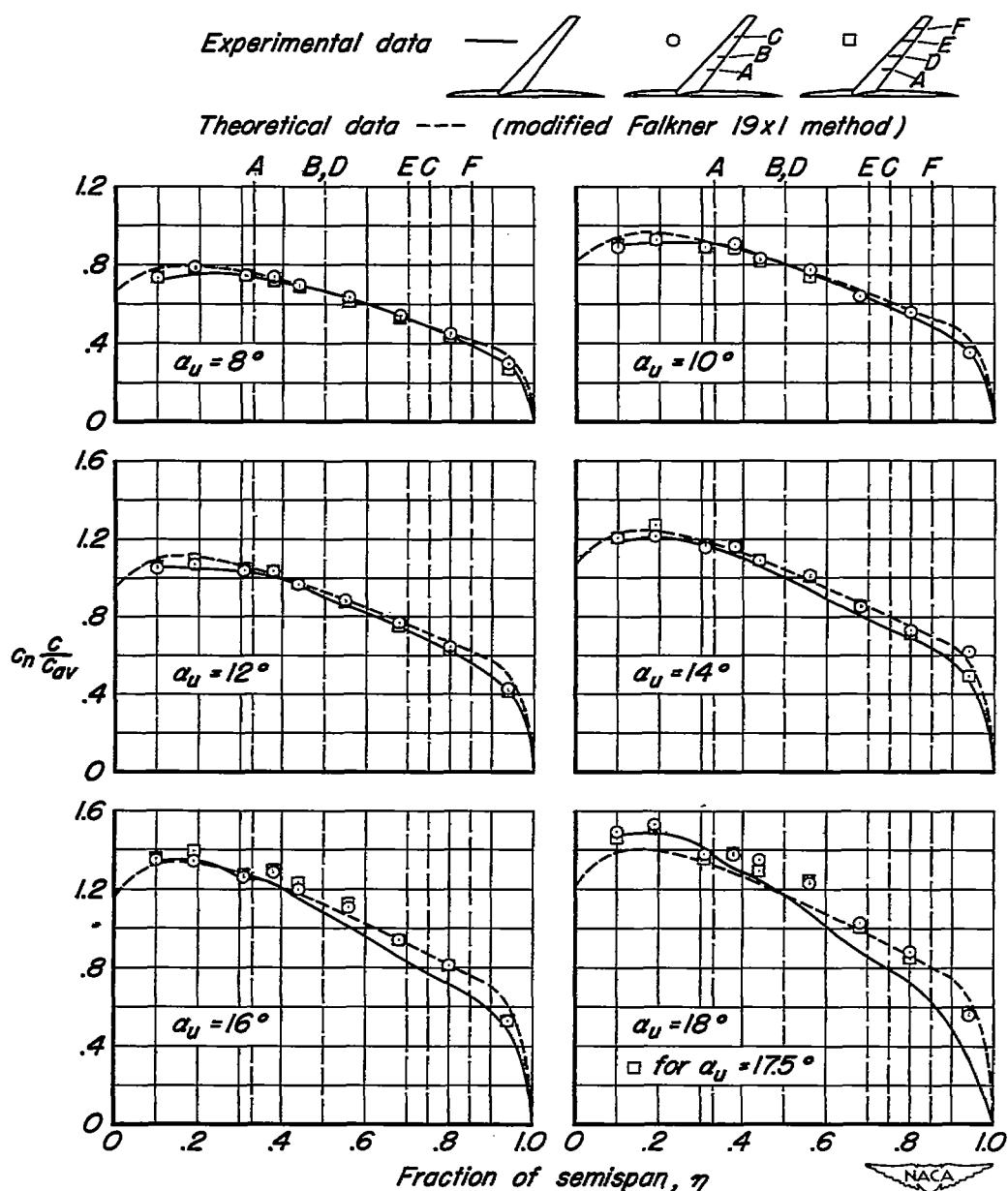
(a) $M, 0.25; R, 8,000,000$

Figure 23-The spanwise distribution of $c_n \frac{C}{C_{av}}$ for the wing-fuselage combination without fences, with three fences, and with four fences.

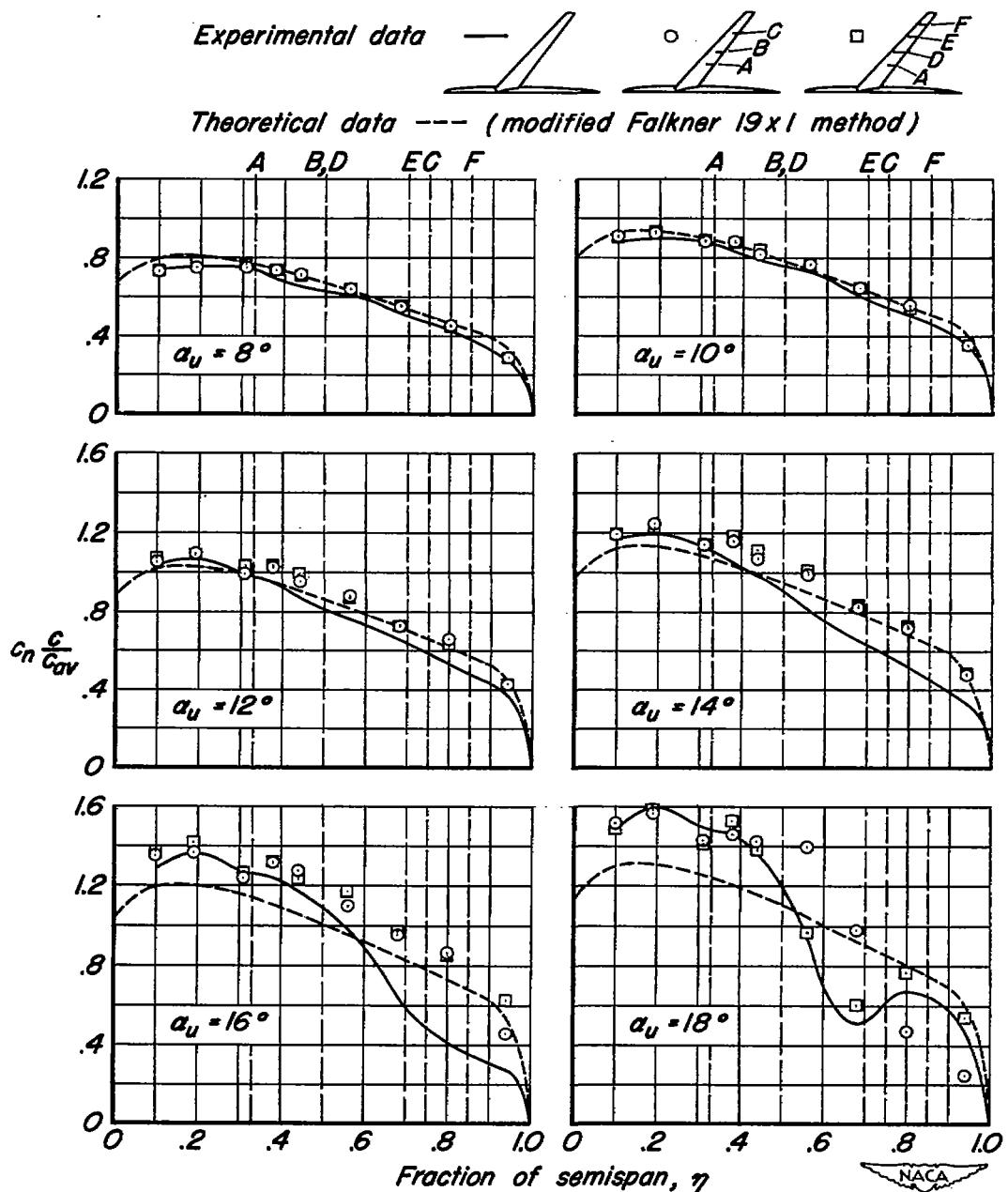
(b) $M, 0.25$; $R, 2,000,000$

Figure 23-Continued.

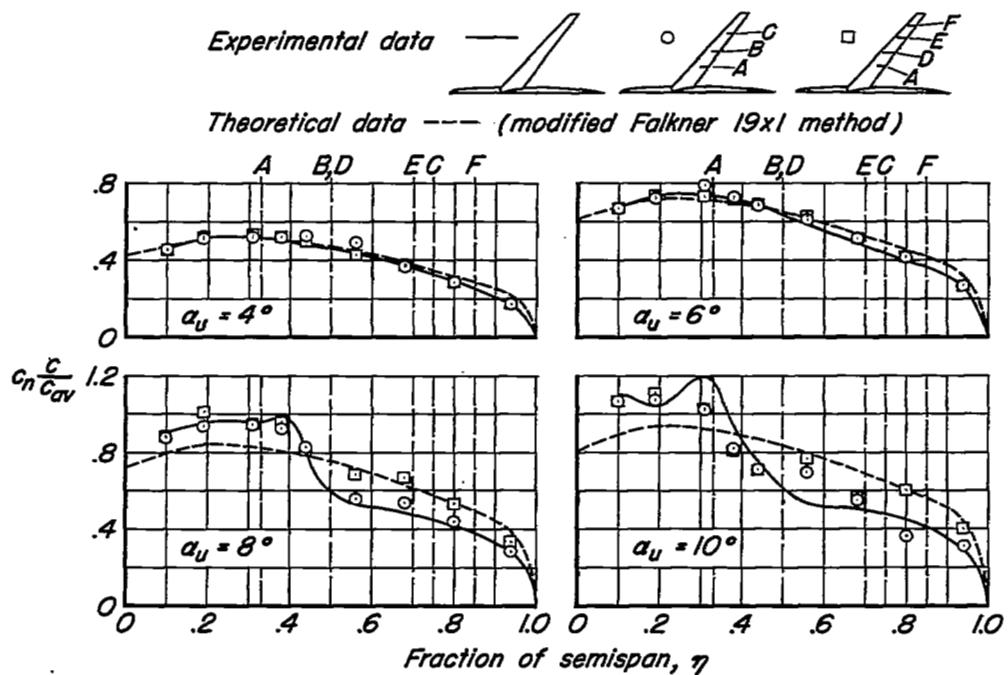
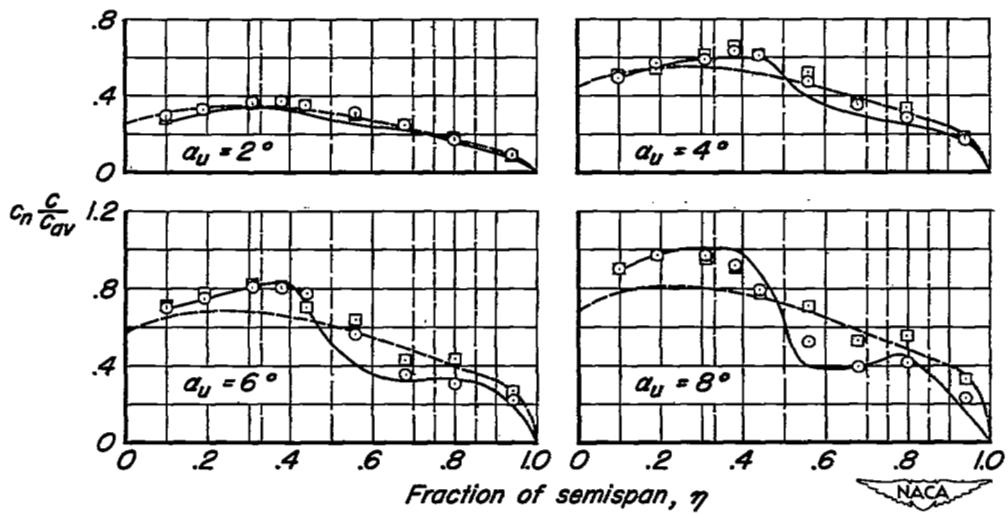
(c) $M, 0.80; R, 2,000,000$ (d) $M, 0.90; R, 2,000,000$

Figure 23.-Concluded.

SECURITY INFORMATION

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